

**EVALUATION OF
OXYGEN TRANSFER
CAPABILITIES:**

**PULSED HYDRAULICS INC
MIXING SYSTEM**

BY

**GSEE, INC.
LAVERGNE, TN.
DECEMBER, 2006**



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1. INTRODUCTION

During the week of November 6, 2006, Pulsed Hydraulics Inc. (PHi) retained GSEE, Inc., to perform unsteady state clean water oxygen transfer tests on the Pulsed Hydraulics Inc. (PHi) Mixing System. Tests were performed at a liquid depth of 20' in the GSEE 21'Ø test basin. The purpose of the testing was to determine the amount of oxygen transferred by the Pulsed Hydraulics Inc. (PHi) Mixing System and to determine the effect of the Pulsed Hydraulics Inc. (PHi) Mixing System on a typical aeration system.

The PHi Mixing System testing was performed November 7-9, 2006. A single PHi Mixing System Forming Plate was installed and tested. Additionally, 28 fine bubble membrane tube diffusers were installed and tested both with and without the PHi Mixing system in operation. The following were present during all of the testing:

Dick Koopmans

Pulsed Hydraulics Inc. (PHi)

Chuck Neir

Pulsed Hydraulics Inc. (PHi)

Michael Hicks

GSEE, Inc.

Oxygen transfer is determined using the ASCE clean water non-steady state test procedures. The ASCE standard requires a regression analysis on the data from each sample location and then averages the obtained results.

Test results are reported at standard conditions of 20°C liquid temperature, one (1) atmosphere barometric pressure, zero (0) dissolved oxygen, and alpha (α) and beta (β) equal to 1.0 (clean tap water). All test results have also been calculated using both the ASCE linear and non-linear regression analysis methods for the determination of the mass transfer coefficient K_{LaT} , the steady-state D.O. saturation value C^* , and the D.O. concentration at time zero C_0 .

2. DESCRIPTION OF THE AERATION TEST BASIN

All testing occurred in the 21' diameter x 31' tall GSEE, Inc. test basins located in LaVergne, TN. The GSEE 21'Ø test basin is shown in Figure 2-1.

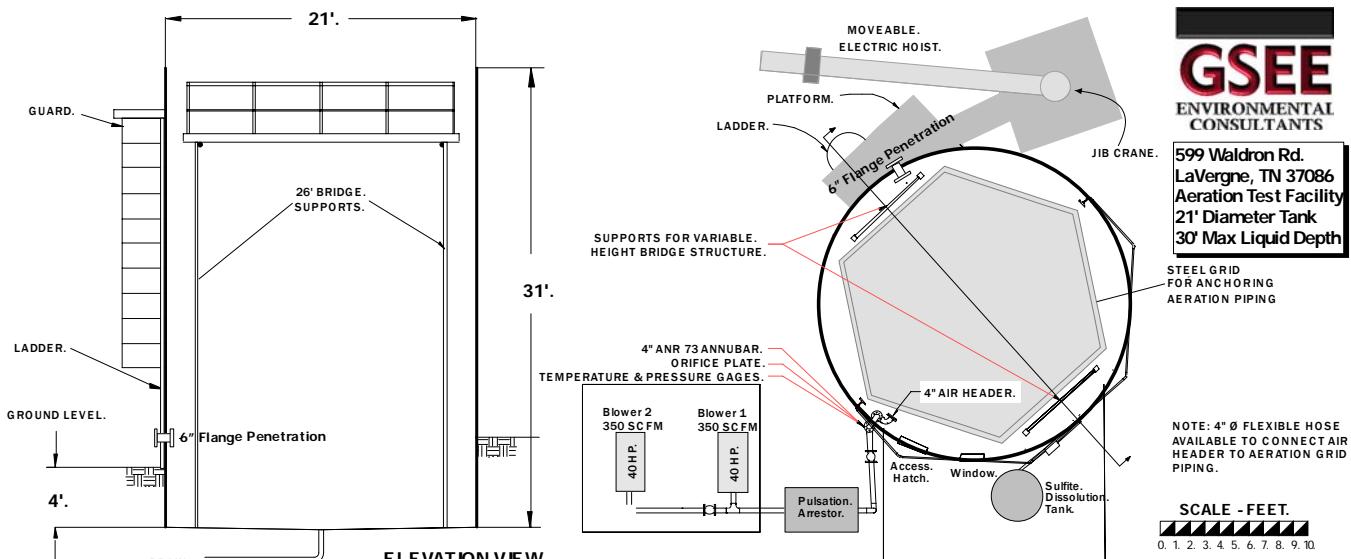
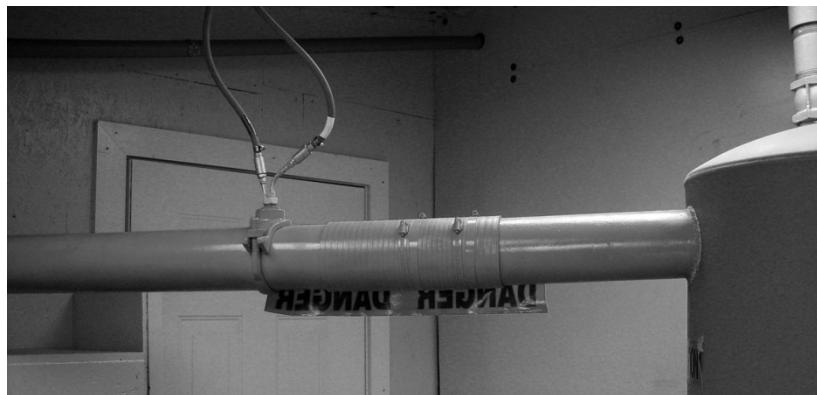
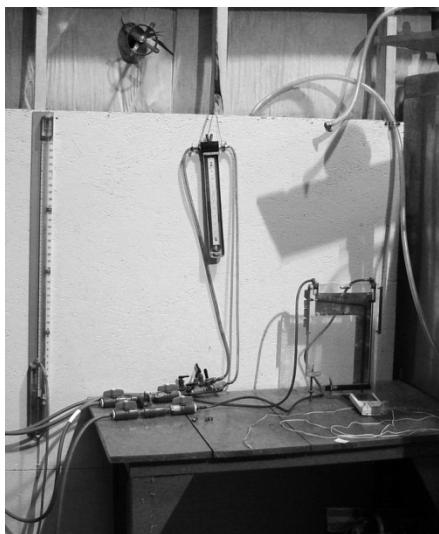


Figure 2-1 GSEE Test Facility

Air was supplied to the Pulsed Hydraulics Inc. (PHi) Mixing System via a Kaeser 5HP compressor.

The air sources for the fine bubble membrane tube diffusers are two positive displacement blowers, driven by 40HP and 50HP motors, respectively. The blowers used for the testing have a maximum operating pressure of 14 PSIG. A bypass valve is used to obtain airflow rates from 0 to 700 SCFM. Exact measurement of the airflow supplied to the test basin is determined using both a 4" ANR-73 Annubar air flow meter and a 1.349"Ø orifice plate installed in the header pipe. Measurement of airflow across the Annubar is monitored using a DWYER oil-filled combination vertical/inclined manometer. Measurement of airflow across the orifice plate is monitored using a water-filled vertical manometer. A mercury manometer is used to monitor the flowing air line pressure. A temperature probe monitors line temperature during each test. A mercury barometer is used to monitor local atmospheric pressure.

The following photographs show the blowers and airflow monitoring equipment:



2.1. Air Flow Calculations

Airflow rate is defined as follows:

SCFM = Standard Cubic Feet per Minute (14.7 PSIA, 68°F, 36% RH and a density of 0.075 Lb/Ft³)

ACFM or Actual Cubic Feet per Minute refers to air flowing at any condition other than standard. ACFM can be calculated as follows:

$$\text{ACFM} = \left[\frac{BP_s - (Rh_s \times Pv_s)}{BP - (Rh_a \times Pv_a)} \right] \times \frac{BP}{(BP + LP)} \times \frac{(460 + LT)}{528} \times SCFM \quad \text{Eq. 2-1}$$

Where:

BP_s	=	Standard Barometric Pressure, 14.7 PSIA
Rh	=	Relative Humidity, % (s = Standard 36%, a = actual operating conditions)
Pv_a	=	Vapor Pressure of Water, psi (s = standard 0.3391, a = at actual temperature)
BP	=	Site Barometric Pressure, PSIA
LP	=	Flowing Line Pressure, PSIG
LT	=	Flowing Line Temperature, °F
528	=	Standard Temperature (460 + 68°F), °R

ICFM is a special form of ACFM referring to the air flow rate at the blower inlet. ICFM is calculated as follows:

$$\text{ICFM} = SCFM \times \left[\frac{BP_s - (Rh_s \times Pv_s)}{BP - (Rh_a \times Pv_a)} \right] \times \frac{(460 + Ta)}{528} \quad \text{Eq. 2-2}$$

Where:

Ta	=	Site Temperature, °F
-----------	---	----------------------

The observed airflow rate may be converted to SI units as follows:

$$\text{Nm}^3 / hr = SCFM \times 0.62067 \quad \text{Eq. 2-3}$$

Where:

Nm³/hr	=	Normal Cubic Meters Per hour (1 Atm., 0°C, 0% Rh)
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The exact airflow rate for each test run is calculated using the following equation¹:

$$SCFM = C'' \sqrt{\frac{(BP + LP)}{(460 + LT)} \Delta h} \quad \text{Eq. 2-1}$$

Where:

C''	=	Annubar Coefficient, corrected for site relative humidity
LT	=	Line Temperature, °F
LP	=	Line Pressure, PSIG
BP	=	Site Barometric Pressure, PSIA
Δh	=	Differential across air flow meter, inches of H ₂ O
SCFM	=	Standard Cubic Feet per Minute (14.696 PSIA, 68°F, 36% RH and a density of 0.075 Lb/Ft ³)

The air flow device coefficient C'' is a C' value that produces the humidity corrected SCFM as described in Eq. A-1, page 14, Annex A of the ASCE Standard "Measurement of Oxygen Transfer in Clean Water".

Once C' is determined, the air flow rate in SCFM is calculated by the following:

¹ Spink, L.K.

"Principles and Practice of FLOW METER ENGINEERING" Ninth Edition, 1975
The FOXBORO COMPANY, Foxboro, Mass.

$$SCFM = C' \sqrt{\frac{(BP + LP)}{(460 + LT)} \Delta h} \quad \text{Eq. 2-2}$$

Where:

C' = Annubar Coefficient

This value of SCFM is not corrected for the observed relative humidity. To correct for humidity, SCFM is converted to ACFM by:

$$ACFM = \frac{14.7}{(BP + LP)} \times \frac{(460 + LT)}{528} \times SCFM \quad \text{Eq. 2-3}$$

The airflow rate in ACFM is then corrected for relative humidity using Eq. A-1 from the ASCE Standard:

$$Q_s = 36.2 \times \left[\frac{(BP + LP) \times \left(1 - \frac{Rh \times Pva}{Pb} \right)}{460 + LT} \right] \times ACFM \quad \text{Eq. 2-4}$$

Where:

Rh = Relative Humidity, %

Pva = Vapor Pressure of Water at ambient temperature

Qs = Humidity corrected air flow rate, SCFM

Once Q_s has been determined, the value of C'' is calculated as follows:

$$C'' = \frac{Q_s}{\sqrt{\frac{(BP + LP)}{(460 + LT)} \Delta h}} \quad \text{Eq. 2-5}$$

Where:

C'' = Humidity corrected C'

The observed airflow rate was converted to SI units as follows:

$$\text{Nm}^3 = SCFM \times 0.62067 \quad \text{Eq. 2-6}$$

Where:

Nm³ = Normal Cubic Meters per Minute (1 Atm., 0°C, 0% Rh)

2.2. Horsepower

The blower HP_{motor} can be determined as follows:

$$HP_{motor} = GHP + MHP \quad \text{Eq. 2-7}$$

Where:

GHP = Gas Horsepower (From adiabatic compression, shown below)

MHP = Mechanical Horsepower (Loss in gear reducers, etc.)

The basic equation for determining the gas horsepower is:

$$GHP = \frac{W_a \times H_a}{33,000 \times \eta_o} \quad \text{Eq. 2-8}$$

Where:

W_a	=	Weight flow of gas, Lbs/Min
H_a	=	Adiabatic Head, Ft-Lbf/Lb _m
η_o	=	Blower Overall Efficiency, %
33,000	=	Units Conversion Factor, Ft-Lbf/Min/HP

The Weight Flow of gas (W_a) can be determined as follows:

$$W_a = ACFM \times \rho \quad \text{Eq. 2-9}$$

Where:

ACFM	=	Actual flow of gas at discharge conditions
ρ	=	Density of flowing gas at discharge conditions
=		$\frac{MW_m \times (BP + LP)}{10.72 \times (LT + 460)}$

Where:

MW_m	=	Molecular Weight of Moist flowing gas
=		$MW_d \times G$

Where:

MW_d	=	Molecular Weight of dry gas
G	=	Specific Gravity of moist gas
=		$1 - \frac{0.378 \times Rh \times Pv_a}{BP}$

The Adiabatic Head (H_a) is calculated as follows:

$$H_a = \frac{R \times Ta \times \left[\left(\frac{BP + LP}{BP} \right)^{\frac{k-1}{k}} - 1 \right]}{\frac{k-1}{k}} \quad \text{Eq. 2-10}$$

Where:

R	=	Gas Constant, Ft-Lbf/Lb _m °R
=		$\frac{1,545}{MW_m}$
k	=	Ratio of specific heats, C _p /C _v

Four (4) Yellow Springs Instruments (YSI) D.O. probes were installed in the test basin to monitor the dissolved oxygen levels during each test. A YSI Model 556 MPS multi parameter meter and probe was used to monitor water quality (Temp, pH, ORP, TDS, D.O., and Barometric Pressure) during each test. The exact aeration grid arrangement is shown as follows:

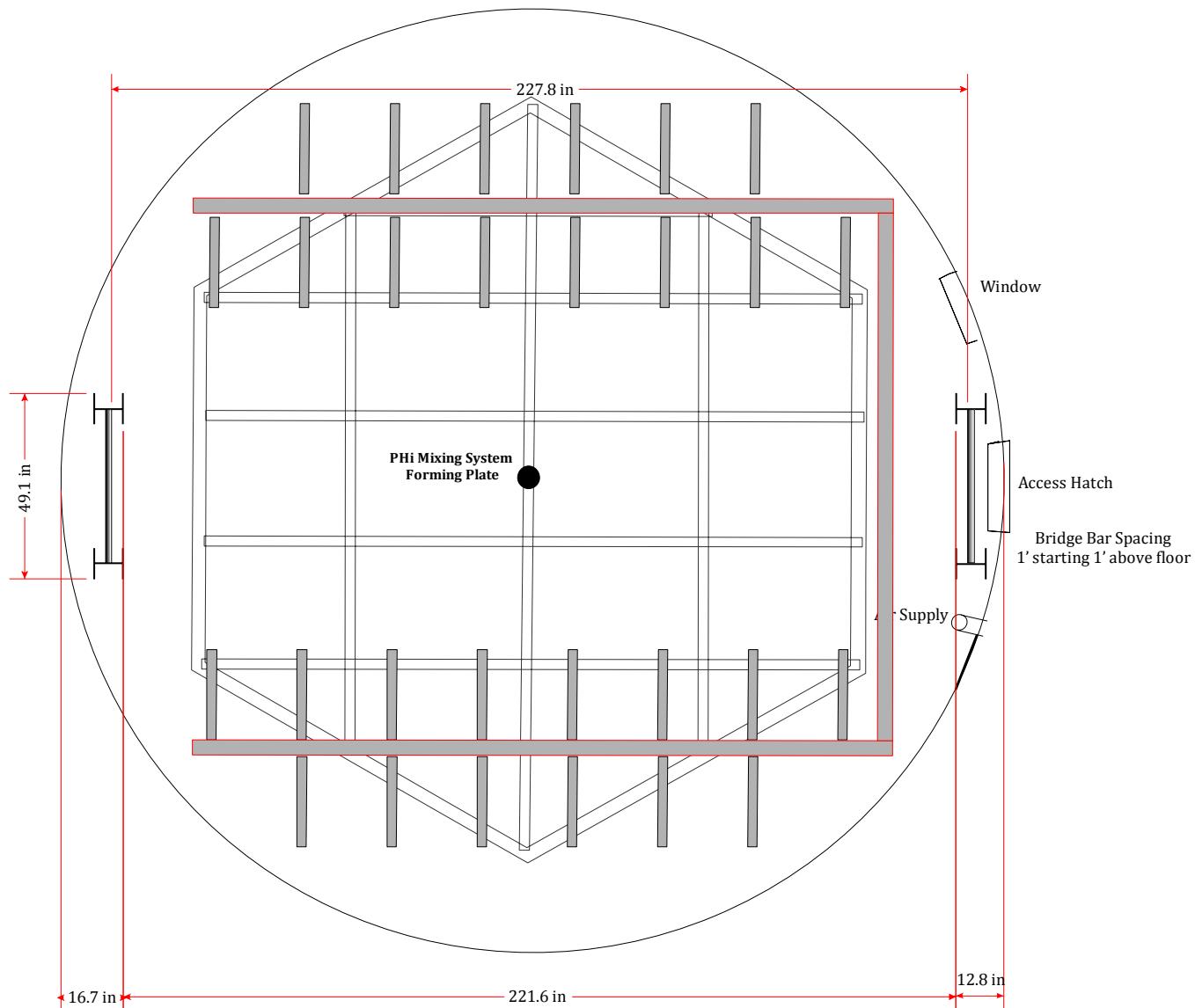


Figure 2-2 – Aeration Gird Arrangement

3. DESCRIPTION OF THE AERATION DEVICES

3.1. Pulsed Hydraulics Inc. (PHi) Mixing System

The Pulsed Hydraulics Inc. (PHi) Mixing System consists of the following:

1. Stainless Steel Forming Plate
2. Kaeser 5HP Compressor
3. Pressure Regulator
4. PLC Control System
5. Rapid Response Injection Valve

3.2. Membrane Tube Diffusers

The fine Bubble membrane tube diffuser aeration system tested consisted of the following:

1. 28 Sanitaire Membrane Tube Diffusers
2. Each diffuser is a $2\frac{1}{2}'' \times 24''$ long EPDM perforated membrane tube

4. TEST PROCEDURES

Before testing, the aeration basin was thoroughly cleaned and filled with potable water.

Four (4) YSI dissolved oxygen meters and probes were placed in the test basin and later used to monitor the dissolved oxygen concentration during each test. The probes were located as follows:

Probe	Probe Depth Below Water Surface (Ft)
1	17
2	3
3	10
4	5
YSI MPS 556	12

Overall test procedures include:

After filling the test basin with tap water, add enough cobalt catalyst to obtain a concentration of cobaltous ion less than 0.1 mg/l. Dissolve the catalyst into the basin contents by running the aeration system a minimum of thirty minutes before testing.

Add enough (100-200% of stoichiometric) sodium sulfite to deoxygenate the tap water in the basin to start each test. Monitor the dissolved oxygen concentration as it depletes then starts to rise, using the *in-situ* dissolved oxygen probes. Measure the water temperature using the D.O. Probe thermisters.

With the aeration system operating at the specified liquid depth, start monitoring as the oxygen concentration increases. Collect data to cover a range of dissolved oxygen concentrations from 1.0 mg/l to 98% of saturation, obtaining a minimum of 100 data points for each probe.

I. **The general test procedures** are:

1. Thoroughly clean the aeration basin before testing and fill with tap water to the desired liquid depth.
2. Operate the aeration system in potable water at the test airflow rate and operating liquid depth for 30 minutes before testing to obtain temperature and mixing equilibrium. Record the liquid temperature a minimum of two times during each test run. Maintain the required airflow rate during testing by monitoring manometers connected across the airflow devices. Monitor operating air pressure and headloss via a mercury manometer. Measure the operating line temperature.
3. Install 4 dissolved oxygen probes with integral stirrers at locations in the test tank as required.
4. Use Cobalt Chloride ($\text{CoCl}_2 \cdot 6\text{H}_2\text{O}$) as a catalyst at a concentration of 0.1 mg/l.
5. Use anhydrous sodium sulfite technical grade (Na_2SO_3) to deoxygenate the test liquid. Add sulfite solution before each test run to decrease the oxygen concentration to zero (1.00 mg/l or less D.O.) and maintained zero for 1 to 3 minutes.
6. Use the azide modification of the Winkler method to calibrate the D.O. probes. Collect a minimum of one-hundred (100) D.O. observations for each D.O. probe between 10 and 98% of saturation.

II. **Detailed test procedures:**

A. **Initial setup**

1. Inspect aeration basin for adequate cleanliness, level of diffusers and correct water depth.
2. Check installation of airflow monitoring device.
3. Check D.O. probe thermisters for liquid temperature monitoring.
4. Prepare YSI (Yellow Springs Instruments) Dissolved Oxygen (D.O.) probes for installation.

- a) Replace electrolyte solution and membranes on each D.O. probe
 - b) Connect probes to YSI D.O. meters
 - c) Check each probe for functioning stirrer mechanism
 - d) Connect all D.O. meters to computer for data logging
 5. Check the placement of each D.O. probe in the test basin.
 6. Start the blowers and begin aerating the test tank.
 7. Check all air flow meters, gages, valves, and fittings on the air supply system for air leakage.
 8. Collect at least two samples from the oxygen saturated aeration basin for analysis using the Winkler titration method to determine the D.O. concentration.
 9. Calibrate all D.O. probes and meters to the saturation value determined by the Winkler method.
 10. Check installation of the temperature gage in the aeration header piping system for the accurate determination of flowing air temperature.
 11. Dissolve Cobalt Chloride into a container of water.
 12. Pour Cobalt solution into the aeration basin.
 13. Allow a minimum of thirty minutes mixing of the cobalt into the aeration basin before the start of testing.
- B. Procedure for clean water aeration testing.
1. Adjust the airflow rate to the test basin to the required test airflow.
 2. Read and record the following data:
 - a) Site barometric pressure (PSIA)
 - b) Operating line pressure from the mercury manometer connected to the header system (PSIG)
 - c) Operating line temperature ($^{\circ}$ F)
 - d) Δh from the Annubar, (Inches of H₂O)
 - e) Liquid Temperature ($^{\circ}$ C)
 - f) Aeration basin oxygen saturation value C_{so} (mg/l) [Winkler Analysis]
 - g) Ambient temperature
 - h) Relative Humidity, %
 3. Pump sodium sulfite slurry into the aeration test basin.
 4. Begin observing D.O. meters.
 5. Monitor D.O. on each of the YSI meters as it drops to 1.0 mg/l.
 6. Continue recording D.O. values versus time for each of the D.O. probes, obtaining a minimum of 100 D.O. values for each probe.
 7. Stop all recording of D.O. values when the aeration basin has reached 6/K_{La}.
 8. Collect a basin water sample and analyze for Total Dissolved Solids (TDS – mg/L)
 9. Perform non-linear regression analysis on the collected data.
 - a) Determine K_{La20} values for each probe
 - b) Calculate SOTR, SOTE, and SAE.
 10. Repeat steps 1-9 for each test run.

5. DATA ANALYSIS METHODS

5.1. Standard ASCE Data Analysis Method

The basic mass-transfer model² used to determine oxygen transfer is as follows:

² Brown, L.C. and Baillod, C.R., "Modeling and Interpreting Oxygen Transfer Data", A.S.C.E. Jour. Environ. Engr. Div., 108, EE4, 607 (1982)

$$\frac{dC}{dT} = K_L a (C^* - C) \quad \text{Eq. 5-1}$$

Which, upon integration, with initial condition $C = C_0$ at $t = 0$, becomes:
(logarithmic form)

$$\ln\left[\frac{C^* - C}{C^* - C_0}\right] = -K_L a t \quad \text{Eq. 5-2}$$

or

(exponential form)

$$C = C^* - (C^* - C_0) e^{-k_L a t} \quad \text{Eq. 5-3}$$

Where:

- C** = D.O. Concentration, mg/L
- C^*** = Equilibrium D.O. concentration, the concentration obtained as time approaches infinity, mg/L
- C_0** = D.O. concentration at time zero, mg/L
- $K_L a$** = Apparent volumetric mass transfer coefficient, t^{-1}

The overall mass transfer coefficient (K_{Lat}) is obtained experimentally by aerating deoxygenated water and observing the rate of change of dissolved oxygen (D.O.) concentration about time.

A non-linear regression of D.O. about time is used to determine K_{Lat} , C^* , and C_0 .

The logarithmic form of the mass transfer model can be rearranged to determine K_{Lat} using a log-deficit linear regression as follows:

$$K_L a_T = \frac{60}{t_2 - t_1} \ln\left[\frac{C^* - C_1}{C^* - C_2}\right] \quad \text{Eq. 5-4}$$

Where:

- K_{Lat}** = Apparent volumetric mass transfer coefficient at test liquid temperature T , hr^{-1}
- C^*** = The observed saturation concentration of oxygen in the test basin at test temperature and barometric pressure at equilibrium, mg/L after an aeration period equal to $6/K_{Lat}$
- C_1 and C_2** = Dissolved oxygen concentration at time t_1 and t_2 respectively, mg/L

For purposes of comparison, K_{Lat} must be corrected to standard temperature, $20^\circ C$. The appropriate correction has been found empirically to be:

$$K_L a_{20} = K_L a_T \Theta^{(20-T)} \quad \text{Eq. 5-5}$$

Where:

- T** = test liquid temperature ($^\circ C$)
- Θ** = 1.024 for all T

With the value of K_{La20} known, it is possible to calculate the pounds of oxygen transferred to the test liquid at standard conditions of $20^\circ C$, maximum oxygen deficit (dissolved oxygen equal to zero), one atmosphere barometric pressure, and alpha and beta equal to 1.0 (clean tap water) for each sample point.

$$\text{SOTR}_i = K_L a_{20i} C_{\infty 20i}^* V$$

Eq. 5-6

Where:

SOTR_i = pounds of oxygen transferred to the test liquid, lb O₂ /hr, for Probe i

V = Liquid volume of water in the test tank with aerators turned off

$$C_{\infty 20i}^* = C_{\infty}^* \left(\frac{1}{\tau \Omega} \right)$$

τ = Temperature correction factor, C_{st}^{*}/C_{s20}^{*}

C_{s20}^{*} = 9.092 mg/L, standard D.O. concentration at 20°C and one atmosphere

C_{st}^{*} = oxygen saturation concentration from **Standard Methods**, mg/L, at test liquid temperature *T*

Ω = Pressure correction factor, P_b/P_s

P_b = Site barometric pressure, PSIA

P_s = Standard barometric pressure, 14.73 PSIA

The overall average value of SOTR is then calculated as the average of the individual SOTR_i values determined for each sample point.

Calculate the standard percent oxygen transfer (SOTE - %) once the oxygen transfer rate is known using the following equation:

$$\text{SOTE} = \frac{\text{SOTR} \times 100}{\text{SCFM} \times 1.036}$$

Eq. 5-7

The blower wire HP is determined using the adiabatic compression formula as described in Section 2 of this report.

Calculate the standard aerator efficiency (SAE) using the following equation:

$$\text{SAE} = N_o = \frac{\text{SOTR}}{\text{HP}}$$

Eq. 5-8

Where:

No = aerator efficiency, lb. O₂/hr-Hp

SOTR = Q_o, standard oxygen transfer rate, lb. O₂/hr

HP_{wire} = Blower HP determined by the adiabatic compression formula

Finally, the reported values may be corrected to a standard TDS concentration of 1,000 mg/L using the following:

$$K_L a_{T \text{ TDS Corrected}} = K_L a_{T \text{ observed}} \times e^{(0.0000965 \times [1000 - \text{TDS}])}$$

Eq. 5-9

Where:

TDS = Observed Total Dissolved Solids concentration for each run, mg/L

All values are then recalculated based on the corrected K_{LaT}.

6. DISCUSSION OF RESULTS

Table 6-1 is a summary of the results of the GSEE, Inc. analysis of the data obtained during the oxygen transfer testing on the Pulsed Hydraulics Inc. (PHi) Mixing System. Individual computer printouts of

the data analysis including time versus D.O. plots for each test run using the specified data analysis method are contained in Appendix 9.1.

Table 6-1 Summary of Oxygen Transfer Test Results

DATE: RUN:	7-Nov-06 1	8-Nov-06 2	8-Nov-06 3	9-Nov-06 4
Barometric Pres. (PSIA)	14.18	14.19	14.18	14.23
Ambient Temperature (°F)	57.0	61.8	64.4	67.9
Relative Humidity (%)	0.68	0.68	0.64	0.57
Line Pressure (PSIG)	45.02	8.87	8.87	45.02
Line Temperature (°F)	57	130	136	68
Water Temp. (°C)	14.61	14.61	14.70	14.96
Orifice Diameter (in)	1.840	1.349	1.349	1.840
Number Of Aeration Devices	1	28	28	1
Side Water Depth (ft)	20.00	19.75	19.75	19.25
Air Release Depth (ft)	20.00	18.75	18.75	19.25
Tank Diameter (ft)	21.00	21.00	21.00	21.00
Average Air Flow (SCFM)	25	41	40	38
Average Air Flow (SCFM/Tube)	25.11	1.47	1.43	37.93
C*20 Standard Conditions	9.62	10.74	10.72	9.16
Tank Volume (Ft ³)	6,927	6,841	6,841	6,667
TDS (mg/L)	318	452	568	676
KLa20 (hr⁻¹)	0.15	2.43	2.90	0.12
SOTR (Lb O₂/Hr)	0.6	11.2	13.3	0.5
SOTE OBSERVED (%)	2.4%	26.2%	32.1%	1.2%
TDS Corrected Results				
KLa20 (hr⁻¹)	0.16	2.57	3.02	0.13
SOTR (Lb O₂/Hr)	0.7	11.8	13.9	0.5
SOTE OBSERVED (%)	2.6%	27.7%	33.5%	1.2%
SOTE (%/Ft)	0.13%	1.48%	1.79%	0.06%

Tests 1 and 4 were performed with only the PHi mixing system in operation. Test 4 was performed using a faster response valve than the one used in tests 1 and 3. Tests 2 was performed using only the 28 fine bubble membrane tube diffusers. Tests 3 used both the membrane tube diffusers and the PHi mixing system.

Note that the PHi mixing system was operated at 65 PSIG rather than 45 PSIG during test 3. The pressure was increased based on visual observation. The increased pressure was required so that the mixing pattern established by the PHi Mixing System would overpower the mixing pattern of the membrane tube diffusers. The increased pressure increased the air flow of the PHi Mixing system from 25 SCFM (6.1 ACFM) observed in Test 1 to 43.7 SCFM (8.1 ACFM) in Test 3. This means an estimated increase in the SOTR from 0.67 lb O₂/Hr for Test 1 to 1.16 lb O₂/Hr for Test 3.

Test 2 indicates that the membrane tube diffusers provide 11.83 lb O₂/Hr at an air flow rate of 41 SCFM. The combination of membrane tubes and PHi Mixing System in Test 3 produced 13.89 lb O₂/Hr. The sum of the individual tests indicate an oxygen transfer of 12.99 lb O₂/hr (11.83+1.16). The combination of the membrane tube diffusers with the PHi Mixing System shows an overall oxygen transfer enhancement of 7.6%.

The Oxygen transfer produced by the PHi Mixing System is significantly lower than equivalent coarse bubble aeration. Coarse bubble aeration typically produces Standard Oxygen Transfer Efficiencies of 0.6% to 0.9% per foot of submergence at depths less than 30'. During Test 1 the PHi Mixing System only produced an SOTE of 0.13% per foot of submergence. Using the faster response valve in Test 4, the SOTE was cut in half to only 0.06% per foot of submergence.

7. CONCLUSIONS AND RECOMMENDATIONS

The results of the unsteady state clean water oxygen transfer tests on the Pulsed Hydraulics Inc. (PHi) Mixing System indicate the following:

1. Oxygen transfer (SOTE) is less than 1/10 that of comparable coarse bubble aeration systems.
2. Combining the PHi Mixing System with a typical fine bubble aeration system enhanced SOTR by 7.6% above the sum of the individual systems.

8. CERTIFICATION

GSEE, Inc., certifies that the results presented in this report are accurate and were obtained using the test procedures described above.



Gerald L. Shell, PE

9. APPENDIX**9.1. Regression Analysis Printouts**

ASCE OXYGEN TRANSFER DETERMINATION

PROJECT: Phi Unit Alone - Pumping				599 Waldron Rd. LaVergne, TN 37086 615/793-7547 FAX 615/793/5070
DATE: 7-Nov-06				
RUN: 1				
	Initial	Mid Point	Final	
Barometric Pres. (PSIA) (mm Hg)	14.186 733.60	14.178 733.20	14.172 732.90	C' Air Flow Device 1 (Annubar) 1,522.09 Air Flow Device 1 (SCFM) 25.08
Ambient Temperature (°F)	61.90	55.00	54.00	C' Air Flow Device 2 (Orifice) 249.82 Air Flow Device 2 (SCFM) 25.15
Relative Humidity (%)	68%	68%	68%	
Line Pressure (PSIG) (In. Hg)	44.943 91.50	45.188 92.00	44.943 91.50	
Line Temperature (°F)	61.90	55.00	54.00	
ΔH Air Flow Dev. 1 (Annubar)	0.002	0.002	0.002	
ΔH Air Flow Dev. 2 (Orifice)	0.089	0.089	0.089	Average Air Flow (SCFM) 25.11
ΔH Air Flow Dev. 3 (Annubar)	NA	NA	NA	Effective Depth Correction (f) 0.10
ΔH Air Flow Dev. 4 (Annubar)	NA	NA	NA	Headloss (In. H ₂ O) 1,006.35
Water Temp. (°C)	14.70	14.60	14.54	C* (mg/l) 10.40
Orifice Diameter (in)		1.840		CsmT (Standard Methods, mg/l) 10.17
Number Of Aeration Devices		1		C* ₂₀ Standard Conditions 9.62
Side Water Depth (ft)		20.00	(6.08 m)	Tank Volume (Ft ³) 6,927.2
Air Release Depth (ft)		20.00	(6.08 m)	(Gallons) 51,819.1
Tank Length (ft)		0.00	(0.00 m)	(m ³) 196.2
Tank Width (ft)		0.00	(0.00 m)	(Million Pounds) 0.432
Tank Diameter (ft)		21.00	(6.38 m)	#Na ₂ SO ₃ @ 160% Stoichiometric 57
Gear Reducer or Belt Efficiency		100.0%		Cobalt Concen. (mg/l) 0.100
Motor Efficiency		93.0%		Grams Cobalt Chloride 80.9
Total HP _{wire} av.		3.76	(2.80 kw)	Total HP _{motor} av. 3.50
				TDS (mg/L) 318.00

NON-LINEAR REGRESSION RESULTS

Probe	K _{LAT}	K _{La20}	SOTR	SOTR/Dev	SOTE	SAE _{wire}	C*	Std. Err.
1	0.13	0.15	0.62	0.62	2.37	0.16	10.40	0.0654
NA	NA	NA	NA	NA	NA	NA	NA	NA
3	0.13	0.14	0.60	0.60	2.29	0.16	10.40	0.0115
4	0.14	0.16	0.66	0.66	2.53	0.17	10.40	0.0392
avg.	0.13	0.15	0.62	0.62	2.40	0.17	10.40	0.0387
Avg	0.13	0.15	0.62	0.62	2.37	0.16	10.40	Exclude Max&Min
TDS	0.14	0.16	0.67	0.67	2.56	0.18	10.40	0.128%
<i>Corrected</i>	/hr	/hr	#O2/hr		%	#O2/hr-WHP		

OXYGEN TRANSFER

Total SCFM:	25.1	40.375 :Nm ³ /Hr	11.852 L/s	#O2/Hr:	0.67	0.302 :KgO2/Hr
SCFM/Diff.:	25.11	40.375 :Nm ³ /hr/Diff		#O2/Hr/Diff.:	0.67	0.302 :KgO2/Hr/Diff.
SCFM/KCF:	3.6	0.206 :Nm ³ /hr/m ³		#O2/Day:	16.0	7.2 :KgO2/Day
Total ICFM:	25.5	12.05 L/s		#O2/Day/1000 Ft ³ :	2	0.04 :KgO2/Day/m ³

LINEAR REGRESSION RESULTS

Probe	K _{LAT}	K _{La20}	SOTR	SOTR/Dev	SOTE	SAE _{wire}	C*	Corr. Coeff.
1	0.12	0.14	0.58	0.58	2.22	0.15	10.48	0.9973
NA	NA	NA	NA	NA	NA	NA	NA	NA
3	0.13	0.14	0.59	0.59	2.28	0.16	10.33	0.9999
4	0.14	0.15	0.64	0.64	2.47	0.17	10.40	0.9996
avg.	0.13	0.15	0.60	0.60	2.32	0.16	10.41	0.9990
Avg	0.13	0.14	0.60	0.60	2.30	0.16	10.40	Exclude Max&Min
TDS	0.14	0.15	0.65	0.65	2.48	0.17	10.41	
<i>Corrected</i>	/hr	/hr	#O2/hr		%	#O2/hr-HPw		

EUROPEAN STANDARD

Probe	K _{LAT}	K _{La10}	SOTR	SOTR/Dev	SAE	C*
1	0.13	0.11	0.27	0.27	0.09	10.40
NA	NA	NA	NA	NA	NA	NA
3	0.13	0.11	0.27	0.27	0.10	10.40
4	0.14	0.12	0.29	0.29	0.10	10.40
NA	NA	NA	NA	NA	NA	NA
NA	NA	NA	NA	NA	NA	NA
avg.	0.13	0.12	0.27	0.27	0.10	10.40
Avg	0.13	0.11	0.27	0.27	0.10	10.40
TDS	0.14	0.12	0.29	0.29	0.10	10.40
<i>Corrected</i>	/hr	/hr	kg O ₂ /hr		kg O ₂ /hr-kw	mg/L

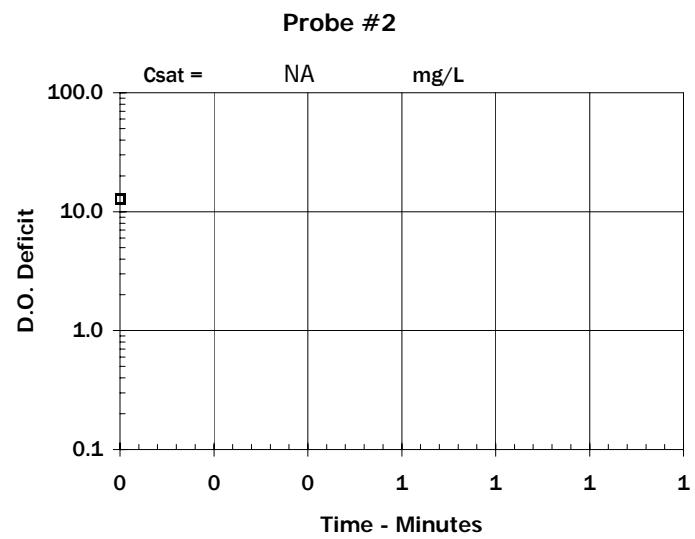
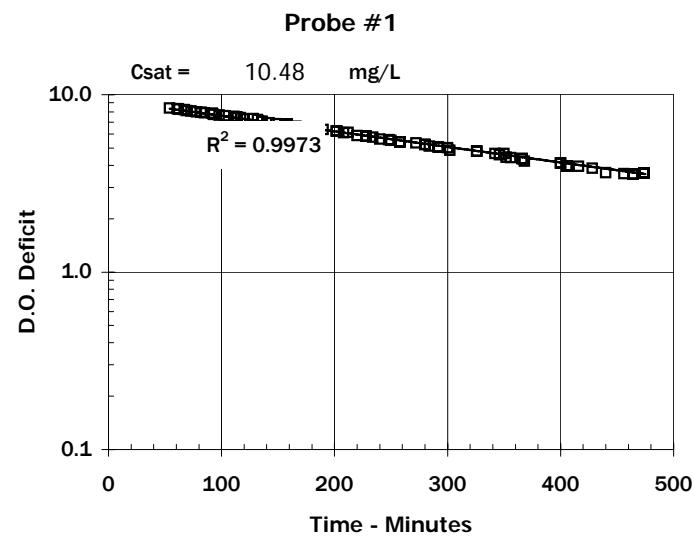
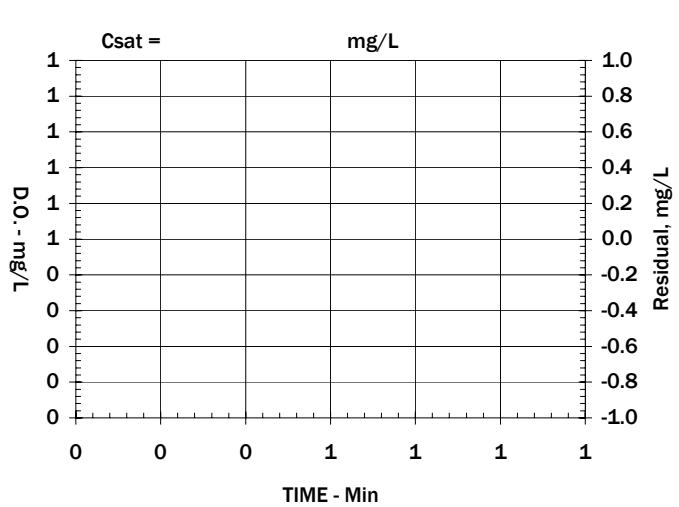
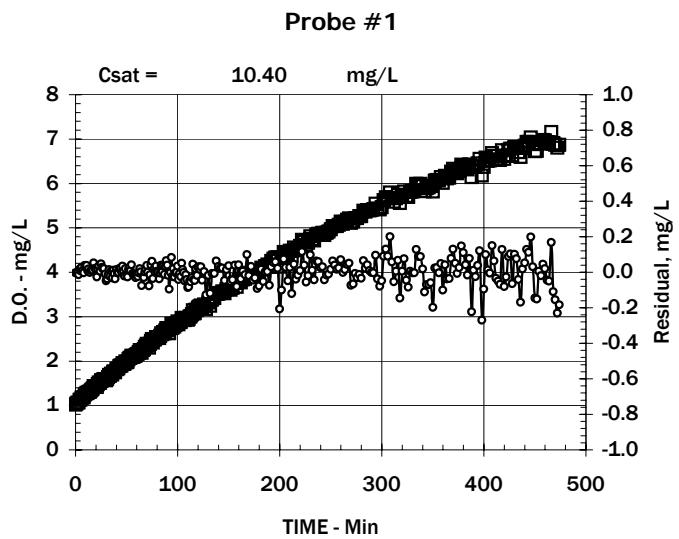
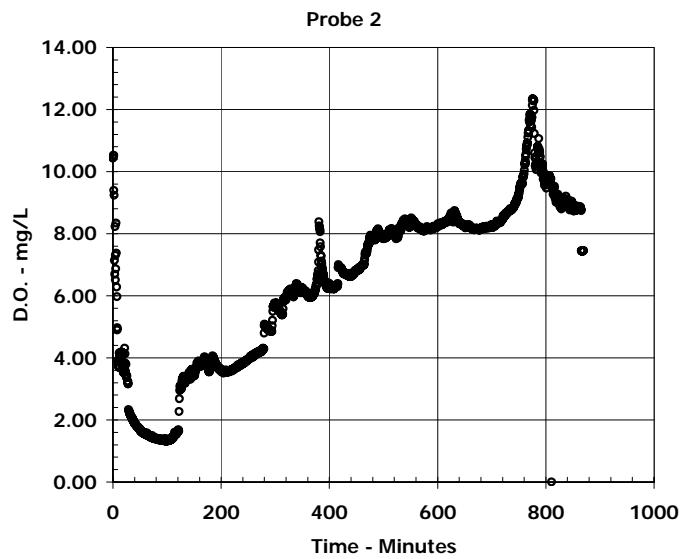
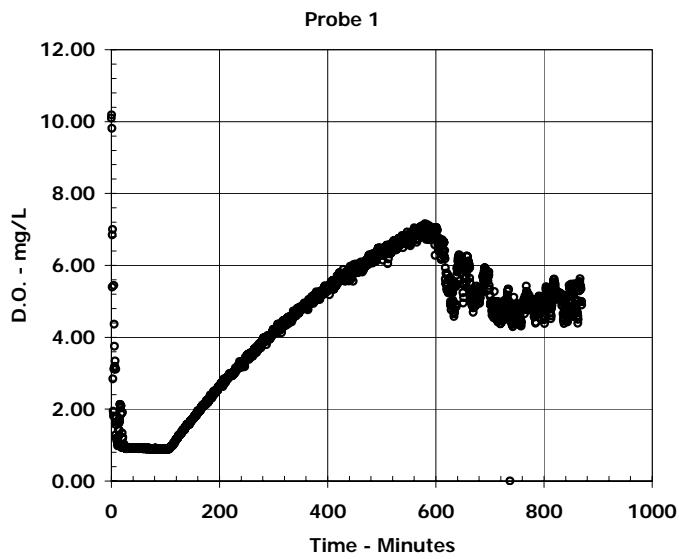
Pt. 1	est.	calc.	Pt. 2	Not Used	Pt. 3	est.	calc.	Pt. 4	est.	calc.		
CO	1.02	1.02			CO	1.03	1.03	CO	2.21	2.21		
Kla-in	0.13	0.13			Kla-in	0.13	0.13	Kla-in	0.14	0.14		
C*	10.40	10.40			C*	10.40	10.40	C*	10.40	10.40		
Sq.Dif.	1.2718				Sq.Dif.	0.0391		Sq.Dif.	0.4566			
Time	D.O.	D.O.calc	diff		Time	D.O.	D.O.calc	diff	Time	D.O.	D.O.calc	diff
0.00	1.02	1.0	0.0		0.00	1.04	1.0	0.0	0.00	2.22	2.2	0.0
1.00	1.04	1.0	0.0		1.00	1.08	1.1	0.0	1.00	2.30	2.2	0.1
2.00	1.06	1.1	0.0		2.00	1.08	1.1	0.0	2.00	2.32	2.2	0.1
3.00	1.07	1.1	0.0		3.00	1.09	1.1	0.0	3.00	2.34	2.3	0.1
4.00	1.12	1.1	0.0		4.00	1.13	1.1	0.0	4.00	2.32	2.3	0.0
5.00	1.13	1.1	0.0		5.00	1.14	1.1	0.0	5.00	2.34	2.3	0.0
6.00	1.17	1.1	0.0		6.00	1.15	1.1	0.0	6.00	2.36	2.3	0.0
7.00	1.17	1.2	0.0		7.00	1.16	1.2	0.0	7.00	2.36	2.3	0.0
8.00	1.18	1.2	0.0		8.00	1.18	1.2	0.0	8.00	2.37	2.4	0.0
9.00	1.24	1.2	0.0		9.00	1.20	1.2	0.0	9.00	2.36	2.4	0.0
10.00	1.26	1.2	0.0		10.00	1.23	1.2	0.0	10.00	2.42	2.4	0.0
11.00	1.28	1.2	0.0		11.00	1.25	1.2	0.0	11.00	2.44	2.4	0.0
12.00	1.27	1.3	0.0		12.00	1.27	1.3	0.0	12.00	2.47	2.4	0.0
13.00	1.30	1.3	0.0		13.00	1.28	1.3	0.0	13.00	2.47	2.5	0.0
14.00	1.30	1.3	0.0		14.00	1.31	1.3	0.0	14.00	2.50	2.5	0.0
15.00	1.33	1.3	0.0		15.00	1.31	1.3	0.0	15.00	2.52	2.5	0.0
16.00	1.35	1.3	0.0		16.00	1.32	1.3	0.0	16.00	2.52	2.5	0.0
17.00	1.37	1.4	0.0		17.00	1.37	1.4	0.0	17.00	2.54	2.5	0.0
18.00	1.43	1.4	0.1		18.00	1.38	1.4	0.0	18.00	2.47	2.5	-0.1
19.00	1.42	1.4	0.0		19.00	1.40	1.4	0.0	19.00	2.58	2.6	0.0
20.00	1.43	1.4	0.0		20.00	1.43	1.4	0.0	20.00	2.59	2.6	0.0
21.00	1.41	1.4	0.0		21.00	1.45	1.4	0.0	21.00	2.58	2.6	0.0
22.00	1.47	1.5	0.0		22.00	1.47	1.5	0.0	22.00	2.61	2.6	0.0
23.00	1.51	1.5	0.0		23.00	1.48	1.5	0.0	23.00	2.62	2.6	0.0
24.00	1.50	1.5	0.0		24.00	1.50	1.5	0.0	24.00	2.67	2.7	0.0
25.00	1.57	1.5	0.0		25.00	1.51	1.5	0.0	25.00	2.67	2.7	0.0
26.00	1.57	1.5	0.0		26.00	1.53	1.5	0.0	26.00	2.71	2.7	0.0
27.00	1.58	1.6	0.0		27.00	1.55	1.5	0.0	27.00	2.72	2.7	0.0
28.00	1.60	1.6	0.0		28.00	1.57	1.6	0.0	28.00	2.75	2.7	0.0
29.00	1.59	1.6	0.0		29.00	1.60	1.6	0.0	29.00	2.75	2.7	0.0
30.00	1.57	1.6	0.0		30.00	1.61	1.6	0.0	30.00	2.76	2.8	0.0
31.00	1.60	1.6	0.0		31.00	1.61	1.6	0.0	31.00	2.81	2.8	0.0
32.00	1.64	1.7	0.0		32.00	1.62	1.6	0.0	32.00	2.77	2.8	0.0
33.00	1.69	1.7	0.0		33.00	1.66	1.7	0.0	33.00	2.76	2.8	-0.1
34.00	1.67	1.7	0.0		34.00	1.66	1.7	0.0	34.00	2.78	2.8	0.0
35.00	1.72	1.7	0.0		35.00	1.71	1.7	0.0	35.00	2.82	2.8	0.0
36.00	1.70	1.7	0.0		36.00	1.72	1.7	0.0	36.00	2.85	2.9	0.0
37.00	1.76	1.7	0.0		37.00	1.73	1.7	0.0	37.00	2.87	2.9	0.0
38.00	1.76	1.8	0.0		38.00	1.75	1.7	0.0	38.00	2.90	2.9	0.0
39.00	1.75	1.8	0.0		39.00	1.77	1.8	0.0	39.00	2.91	2.9	0.0
40.00	1.82	1.8	0.0		40.00	1.78	1.8	0.0	40.00	2.91	2.9	0.0
41.00	1.82	1.8	0.0		41.00	1.81	1.8	0.0	41.00	2.93	3.0	0.0
42.00	1.84	1.8	0.0		42.00	1.81	1.8	0.0	42.00	2.95	3.0	0.0
43.00	1.88	1.9	0.0		43.00	1.85	1.8	0.0	43.00	2.94	3.0	0.0
44.00	1.90	1.9	0.0		44.00	1.85	1.9	0.0	44.00	2.97	3.0	0.0
45.00	1.90	1.9	0.0		45.00	1.89	1.9	0.0	45.00	2.99	3.0	0.0
46.00	1.95	1.9	0.0		46.00	1.87	1.9	0.0	46.00	3.01	3.0	0.0
47.00	1.94	1.9	0.0		47.00	1.89	1.9	0.0	47.00	3.03	3.1	0.0
48.00	1.93	2.0	0.0		48.00	1.94	1.9	0.0	48.00	3.03	3.1	0.0
49.00	1.99	2.0	0.0		49.00	1.95	1.9	0.0	49.00	3.06	3.1	0.0
50.00	1.97	2.0	0.0		50.00	1.97	2.0	0.0	50.00	3.06	3.1	0.0
51.00	1.98	2.0	0.0		51.00	1.99	2.0	0.0	51.00	3.11	3.1	0.0
52.00	2.04	2.0	0.0		52.00	1.99	2.0	0.0	52.00	3.11	3.1	0.0
53.00	2.07	2.0	0.0		53.00	2.01	2.0	0.0	53.00	3.13	3.2	0.0
54.00	2.07	2.1	0.0		54.00	2.03	2.0	0.0	54.00	3.19	3.2	0.0
55.00	2.12	2.1	0.0		55.00	2.06	2.1	0.0	55.00	3.18	3.2	0.0
56.00	2.09	2.1	0.0		56.00	2.08	2.1	0.0	56.00	3.19	3.2	0.0
57.00	2.10	2.1	0.0		57.00	2.08	2.1	0.0	57.00	3.23	3.2	0.0
58.00	2.11	2.1	0.0		58.00	2.12	2.1	0.0	58.00	3.24	3.2	0.0
59.00	2.12	2.2	0.0		59.00	2.12	2.1	0.0	59.00	3.26	3.3	0.0
60.00	2.15	2.2	0.0		60.00	2.14	2.1	0.0	60.00	3.26	3.3	0.0
61.00	2.16	2.2	0.0		61.00	2.18	2.2	0.0	61.00	3.28	3.3	0.0
62.00	2.20	2.2	0.0		62.00	2.17	2.2	0.0	62.00	3.30	3.3	0.0
63.00	2.24	2.2	0.0		63.00	2.21	2.2	0.0	63.00	3.30	3.3	0.0
64.00	2.24	2.2	0.0		64.00	2.22	2.2	0.0	64.00	3.34	3.3	0.0
65.00	2.18	2.3	-0.1		65.00	2.22	2.2	0.0	65.00	3.35	3.4	0.0
66.00	2.25	2.3	0.0		66.00	2.24	2.2	0.0	66.00	3.38	3.4	0.0
67.00	2.26	2.3	0.0		67.00	2.25	2.3	0.0	67.00	3.37	3.4	0.0
68.00	2.31	2.3	0.0		68.00	2.29	2.3	0.0	68.00	3.40	3.4	0.0
69.00	2.34	2.3	0.0		69.00	2.29	2.3	0.0	69.00	3.40	3.4	0.0
70.00	2.38	2.3	0.0		70.00	2.31	2.3	0.0	70.00	3.42	3.4	0.0
71.00	2.36	2.4	0.0		71.00	2.32	2.3	0.0	71.00	3.43	3.5	0.0
72.00	2.30	2.4	-0.1		72.00	2.33	2.3	0.0	72.00	3.44	3.5	0.0
73.00	2.38	2.4	0.0		73.00	2.34	2.4	0.0	73.00	3.44	3.5	0.0
74.00	2.45	2.4	0.0		74.00	2.38	2.4	0.0	74.00	3.48	3.5	0.0
75.00	2.49	2.4	0.1		75.00	2.38	2.4	0.0	75.00	3.50	3.5	0.0
76.00	2.41	2.4	0.0		76.00	2.42	2.4	0.0	76.00	3.44	3.5	-0.1
77.00	2.48	2.5	0.0		77.00	2.42	2.4	0.0	77.00	3.60	3.5	0.1

Pt. 1	est.	calc.	Pt. 2	Not Used	Pt. 3	est.	calc.	Pt. 4	est.	calc.		
CO	1.02	1.02			CO	1.03	1.03	CO	2.21	2.21		
Kla-in	0.13	0.13			Kla-in	0.13	0.13	Kla-in	0.14	0.14		
C*	10.40	10.40			C*	10.40	10.40	C*	10.40	10.40		
Sq.Dif.	1.2718				Sq.Dif.	0.0391		Sq.Dif.	0.4566			
Time	D.O.	D.O.calc	diff		Time	D.O.	D.O.calc	diff	Time	D.O.	D.O.calc	diff
78.00	2.48	2.5	0.0		78.00	2.43	2.4	0.0	78.00	3.56	3.6	0.0
79.00	2.53	2.5	0.0		79.00	2.45	2.5	0.0	79.00	3.53	3.6	0.0
80.00	2.52	2.5	0.0		80.00	2.47	2.5	0.0	80.00	3.56	3.6	0.0
81.00	2.53	2.5	0.0		81.00	2.50	2.5	0.0	81.00	3.59	3.6	0.0
82.00	2.51	2.6	0.0		82.00	2.50	2.5	0.0	82.00	3.61	3.6	0.0
83.00	2.56	2.6	0.0		83.00	2.52	2.5	0.0	83.00	3.59	3.6	-0.1
84.00	2.63	2.6	0.0		84.00	2.54	2.5	0.0	84.00	3.53	3.7	-0.1
85.00	2.60	2.6	0.0		85.00	2.57	2.6	0.0	85.00	3.76	3.7	0.1
86.00	2.66	2.6	0.0		86.00	2.57	2.6	0.0	86.00	3.59	3.7	-0.1
87.00	2.63	2.6	0.0		87.00	2.58	2.6	0.0	87.00	3.60	3.7	-0.1
88.00	2.69	2.7	0.0		88.00	2.62	2.6	0.0	88.00	3.65	3.7	-0.1
89.00	2.74	2.7	0.1		89.00	2.63	2.6	0.0	89.00	3.74	3.7	0.0
90.00	2.73	2.7	0.0		90.00	2.62	2.6	0.0	90.00	3.78	3.7	0.0
91.00	2.69	2.7	0.0		91.00	2.66	2.7	0.0	91.00	3.82	3.8	0.1
92.00	2.63	2.7	-0.1		92.00	2.69	2.7	0.0	92.00	3.83	3.8	0.0
93.00	2.74	2.7	0.0		93.00	2.70	2.7	0.0	93.00	3.85	3.8	0.1
94.00	2.84	2.8	0.1		94.00	2.70	2.7	0.0	94.00	3.88	3.8	0.1
95.00	2.75	2.8	0.0		95.00	2.70	2.7	0.0	95.00	3.84	3.8	0.0
96.00	2.81	2.8	0.0		96.00	2.70	2.7	0.0	96.00	3.80	3.8	0.0
97.00	2.78	2.8	0.0		97.00	2.74	2.8	0.0	97.00	3.87	3.9	0.0
98.00	2.82	2.8	0.0		98.00	2.76	2.8	0.0	98.00	3.87	3.9	0.0
99.00	2.84	2.8	0.0		99.00	2.79	2.8	0.0	99.00	3.88	3.9	0.0
100.00	2.89	2.9	0.0		100.00	2.80	2.8	0.0	100.00	3.93	3.9	0.0
101.00	2.83	2.9	0.0		101.00	2.81	2.8	0.0	101.00	3.97	3.9	0.1
102.00	2.88	2.9	0.0		102.00	2.82	2.8	0.0	102.00	3.95	3.9	0.0
103.00	2.88	2.9	0.0		103.00	2.85	2.9	0.0	103.00	3.97	3.9	0.0
104.00	2.97	2.9	0.1		104.00	2.86	2.9	0.0	104.00	3.97	4.0	0.0
105.00	2.95	2.9	0.0		105.00	2.87	2.9	0.0	105.00	4.02	4.0	0.0
106.00	2.95	3.0	0.0		106.00	2.89	2.9	0.0	106.00	4.03	4.0	0.0
107.00	2.92	3.0	0.0		107.00	2.92	2.9	0.0	107.00	3.95	4.0	-0.1
108.00	2.97	3.0	0.0		108.00	2.94	2.9	0.0	108.00	4.06	4.0	0.0
109.00	2.96	3.0	0.0		109.00	2.94	2.9	0.0	109.00	3.97	4.0	-0.1
110.00	2.93	3.0	-0.1		110.00	2.97	3.0	0.0	110.00	4.08	4.1	0.0
111.00	2.95	3.0	-0.1		111.00	2.98	3.0	0.0	111.00	4.12	4.1	0.1
112.00	3.00	3.0	0.0		112.00	2.98	3.0	0.0	112.00	4.09	4.1	0.0
113.00	3.01	3.1	-0.1		113.00	2.98	3.0	0.0	113.00	4.13	4.1	0.0
114.00	3.05	3.1	0.0		114.00	3.00	3.0	0.0	114.00	4.12	4.1	0.0
115.00	3.14	3.1	0.0		115.00	3.03	3.0	0.0	115.00	4.14	4.1	0.0
116.00	3.07	3.1	0.0		116.00	3.04	3.1	0.0	116.00	4.15	4.1	0.0
117.00	3.08	3.1	0.0		117.00	3.06	3.1	0.0	117.00	4.18	4.2	0.0
118.00	3.16	3.1	0.0		118.00	3.08	3.1	0.0	118.00	4.18	4.2	0.0
119.00	3.14	3.2	0.0		119.00	3.10	3.1	0.0	119.00	4.20	4.2	0.0
120.00	3.20	3.2	0.0		120.00	3.12	3.1	0.0	120.00	4.14	4.2	-0.1
121.00	3.22	3.2	0.0		121.00	3.13	3.1	0.0	121.00	4.27	4.2	0.1
122.00	3.22	3.2	0.0		122.00	3.17	3.1	0.0	122.00	4.23	4.2	0.0
123.00	3.25	3.2	0.0		123.00	3.17	3.2	0.0	123.00	4.26	4.2	0.0
124.00	3.19	3.2	0.0		124.00	3.17	3.2	0.0	124.00	4.26	4.3	0.0
126.00	3.27	3.3	0.0		126.00	3.19	3.2	0.0	126.00	4.31	4.3	0.0
128.00	3.17	3.3	-0.1		128.00	3.23	3.2	0.0	128.00	4.23	4.3	-0.1
130.00	3.31	3.3	0.0		130.00	3.26	3.3	0.0	130.00	4.33	4.3	0.0
132.00	3.24	3.4	-0.1		132.00	3.29	3.3	0.0	132.00	4.37	4.4	0.0
134.00	3.38	3.4	0.0		134.00	3.33	3.3	0.0	134.00	4.41	4.4	0.0
136.00	3.41	3.4	0.0		136.00	3.37	3.4	0.0	136.00	4.44	4.4	0.0
138.00	3.51	3.5	0.1		138.00	3.38	3.4	0.0	138.00	4.43	4.4	0.0
140.00	3.51	3.5	0.0		140.00	3.42	3.4	0.0	140.00	4.48	4.5	0.0
142.00	3.53	3.5	0.0		142.00	3.43	3.4	0.0	142.00	4.46	4.5	0.0
144.00	3.56	3.5	0.0		144.00	3.47	3.5	0.0	144.00	4.53	4.5	0.0
146.00	3.52	3.6	0.0		146.00	3.50	3.5	0.0	146.00	4.56	4.6	0.0
148.00	3.61	3.6	0.0		148.00	3.53	3.5	0.0	148.00	4.58	4.6	0.0
150.00	3.67	3.6	0.0		150.00	3.55	3.6	0.0	150.00	4.64	4.6	0.0
152.00	3.60	3.7	-0.1		152.00	3.59	3.6	0.0	152.00	4.64	4.6	0.0
154.00	3.64	3.7	0.0		154.00	3.61	3.6	0.0	154.00	4.66	4.7	0.0
156.00	3.76	3.7	0.0		156.00	3.65	3.6	0.0	156.00	4.67	4.7	0.0
158.00	3.67	3.7	-0.1		158.00	3.67	3.7	0.0	158.00	4.71	4.7	0.0
160.00	3.82	3.8	0.0		160.00	3.69	3.7	0.0	160.00	4.74	4.7	0.0
162.00	3.77	3.8	0.0		162.00	3.73	3.7	0.0	162.00	4.78	4.8	0.0
164.00	3.84	3.8	0.0		164.00	3.75	3.8	0.0	164.00	4.76	4.8	0.0
166.00	3.85	3.9	0.0		166.00	3.78	3.8	0.0	166.00	4.82	4.8	0.0
168.00	3.99	3.9	0.1		168.00	3.81	3.8	0.0	168.00	4.84	4.8	0.0
170.00	3.90	3.9	0.0		170.00	3.83	3.8	0.0	170.00	4.88	4.9	0.0
172.00	3.98	3.9	0.0		172.00	3.86	3.9	0.0	172.00	4.86	4.9	0.0
174.00	3.93	4.0	0.0		174.00	3.90	3.9	0.0	174.00	4.92	4.9	0.0
176.00	3.97	4.0	0.0		176.00	3.92	3.9	0.0	176.00	4.96	5.0	0.0
178.00	3.94	4.0	-0.1		178.00	3.94	3.9	0.0	178.00	4.86	5.0	-0.1
180.00	3.98	4.1	-0.1		180.00	3.96	4.0	0.0	180.00	5.01	5.0	0.0
182.00	4.10	4.1	0.0		182.00	3.99	4.0	0.0	182.00	5.03	5.0	0.0
184.00	4.06	4.1	-0.1		184.00	4.04	4.0	0.0	184.00	5.07	5.1	0.0
186.00	4.14	4.1	0.0		186.00	4.05	4.1	0.0	186.00	5.09	5.1	0.0

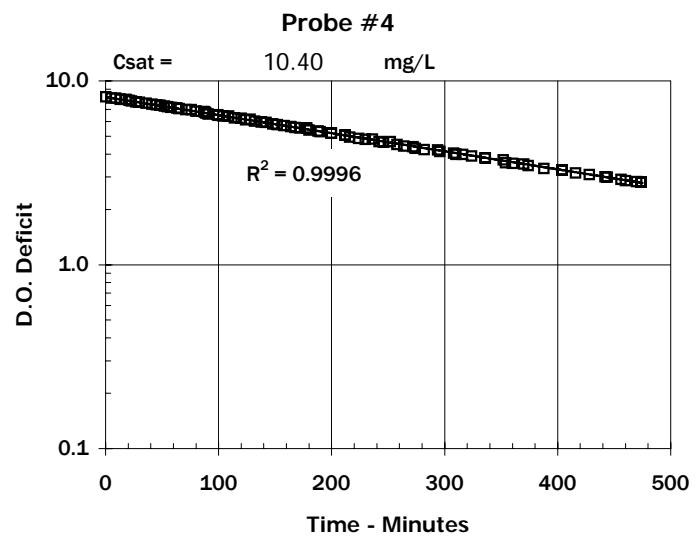
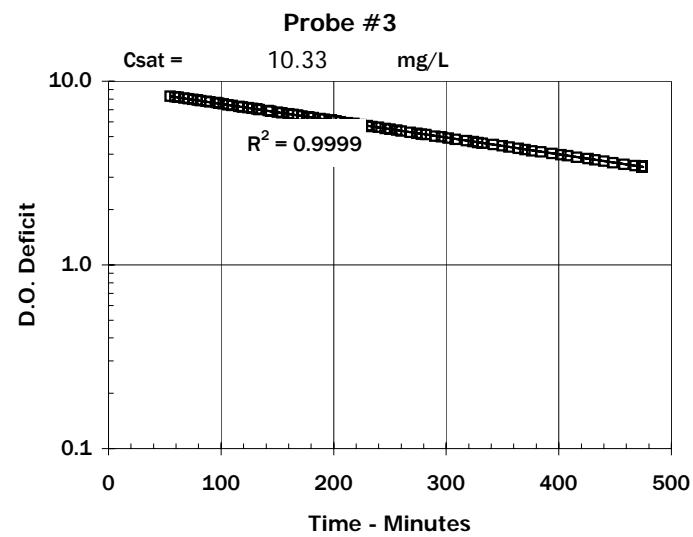
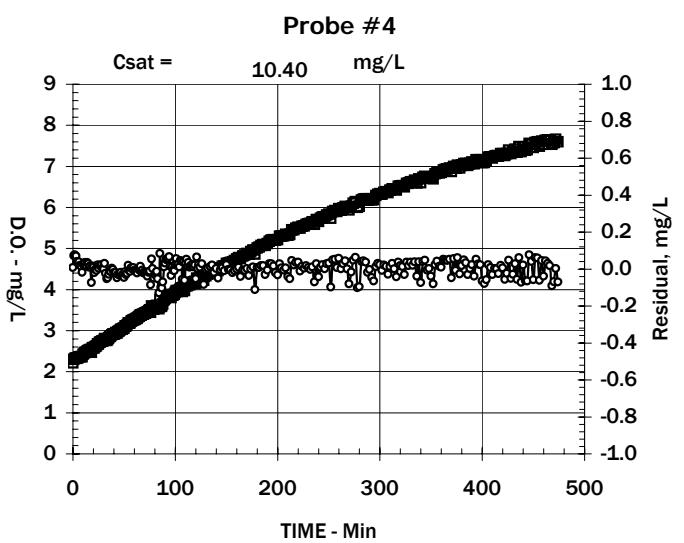
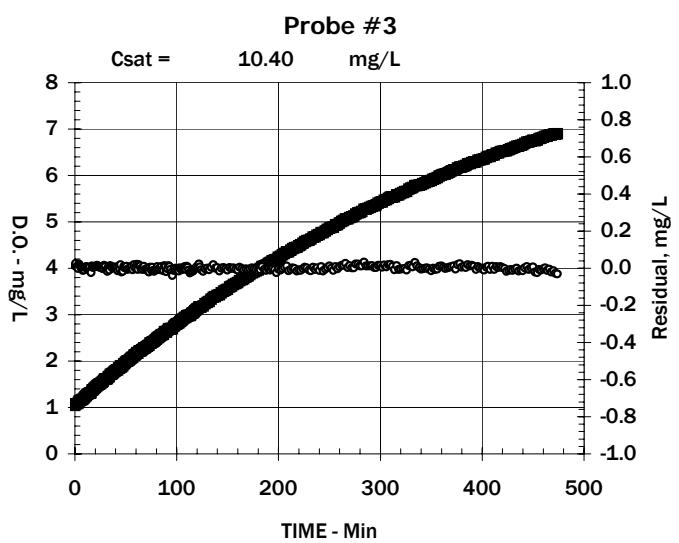
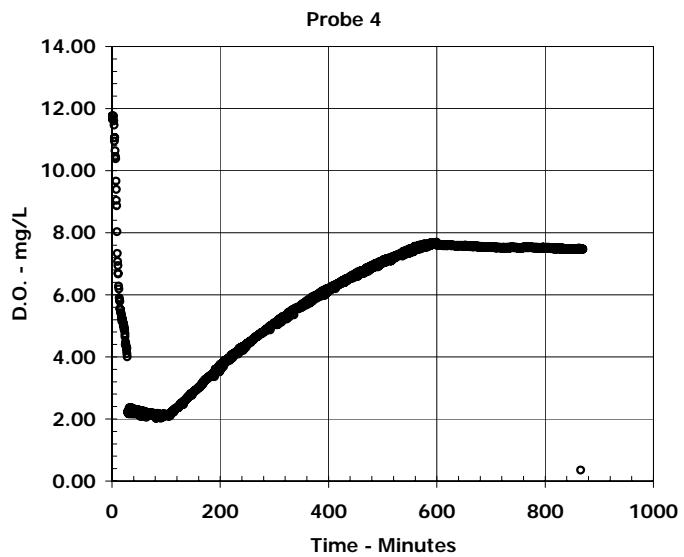
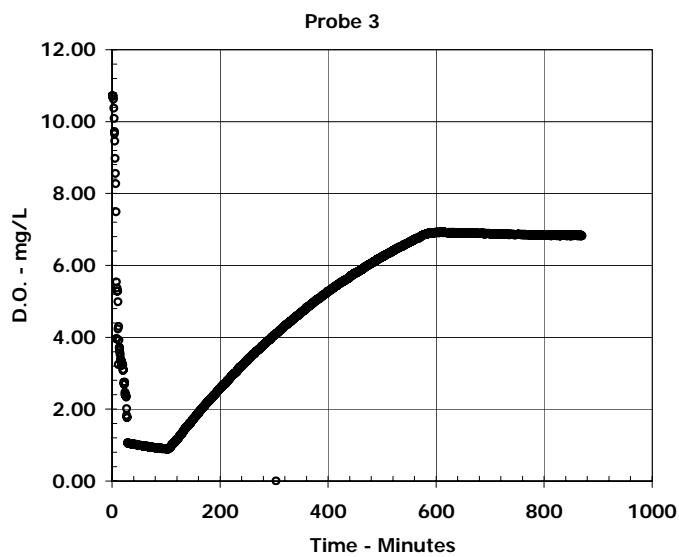
Pt. 1	est.	calc.	Pt. 2	Not Used	Pt. 3	est.	calc.	Pt. 4	est.	calc.		
CO	1.02	1.02			CO	1.03	1.03	CO	2.21	2.21		
Kla-in	0.13	0.13			Kla-in	0.13	0.13	Kla-in	0.14	0.14		
C*	10.40	10.40			C*	10.40	10.40	C*	10.40	10.40		
Sq.Dif.	1.2718				Sq.Dif.	0.0391		Sq.Dif.	0.4566			
Time	D.O.	D.O.calc	diff		Time	D.O.	D.O.calc	diff	Time	D.O.	D.O.calc	diff
188.00	4.17	4.2	0.0		188.00	4.07	4.1	0.0	188.00	5.07	5.1	0.0
190.00	4.12	4.2	-0.1		190.00	4.10	4.1	0.0	190.00	5.12	5.1	0.0
192.00	4.25	4.2	0.0		192.00	4.12	4.1	0.0	192.00	5.18	5.1	0.0
194.00	4.30	4.2	0.1		194.00	4.16	4.2	0.0	194.00	5.20	5.2	0.0
196.00	4.33	4.3	0.1		196.00	4.18	4.2	0.0	196.00	5.21	5.2	0.0
198.00	4.32	4.3	0.0		198.00	4.19	4.2	0.0	198.00	5.20	5.2	0.0
200.00	4.12	4.3	-0.2		200.00	4.23	4.2	0.0	200.00	5.21	5.2	0.0
202.00	4.25	4.4	-0.1		202.00	4.25	4.3	0.0	202.00	5.30	5.3	0.0
204.00	4.45	4.4	0.1		204.00	4.29	4.3	0.0	204.00	5.30	5.3	0.0
206.00	4.43	4.4	0.0		206.00	4.32	4.3	0.0	206.00	5.31	5.3	0.0
208.00	4.38	4.4	0.0		208.00	4.35	4.3	0.0	208.00	5.35	5.3	0.0
210.00	4.48	4.5	0.0		210.00	4.35	4.4	0.0	210.00	5.32	5.4	0.0
212.00	4.36	4.5	-0.1		212.00	4.39	4.4	0.0	212.00	5.33	5.4	-0.1
214.00	4.55	4.5	0.0		214.00	4.42	4.4	0.0	214.00	5.45	5.4	0.0
216.00	4.49	4.5	0.0		216.00	4.44	4.4	0.0	216.00	5.45	5.4	0.0
218.00	4.54	4.6	0.0		218.00	4.45	4.5	0.0	218.00	5.49	5.5	0.0
220.00	4.59	4.6	0.0		220.00	4.48	4.5	0.0	220.00	5.51	5.5	0.0
222.00	4.73	4.6	0.1		222.00	4.50	4.5	0.0	222.00	5.49	5.5	0.0
224.00	4.67	4.6	0.0		224.00	4.54	4.5	0.0	224.00	5.54	5.5	0.0
226.00	4.60	4.7	-0.1		226.00	4.57	4.6	0.0	226.00	5.55	5.5	0.0
228.00	4.66	4.7	0.0		228.00	4.59	4.6	0.0	228.00	5.59	5.6	0.0
230.00	4.81	4.7	0.1		230.00	4.60	4.6	0.0	230.00	5.60	5.6	0.0
232.00	4.75	4.7	0.0		232.00	4.62	4.6	0.0	232.00	5.61	5.6	0.0
234.00	4.72	4.8	0.0		234.00	4.67	4.7	0.0	234.00	5.65	5.6	0.0
236.00	4.85	4.8	0.1		236.00	4.68	4.7	0.0	236.00	5.59	5.7	-0.1
238.00	4.87	4.8	0.1		238.00	4.71	4.7	0.0	238.00	5.71	5.7	0.0
240.00	4.86	4.8	0.0		240.00	4.72	4.7	0.0	240.00	5.66	5.7	0.0
242.00	4.89	4.9	0.0		242.00	4.77	4.8	0.0	242.00	5.73	5.7	0.0
244.00	4.84	4.9	0.0		244.00	4.77	4.8	0.0	244.00	5.77	5.7	0.0
246.00	4.89	4.9	0.0		246.00	4.80	4.8	0.0	246.00	5.77	5.8	0.0
248.00	4.92	4.9	0.0		248.00	4.83	4.8	0.0	248.00	5.82	5.8	0.0
250.00	4.97	5.0	0.0		250.00	4.86	4.9	0.0	250.00	5.84	5.8	0.0
252.00	5.04	5.0	0.1		252.00	4.87	4.9	0.0	252.00	5.73	5.8	-0.1
254.00	5.04	5.0	0.0		254.00	4.89	4.9	0.0	254.00	5.90	5.9	0.0
256.00	5.04	5.0	0.0		256.00	4.93	4.9	0.0	256.00	5.92	5.9	0.1
258.00	5.07	5.0	0.0		258.00	4.94	4.9	0.0	258.00	5.90	5.9	0.0
260.00	5.14	5.1	0.1		260.00	4.97	5.0	0.0	260.00	5.97	5.9	0.1
262.00	5.09	5.1	0.0		262.00	5.01	5.0	0.0	262.00	5.94	5.9	0.0
264.00	5.13	5.1	0.0		264.00	5.03	5.0	0.0	264.00	5.98	6.0	0.0
266.00	5.18	5.1	0.0		266.00	5.06	5.0	0.0	266.00	6.02	6.0	0.0
268.00	5.21	5.2	0.1		268.00	5.06	5.1	0.0	268.00	6.00	6.0	0.0
270.00	5.11	5.2	-0.1		270.00	5.09	5.1	0.0	270.00	5.94	6.0	-0.1
272.00	5.14	5.2	-0.1		272.00	5.10	5.1	0.0	272.00	6.02	6.0	0.0
274.00	5.22	5.2	0.0		274.00	5.13	5.1	0.0	274.00	6.10	6.1	0.0
276.00	5.22	5.3	0.0		276.00	5.17	5.1	0.0	276.00	6.14	6.1	0.1
278.00	5.26	5.3	0.0		278.00	5.19	5.2	0.0	278.00	6.00	6.1	-0.1
280.00	5.26	5.3	0.0		280.00	5.20	5.2	0.0	280.00	6.02	6.1	-0.1
282.00	5.38	5.3	0.1		282.00	5.22	5.2	0.0	282.00	6.18	6.1	0.0
284.00	5.36	5.3	0.0		284.00	5.27	5.2	0.0	284.00	6.20	6.2	0.0
286.00	5.40	5.4	0.0		286.00	5.27	5.3	0.0	286.00	6.21	6.2	0.0
288.00	5.39	5.4	0.0		288.00	5.29	5.3	0.0	288.00	6.18	6.2	0.0
290.00	5.40	5.4	0.0		290.00	5.31	5.3	0.0	290.00	6.21	6.2	0.0
292.00	5.42	5.4	0.0		292.00	5.33	5.3	0.0	292.00	6.19	6.2	0.0
294.00	5.54	5.4	0.1		294.00	5.34	5.3	0.0	294.00	6.19	6.3	-0.1
296.00	5.43	5.5	0.0		296.00	5.36	5.4	0.0	296.00	6.29	6.3	0.0
298.00	5.41	5.5	-0.1		298.00	5.40	5.4	0.0	298.00	6.32	6.3	0.0
300.00	5.46	5.5	0.0		300.00	5.42	5.4	0.0	300.00	6.33	6.3	0.0
302.00	5.62	5.5	0.1		302.00	5.43	5.4	0.0	302.00	6.32	6.3	0.0
304.00	5.68	5.6	0.1		304.00	5.46	5.4	0.0	304.00	6.37	6.3	0.0
306.00	5.66	5.6	0.1		306.00	5.47	5.5	0.0	306.00	6.38	6.4	0.0
308.00	5.80	5.6	0.2		308.00	5.51	5.5	0.0	308.00	6.36	6.4	0.0
310.00	5.67	5.6	0.1		310.00	5.53	5.5	0.0	310.00	6.42	6.4	0.0
312.00	5.58	5.6	-0.1		312.00	5.54	5.5	0.0	312.00	6.45	6.4	0.0
314.00	5.66	5.7	0.0		314.00	5.54	5.5	0.0	314.00	6.44	6.4	0.0
316.00	5.75	5.7	0.1		316.00	5.58	5.6	0.0	316.00	6.42	6.5	0.0
318.00	5.55	5.7	-0.1		318.00	5.58	5.6	0.0	318.00	6.51	6.5	0.0
320.00	5.72	5.7	0.0		320.00	5.60	5.6	0.0	320.00	6.51	6.5	0.0
322.00	5.82	5.7	0.1		322.00	5.63	5.6	0.0	322.00	6.53	6.5	0.0
324.00	5.71	5.8	0.0		324.00	5.65	5.6	0.0	324.00	6.50	6.5	0.0
326.00	5.69	5.8	-0.1		326.00	5.66	5.7	0.0	326.00	6.59	6.5	0.0
328.00	5.81	5.8	0.0		328.00	5.70	5.7	0.0	328.00	6.59	6.6	0.0
330.00	5.82	5.8	0.0		330.00	5.72	5.7	0.0	330.00	6.62	6.6	0.0
332.00	5.84	5.8	0.0		332.00	5.73	5.7	0.0	332.00	6.62	6.6	0.0
334.00	5.99	5.9	0.1		334.00	5.78	5.7	0.0	334.00	6.66	6.6	0.0
336.00	5.97	5.9	0.1		336.00	5.78	5.8	0.0	336.00	6.60	6.6	0.0
338.00	5.99	5.9	0.1		338.00	5.79	5.8	0.0	338.00	6.69	6.7	0.0
340.00	5.94	5.9	0.0		340.00	5.80	5.8	0.0	340.00	6.60	6.7	-0.1
342.00	5.83	5.9	-0.1		342.00	5.82	5.8	0.0	342.00	6.73	6.7	0.0

Pt. 1	est.	calc.	Pt. 2	Not Used	Pt. 3	est.	calc.	Pt. 4	est.	calc.		
CO	1.02	1.02			CO	1.03	1.03	CO	2.21	2.21		
Kla-in	0.13	0.13			Kla-in	0.13	0.13	Kla-in	0.14	0.14		
C*	10.40	10.40			C*	10.40	10.40	C*	10.40	10.40		
Sq.Dif.	1.2718				Sq.Dif.	0.0391		Sq.Dif.	0.4566			
Time	D.O.	D.O.calc	diff		Time	D.O.	D.O.calc	diff	Time	D.O.	D.O.calc	diff
344.00	5.89	6.0	-0.1		344.00	5.84	5.8	0.0	344.00	6.75	6.7	0.0
346.00	5.91	6.0	-0.1		346.00	5.87	5.9	0.0	346.00	6.72	6.7	0.0
348.00	5.94	6.0	-0.1		348.00	5.88	5.9	0.0	348.00	6.74	6.7	0.0
350.00	5.82	6.0	-0.2		350.00	5.89	5.9	0.0	350.00	6.72	6.8	0.0
352.00	6.06	6.0	0.0		352.00	5.92	5.9	0.0	352.00	6.69	6.8	-0.1
354.00	6.08	6.1	0.0		354.00	5.93	5.9	0.0	354.00	6.82	6.8	0.0
356.00	6.07	6.1	0.0		356.00	5.95	6.0	0.0	356.00	6.85	6.8	0.0
358.00	6.14	6.1	0.0		358.00	5.98	6.0	0.0	358.00	6.84	6.8	0.0
360.00	6.01	6.1	-0.1		360.00	6.01	6.0	0.0	360.00	6.85	6.8	0.0
362.00	6.17	6.1	0.0		362.00	6.02	6.0	0.0	362.00	6.91	6.9	0.1
364.00	6.11	6.1	0.0		364.00	6.03	6.0	0.0	364.00	6.92	6.9	0.0
366.00	6.13	6.2	0.0		366.00	6.05	6.0	0.0	366.00	6.94	6.9	0.0
368.00	6.26	6.2	0.1		368.00	6.07	6.1	0.0	368.00	6.96	6.9	0.1
370.00	6.33	6.2	0.1		370.00	6.09	6.1	0.0	370.00	6.88	6.9	0.0
372.00	6.27	6.2	0.1		372.00	6.12	6.1	0.0	372.00	7.00	6.9	0.1
374.00	6.23	6.2	0.0		374.00	6.12	6.1	0.0	374.00	6.95	7.0	0.0
376.00	6.28	6.3	0.0		376.00	6.16	6.1	0.0	376.00	7.03	7.0	0.1
378.00	6.42	6.3	0.1		378.00	6.18	6.2	0.0	378.00	6.96	7.0	0.0
380.00	6.40	6.3	0.1		380.00	6.18	6.2	0.0	380.00	7.02	7.0	0.0
382.00	6.35	6.3	0.0		382.00	6.20	6.2	0.0	382.00	7.07	7.0	0.0
384.00	6.31	6.3	0.0		384.00	6.21	6.2	0.0	384.00	7.07	7.0	0.0
386.00	6.42	6.3	0.1		386.00	6.25	6.2	0.0	386.00	7.02	7.0	0.0
388.00	6.14	6.4	-0.2		388.00	6.26	6.2	0.0	388.00	7.07	7.1	0.0
390.00	6.39	6.4	0.0		390.00	6.28	6.3	0.0	390.00	7.10	7.1	0.0
392.00	6.37	6.4	0.0		392.00	6.29	6.3	0.0	392.00	7.06	7.1	0.0
394.00	6.45	6.4	0.0		394.00	6.29	6.3	0.0	394.00	7.16	7.1	0.1
396.00	6.55	6.4	0.1		396.00	6.32	6.3	0.0	396.00	7.15	7.1	0.0
398.00	6.18	6.4	-0.3		398.00	6.33	6.3	0.0	398.00	7.16	7.1	0.0
400.00	6.37	6.5	-0.1		400.00	6.34	6.3	0.0	400.00	7.09	7.2	-0.1
402.00	6.58	6.5	0.1		402.00	6.35	6.4	0.0	402.00	7.09	7.2	-0.1
404.00	6.51	6.5	0.0		404.00	6.39	6.4	0.0	404.00	7.13	7.2	-0.1
406.00	6.51	6.5	0.0		406.00	6.41	6.4	0.0	406.00	7.22	7.2	0.0
408.00	6.68	6.5	0.2		408.00	6.41	6.4	0.0	408.00	7.22	7.2	0.0
410.00	6.61	6.6	0.1		410.00	6.44	6.4	0.0	410.00	7.20	7.2	0.0
412.00	6.53	6.6	0.0		412.00	6.44	6.4	0.0	412.00	7.25	7.2	0.0
414.00	6.53	6.6	-0.1		414.00	6.47	6.5	0.0	414.00	7.26	7.3	0.0
416.00	6.53	6.6	-0.1		416.00	6.49	6.5	0.0	416.00	7.25	7.3	0.0
418.00	6.74	6.6	0.1		418.00	6.51	6.5	0.0	418.00	7.31	7.3	0.0
420.00	6.55	6.6	-0.1		420.00	6.52	6.5	0.0	420.00	7.31	7.3	0.0
422.00	6.62	6.6	0.0		422.00	6.53	6.5	0.0	422.00	7.26	7.3	-0.1
424.00	6.75	6.7	0.1		424.00	6.53	6.5	0.0	424.00	7.31	7.3	0.0
426.00	6.79	6.7	0.1		426.00	6.55	6.6	0.0	426.00	7.39	7.3	0.0
428.00	6.63	6.7	-0.1		428.00	6.57	6.6	0.0	428.00	7.31	7.4	-0.1
430.00	6.82	6.7	0.1		430.00	6.58	6.6	0.0	430.00	7.34	7.4	0.0
432.00	6.81	6.7	0.1		432.00	6.61	6.6	0.0	432.00	7.42	7.4	0.0
434.00	6.70	6.7	0.0		434.00	6.63	6.6	0.0	434.00	7.34	7.4	-0.1
436.00	6.59	6.8	-0.2		436.00	6.63	6.6	0.0	436.00	7.48	7.4	0.1
438.00	6.80	6.8	0.0		438.00	6.65	6.7	0.0	438.00	7.36	7.4	-0.1
440.00	6.85	6.8	0.1		440.00	6.66	6.7	0.0	440.00	7.47	7.4	0.0
442.00	6.94	6.8	0.1		442.00	6.69	6.7	0.0	442.00	7.39	7.5	-0.1
444.00	6.94	6.8	0.1		444.00	6.71	6.7	0.0	444.00	7.41	7.5	-0.1
446.00	7.04	6.8	0.2		446.00	6.71	6.7	0.0	446.00	7.56	7.5	0.1
448.00	6.89	6.9	0.0		448.00	6.74	6.7	0.0	448.00	7.54	7.5	0.0
450.00	6.72	6.9	-0.1		450.00	6.76	6.8	0.0	450.00	7.45	7.5	-0.1
452.00	6.73	6.9	-0.2		452.00	6.75	6.8	0.0	452.00	7.59	7.5	0.1
454.00	6.91	6.9	0.0		454.00	6.76	6.8	0.0	454.00	7.60	7.5	0.1
456.00	6.90	6.9	0.0		456.00	6.79	6.8	0.0	456.00	7.49	7.6	-0.1
458.00	6.98	6.9	0.0		458.00	6.80	6.8	0.0	458.00	7.61	7.6	0.0
460.00	6.97	6.9	0.0		460.00	6.82	6.8	0.0	460.00	7.54	7.6	0.0
462.00	6.92	7.0	0.0		462.00	6.84	6.8	0.0	462.00	7.63	7.6	0.0
464.00	6.93	7.0	-0.1		464.00	6.84	6.9	0.0	464.00	7.63	7.6	0.0
466.00	7.16	7.0	0.2		466.00	6.87	6.9	0.0	466.00	7.63	7.6	0.0
468.00	6.90	7.0	-0.1		468.00	6.87	6.9	0.0	468.00	7.54	7.6	-0.1
470.00	6.87	7.0	-0.2		470.00	6.89	6.9	0.0	470.00	7.57	7.6	-0.1
472.00	6.81	7.0	-0.2		472.00	6.89	6.9	0.0	472.00	7.66	7.7	0.0
474.00	6.87	7.1	-0.2		474.00	6.90	6.9	0.0	474.00	7.60	7.7	-0.1

Probe 1			Probe 2			Probe 3			Probe 4		
Lower	9.80%	Upper	Lower	10.04%	Upper	Lower	66.32%	Upper	21.30%	Upper	73.61%
Value	Abs.Un.	%LSE	Value	Abs.Un.	%LSE	Value	Abs.Un.	%LSE	Value	Abs.Un.	%LSE
C*	10.403	0.100	0.965	C*	10.403	0.019	0.181	C*	10.403	0.053	0.511
CO	1.023	0.011	1.030	CO	1.032	0.002	0.178	CO	2.208	0.006	0.288
KLaT	0.130	0.000	1.693	KLaT	0.126	0.000	0.314	KLaT	0.139	0.000	1.054
Error	0.065		Error	0.011		Error	0.039				
PROJECT:	PHI Unit Alone - Pumping										
DATE:	11/7/2006										
RUN:	1.00										



Project: PHi Unit Alone - Pumping
 Date: Nov 07, 2006
 Run: 1



Project: PHi Unit Alone - Pumping
 Date: Nov 07, 2006
 Run: 1

**AIR FLOW RATE DETERMINATION
ANR 73 COMMERCIAL ANNULAR**

PROJECT : PHi Unit Alone - Pumping

$$\text{SCFM} = C'' \frac{[BP + LP]}{[LT + 460]}$$

$$C' = Fna * k * D^2 * Fra * Fpb * Ftb * Fg * Fpv * Faa * Fl * Fm * Ya$$

C'' = C' VALUE CORRECTED FOR HUMIDITY

RUN # 1
DATE Nov-06

OPERATING CONDITIONS

ANNULAR TYPE		AWR-73	
BAROMETRIC PRESSURE	* BP	14.18	PSIA
LINE PRESSURE	* LP	45.02	PSIG
LINE TEMPERATURE	* LT	57	°F
DIFFERENTIAL PRESSURE	* ^H	0.00	In. H2O
RELATIVE HUMIDITY	* RH	68%	%
AMBIENT TEMPERATURE	*	15.5	57 °F
PIPE INSIDE DIAMETER	* D	4.026	In.
UNITS CONVERSION FACTOR	Fna	128.520	
ANNULAR FLOW COEFFICIENT	k	0.746	
SQUARE OF PIPE ID	D^2	16.209	
BASE PRESSURE		14.700	PSIA
BASE PRESSURE FACTOR	Fpb	1.002	
BASE TEMPERATURE		68.000	°F
BASE TEMPERATURE FACTOR	Ftb	1.015	
THERMAL EXPANSION FACTOR	Faa	1.001	
MANOMETER LOCATION FACTOR	Fl	1.000	
HG MANOMETER CORRECTION FACTOR	Fm	1.000	
REYNOLD NUMBER	Rd	10,210.3	
FLOWING VISCOSITY	vis	0.018	cP
REYNOLD NUMBER FACTOR	Fra	0.965	
SPECIFIC GRAVITY	g	1.000	
SPECIFIC GRAVITY FACTOR	Fg	1.000	
SUPERCOMPRESSIBILITY	Z	0.998	
SUPERCOMPRESSIBILITY FACTOR	Fpv	1.001	
GAS EXPANSION FACTOR	Ya	1.000	
SCFM UNCORRECTED FOR HUMIDITY	SCFM	25.2	
C'		1,527.21	
VAPOR PRESSURE OF WATER AMB. TEMP.	VP	0.231	
ACTUAL CUBIC FEET PER MINUTE	ACFM	6.1	69.2
HUMIDITY CORRECTED STANDARD AIR FLOW	SCFM	25.1	@68°F, 36% RH, 14.7 PSIA
INLET CUBIC FEET PER MINUTE	ICFM	25.5	
C"		1,522.09	

FORMULAS AND FACTORS DERIVED FROM: L.K.Spink; "Principles and Practice of FLOW METER ENGINEERING"; Ninth Ed., Nov 1975; The FOXBORO CO., Foxboro, Mass.
"ORIFICE FLOW METER"; THE BRISTOL COMPANY; Waterbury, Conn.

"ANNULAR FLOW HANDBOOK"; August 1978; DIETERICH STANDARD CORPORATION; Boulder, Co.

HUMIDITY CORRECTED AIR FLOW DETERMINED per: "ASCE STANDARD Measurement of Oxygen Transfer in Clean Water"; ANNEX A; July 1984; American Society of Civil Engineers

ASCE OXYGEN TRANSFER DETERMINATION

PROJECT: Phi - Membrane Tube Diffusers Only	599 Waldron Rd.			
DATE: 8-Nov-06	LaVergne, TN 37086			
RUN: 2	615/793-7547			
	FAX 615/793/5070			
	Initial	Mid Point	Final	
Barometric Pres. (PSIA) (mm Hg)	14.189 733.80	14.189 733.80	14.189 733.80	C' Air Flow Device 1 (Annubar) 1,519.15 Air Flow Device 1 (SCFM) 41.41
Ambient Temperature (°F)	61.00	61.50	63.00	C' Air Flow Device 2 (Orifice) 133.92 Air Flow Device 2 (SCFM) 41.16
Relative Humidity (%)	69%	69%	67%	
Line Pressure (PSIG) (In. Hg)	8.866 18.05	8.866 18.05	8.866 18.05	
Line Temperature (°F)	124.00	131.00	134.00	
ΔH Air Flow Dev. 1 (Annubar)	0.019	0.019	0.019	Average Air Flow (SCFM) 41.28
ΔH Air Flow Dev. 2 (Orifice)	2.450	2.400	2.400	Effective Depth Correction (f) 0.33
ΔH Air Flow Dev. 3 (Annubar)	NA	NA	NA	Headloss (In. H2O) 20.42
ΔH Air Flow Dev. 4 (Annubar)	NA	NA	NA	C* (mg/l) 11.66
Water Temp. (°C)	14.60	14.61	14.62	CsmT (Standard Methods, mg/l) 10.17
Orifice Diameter (in)		1.349		C* ₂₀ Standard Conditions 10.74
Number Of Aeration Devices		28		Tank Volume (Ft ³) 6,840.6
Side Water Depth (ft)		19.75	(6.00 m)	(Gallons) 51,171.4
Air Release Depth (ft)		18.75	(5.70 m)	(m ³) 193.7
Tank Length (ft)		0.00	(0.00 m)	(Million Pounds) 0.427
Tank Width (ft)		0.00	(0.00 m)	
Tank Diameter (ft)		21.00	(6.38 m)	#Na ₂ SO ₃ @ 160% Stoichiometric 63
Gear Reducer or Belt Efficiency		100.0%		Cobalt Concen. (mg/l) 0.100
Motor Efficiency		89.0%		Grams Cobalt Chloride 79.9
Total HP _{wire} av.		2.76	(2.06 kw)	Total HP _{motor} av. 2.46
				TDS (mg/L) 452.00

NON-LINEAR REGRESSION RESULTS

Probe	K _{LAT}	K _{La20}	SOTR	SOTR/Dev	SOTE	SAE _{wire}	C*	Std. Err.
1	2.13	2.42	11.28	0.40	26.37	4.09	11.79	0.0855
2	2.14	2.43	11.22	0.40	26.23	4.07	11.66	0.0342
3	2.14	2.44	11.34	0.40	26.51	4.11	11.77	0.0240
4	2.15	2.44	11.05	0.39	25.83	4.00	11.43	0.0298
avg.	2.14	2.43	11.22	0.40	26.23	4.07	11.66	0.0434
Avg	2.14	2.43	11.28	0.40	26.36	4.09	11.72	Exclude Max&Min
TDS	2.26	2.57	11.83	0.42	27.66	4.29	11.66	1.48%
<i>Corrected</i>	/hr	/hr	#O2/hr		%	#O2/hr-WHP		

OXYGEN TRANSFER

Total SCFM:	41.3	66.374 :Nm ³ /Hr	19.484 L/s	#O2/Hr:	11.83	5.366 :KgO2/Hr
SCFM/Diff.:	1.47	2.371 :Nm ³ /hr/Diff		#O2/Hr/Diff.:	0.42	0.192 :KgO2/Hr/Diff.
SCFM/KCF:	6.0	0.343 :Nm ³ /hr/m ³		#O2/Day:	283.9	128.8 :KgO2/Day
Total ICFM:	48.1	22.72 L/s		#O2/Day/1000 Ft ³ :	42	0.66 :KgO2/Day/m ³

LINEAR REGRESSION RESULTS

Probe	K _{LAT}	K _{La20}	SOTR	SOTR/Dev	SOTE	SAE _{wire}	C*	Corr. Coeff.
1	2.17	2.46	11.30	0.40	26.43	4.10	11.61	0.9983
2	2.20	2.50	11.42	0.41	26.71	4.14	11.55	0.9994
3	2.20	2.50	11.54	0.41	26.98	4.18	11.68	0.9999
4	2.13	2.42	10.94	0.39	25.58	3.97	11.43	0.9995
avg.	2.17	2.47	11.30	0.40	26.42	4.10	11.57	0.9993
Avg	2.18	2.48	11.35	0.41	26.55	4.12	11.58	Exclude Max&Min
TDS	2.29	2.60	11.91	0.43	27.86	4.32	11.57	
<i>Corrected</i>	/hr	/hr	#O2/hr		%	#O2/hr-HPw		

EUROPEAN STANDARD

Probe	K _{LAT}	K _{La10}	SOTR	SOTR/Dev	SAE	C*
1	2.15	1.93	5.09	0.18	2.48	11.79
2	2.17	1.95	5.09	0.18	2.48	11.66
3	2.17	1.96	5.14	0.18	2.50	11.77
4	2.14	1.93	4.92	0.18	2.39	11.43
NA	NA	NA	NA	NA	NA	NA
NA	NA	NA	NA	NA	NA	NA
avg.	2.16	1.94	5.06	0.18	2.46	11.66
Avg	2.16	1.94	5.09	0.18	2.48	11.72
TDS	2.27	2.05	5.34	0.19	2.59	11.66
<i>Corrected</i>	/hr	/hr	kg O ₂ /hr		kg O ₂ /hr-kw	mg/L

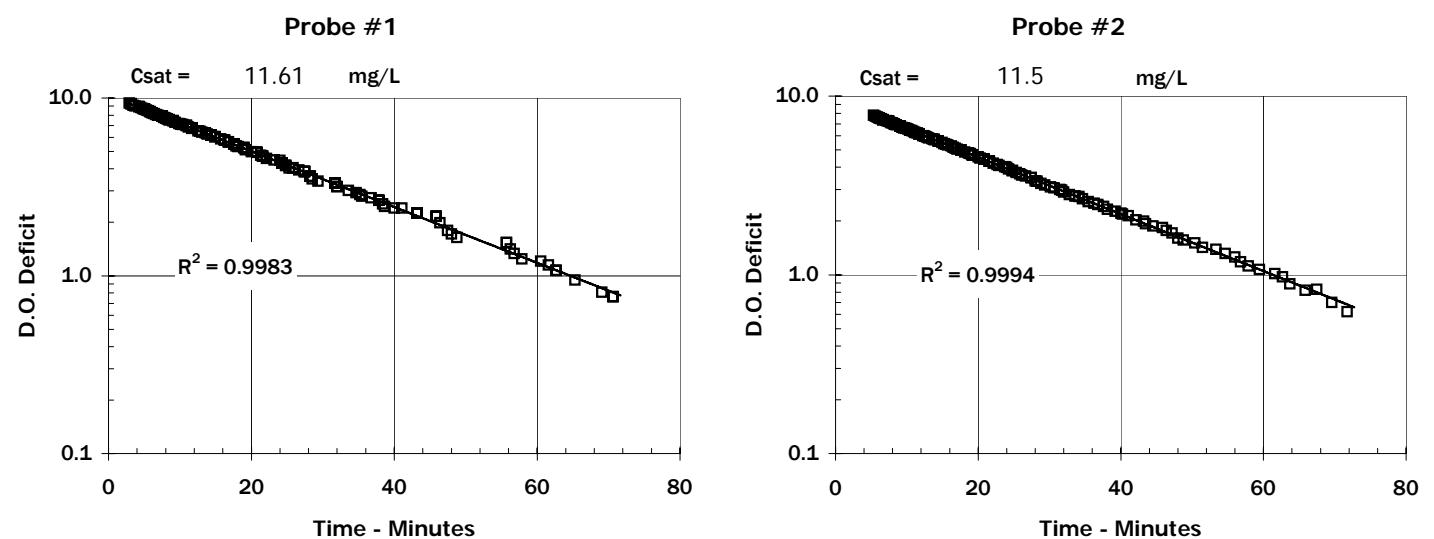
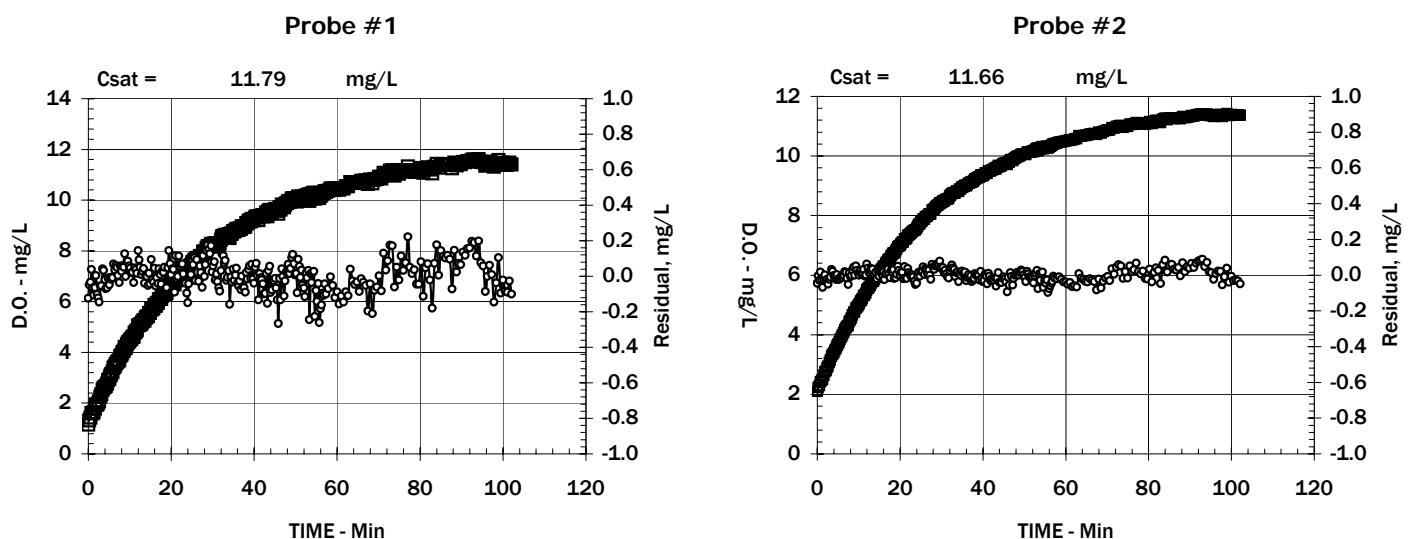
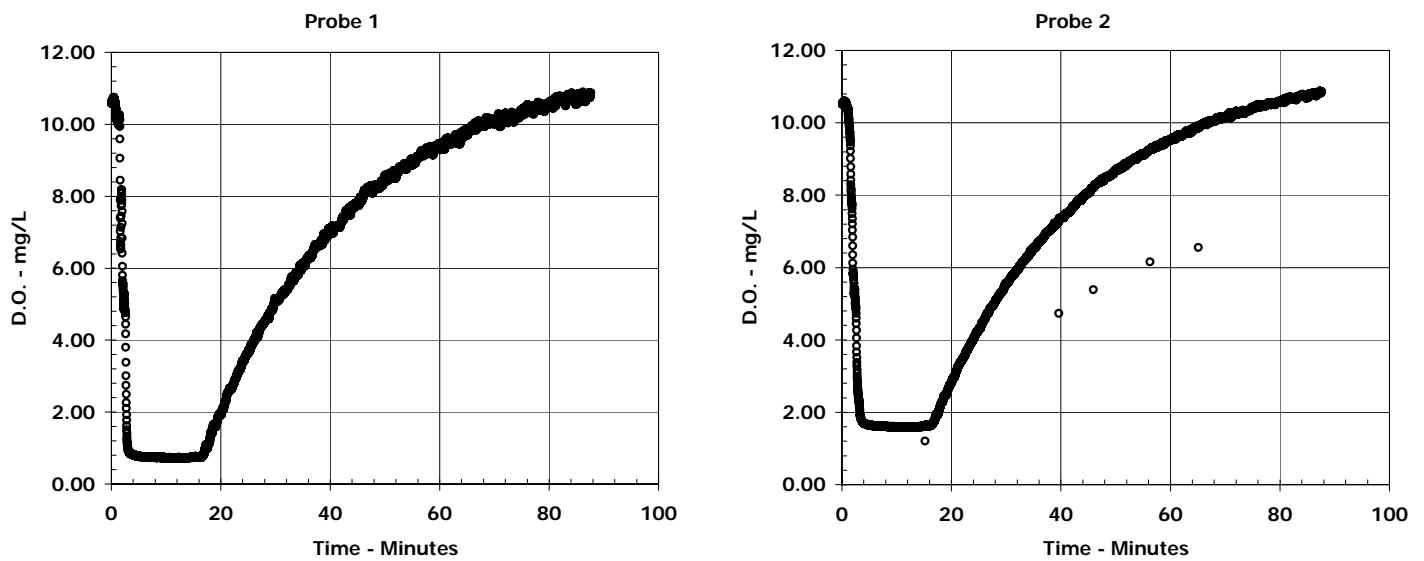
Pt. 1	est.	calc.	Pt. 2	est.	calc.	Pt. 3	est.	calc.	Pt. 4	est.	calc.
CO	1.27	1.27	CO	2.13	2.13	CO	1.80	1.80	CO	3.34	3.34
Kla-in	2.13	2.13	Kla-in	2.14	2.14	Kla-in	2.14	2.14	Kla-in	2.15	2.15
C*	11.79	11.79	C*	11.66	11.66	C*	11.77	11.77	C*	11.43	11.43
Sq.Dif.	2.1730	Sq.Dif.	0.3471	Sq.Dif.	0.1710 <th>Sq.Dif.</th> <td>0.2643</td> <th>Sq.Dif.</th> <td>0.2643</td> <th>Sq.Dif.</th> <td>0.2643</td>	Sq.Dif.	0.2643	Sq.Dif.	0.2643	Sq.Dif.	0.2643
Time	D.O.	D.O.calc	diff	Time	D.O.	D.O.calc	diff	Time	D.O.	D.O.calc	diff
0.00	1.14	1.3	-0.1	0.00	2.09	2.1	0.0	0.00	1.75	1.8	-0.1
0.26	1.31	1.4	0.0	0.26	2.22	2.2	0.0	0.26	1.90	1.9	0.0
0.53	1.43	1.5	0.0	0.53	2.28	2.3	0.0	0.53	1.98	2.0	0.0
0.80	1.60	1.6	0.0	0.80	2.42	2.4	0.0	0.80	2.09	2.1	0.0
1.06	1.59	1.7	-0.1	1.06	2.46	2.5	0.0	1.06	2.18	2.2	0.0
1.33	1.64	1.8	-0.1	1.33	2.51	2.6	-0.1	1.33	2.19	2.3	-0.1
1.60	1.78	1.8	-0.1	1.60	2.63	2.7	0.0	1.60	2.35	2.4	0.0
1.86	1.94	1.9	0.0	1.86	2.75	2.7	0.0	1.86	2.52	2.4	0.1
2.13	1.93	2.0	-0.1	2.13	2.80	2.8	0.0	2.13	2.57	2.5	0.0
2.39	2.00	2.1	-0.1	2.39	2.89	2.9	0.0	2.39	2.65	2.6	0.0
2.66	2.07	2.2	-0.1	2.66	2.95	3.0	-0.1	2.66	2.71	2.7	0.0
2.93	2.25	2.3	-0.1	2.93	3.06	3.1	0.0	2.93	2.77	2.8	0.0
3.20	2.34	2.4	-0.1	3.20	3.152	3.2	0.0	3.20	2.89	2.9	0.0
3.46	2.52	2.5	0.0	3.46	3.274	3.2	0.0	3.46	3.00	3.0	0.0
3.73	2.60	2.6	0.0	3.73	3.342	3.3	0.0	3.73	3.08	3.0	0.0
4.00	2.64	2.7	0.0	4.00	3.399	3.4	0.0	4.00	3.14	3.1	0.0
4.26	2.67	2.7	-0.1	4.26	3.468	3.5	0.0	4.26	3.23	3.2	0.0
4.53	2.76	2.8	-0.1	4.53	3.532	3.6	0.0	4.53	3.29	3.3	0.0
4.79	2.90	2.9	0.0	4.79	3.64	3.6	0.0	4.79	3.36	3.4	0.0
5.06	2.95	3.0	0.0	5.06	3.68	3.7	0.0	5.06	3.45	3.5	0.0
5.33	3.07	3.1	0.0	5.33	3.76	3.8	0.0	5.33	3.49	3.5	0.0
5.59	3.14	3.2	0.0	5.59	3.84	3.9	0.0	5.59	3.56	3.6	0.0
5.86	3.23	3.2	0.0	5.86	3.92	3.9	0.0	5.86	3.69	3.7	0.0
6.13	3.39	3.3	0.1	6.13	3.99	4.0	0.0	6.13	3.70	3.8	-0.1
6.40	3.44	3.4	0.0	6.40	4.08	4.1	0.0	6.40	3.83	3.8	0.0
6.66	3.54	3.5	0.1	6.66	4.17	4.2	0.0	6.66	3.91	3.9	0.0
6.93	3.61	3.6	0.0	6.93	4.24	4.2	0.0	6.93	3.99	4.0	0.0
7.20	3.64	3.6	0.0	7.20	4.27	4.3	0.0	7.20	4.04	4.1	0.0
7.46	3.68	3.7	0.0	7.46	4.31	4.4	-0.1	7.46	4.04	4.1	-0.1
7.73	3.85	3.8	0.1	7.73	4.44	4.4	0.0	7.73	4.20	4.2	0.0
8.00	3.89	3.9	0.0	8.00	4.49	4.5	0.0	8.00	4.24	4.3	0.0
8.26	4.00	3.9	0.1	8.26	4.56	4.6	0.0	8.26	4.29	4.4	-0.1
8.53	4.07	4.0	0.1	8.53	4.66	4.6	0.0	8.53	4.42	4.4	0.0
8.80	4.21	4.1	0.1	8.80	4.75	4.7	0.0	8.80	4.46	4.5	0.0
9.06	4.16	4.2	0.0	9.06	4.77	4.8	0.0	9.06	4.56	4.6	0.0
9.33	4.32	4.2	0.1	9.33	4.88	4.8	0.1	9.33	4.68	4.6	0.1
9.59	4.39	4.3	0.1	9.59	4.92	4.9	0.0	9.59	4.67	4.7	0.0
9.86	4.43	4.4	0.1	9.86	4.97	5.0	0.0	9.86	4.76	4.8	0.0
10.13	4.49	4.4	0.0	10.13	5.02	5.0	0.0	10.13	4.81	4.8	0.0
10.40	4.53	4.5	0.0	10.40	5.11	5.1	0.0	10.40	4.96	4.9	0.1
10.66	4.60	4.6	0.0	10.66	5.16	5.1	0.0	10.66	4.97	5.0	0.0
10.93	4.61	4.6	0.0	10.93	5.21	5.2	0.0	10.93	5.07	5.0	0.0
11.19	4.76	4.7	0.0	11.19	5.30	5.3	0.0	11.19	5.12	5.1	0.0
11.46	4.82	4.8	0.0	11.46	5.33	5.3	0.0	11.46	5.15	5.2	0.0
11.73	4.86	4.8	0.0	11.73	5.39	5.4	0.0	11.73	5.18	5.2	0.0
12.00	5.06	4.9	0.1	12.00	5.52	5.5	0.1	12.00	5.29	5.3	0.0
12.26	5.07	5.0	0.1	12.26	5.55	5.5	0.0	12.26	5.36	5.3	0.0
12.53	5.09	5.0	0.1	12.53	5.58	5.6	0.0	12.53	5.39	5.4	0.0
12.80	5.12	5.1	0.0	12.80	5.65	5.6	0.0	12.80	5.49	5.5	0.0
13.06	5.20	5.2	0.0	13.06	5.72	5.7	0.0	13.06	5.56	5.5	0.0
13.33	5.28	5.2	0.0	13.33	5.77	5.7	0.0	13.33	5.58	5.6	0.0
13.59	5.25	5.3	0.0	13.59	5.79	5.8	0.0	13.59	5.63	5.6	0.0
13.86	5.36	5.4	0.0	13.86	5.85	5.9	0.0	13.86	5.69	5.7	0.0
14.13	5.41	5.4	0.0	14.13	5.92	5.9	0.0	14.13	5.80	5.8	0.0
14.40	5.42	5.5	-0.1	14.40	5.94	6.0	0.0	14.40	5.84	5.8	0.0
14.66	5.55	5.5	0.0	14.66	6.04	6.0	0.0	14.66	5.90	5.9	0.0
14.93	5.55	5.6	0.0	14.93	6.06	6.1	0.0	14.93	5.96	5.9	0.0
15.19	5.74	5.7	0.1	15.19	6.14	6.1	0.0	15.19	5.95	6.0	0.0
15.46	5.69	5.7	0.0	15.46	6.19	6.2	0.0	15.46	6.08	6.0	0.0
15.73	5.73	5.8	0.0	15.73	6.23	6.2	0.0	15.73	6.10	6.1	0.0
16.00	5.87	5.8	0.0	16.00	6.30	6.3	0.0	16.00	6.17	6.1	0.0
16.26	5.82	5.9	-0.1	16.26	6.30	6.3	0.0	16.26	6.21	6.2	0.0
16.53	5.93	5.9	0.0	16.53	6.39	6.4	0.0	16.53	6.27	6.2	0.0
16.80	5.95	6.0	0.0	16.80	6.44	6.4	0.0	16.80	6.34	6.3	0.0
17.06	6.09	6.0	0.0	17.06	6.51	6.5	0.0	17.06	6.38	6.4	0.0
17.33	6.11	6.1	0.0	17.33	6.54	6.5	0.0	17.33	6.39	6.4	0.0
17.60	6.11	6.2	0.0	17.60	6.56	6.6	0.0	17.60	6.44	6.5	0.0
17.86	6.23	6.2	0.0	17.86	6.65	6.6	0.0	17.86	6.52	6.5	0.0
18.13	6.28	6.3	0.0	18.13	6.69	6.7	0.0	18.13	6.58	6.6	0.0
18.39	6.36	6.3	0.1	18.39	6.75	6.7	0.0	18.39	6.62	6.6	0.0
18.66	6.29	6.4	-0.1	18.66	6.75	6.8	0.0	18.66	6.65	6.7	0.0
18.93	6.35	6.4	-0.1	18.93	6.80	6.8	0.0	18.93	6.70	6.7	0.0
19.19	6.51	6.5	0.0	19.19	6.86	6.9	0.0	19.19	6.74	6.8	0.0
19.46	6.66	6.5	0.1	19.46	6.95	6.9	0.0	19.46	6.78	6.8	0.0
19.73	6.63	6.6	0.1	19.73	6.98	7.0	0.0	19.73	6.84	6.8	0.0
20.00	6.62	6.6	0.0	20.00	6.99	7.0	0.0	20.00	6.87	6.9	0.0
20.26	6.70	6.7	0.0	20.26	7.05	7.0	0.0	20.26	6.92	6.9	0.0
20.53	6.75	6.7	0.0	20.53	7.10	7.1	0.0	20.53	6.98	7.0	0.0

Pt. 1	est.	calc.	Pt. 2	est.	calc.	Pt. 3	est.	calc.	Pt. 4	est.	calc.
CO	1.27	1.27	CO	2.13	2.13	CO	1.80	1.80	CO	3.34	3.34
Kla-in	2.13	2.13	Kla-in	2.14	2.14	Kla-in	2.14	2.14	Kla-in	2.15	2.15
C*	11.79	11.79	C*	11.66	11.66	C*	11.77	11.77	C*	11.43	11.43
Sq.Dif.	2.1730	Sq.Dif.	0.3471	Sq.Dif.	0.1710 <th>Sq.Dif.</th> <td>0.1710<th>Sq.Dif.</th><td>0.2643</td><th>Sq.Dif.</th><td>0.2643</td></td>	Sq.Dif.	0.1710 <th>Sq.Dif.</th> <td>0.2643</td> <th>Sq.Dif.</th> <td>0.2643</td>	Sq.Dif.	0.2643	Sq.Dif.	0.2643
Time	D.O.	D.O.calc	diff	Time	D.O.	D.O.calc	diff	Time	D.O.	D.O.calc	diff
20.80	6.67	6.8	-0.1	20.80	7.11	7.1	0.0	20.80	7.03	7.0	0.0
21.06	6.92	6.8	0.1	21.06	7.22	7.2	0.0	21.06	7.09	7.1	0.0
21.33	6.84	6.9	0.0	21.33	7.19	7.2	0.0	21.33	7.10	7.1	0.0
21.60	6.90	6.9	0.0	21.60	7.24	7.3	0.0	21.60	7.13	7.2	0.0
21.86	7.06	6.9	0.1	21.86	7.33	7.3	0.0	21.86	7.19	7.2	0.0
22.13	7.05	7.0	0.1	22.13	7.35	7.3	0.0	22.13	7.24	7.3	0.0
22.39	7.10	7.0	0.1	22.39	7.38	7.4	0.0	22.39	7.30	7.3	0.0
22.66	7.15	7.1	0.1	22.66	7.41	7.4	0.0	22.66	7.29	7.3	-0.1
22.93	7.14	7.1	0.0	22.93	7.46	7.5	0.0	22.93	7.39	7.4	0.0
23.19	7.14	7.2	0.0	23.19	7.49	7.5	0.0	23.19	7.40	7.4	0.0
23.46	7.17	7.2	0.0	23.46	7.50	7.5	0.0	23.46	7.42	7.5	0.0
23.73	7.16	7.3	-0.1	23.73	7.53	7.6	-0.1	23.73	7.45	7.5	-0.1
24.00	7.15	7.3	-0.2	24.00	7.57	7.6	0.0	24.00	7.53	7.5	0.0
24.26	7.30	7.3	0.0	24.26	7.64	7.7	0.0	24.26	7.56	7.6	0.0
24.53	7.40	7.4	0.0	24.53	7.71	7.7	0.0	24.53	7.63	7.6	0.0
24.80	7.43	7.4	0.0	24.80	7.72	7.7	0.0	24.80	7.65	7.7	0.0
25.06	7.55	7.5	0.1	25.06	7.79	7.8	0.0	25.06	7.69	7.7	0.0
25.33	7.57	7.5	0.1	25.33	7.83	7.8	0.0	25.33	7.75	7.7	0.0
25.60	7.65	7.5	0.1	25.60	7.89	7.8	0.0	25.60	7.83	7.8	0.1
25.86	7.56	7.6	0.0	25.86	7.88	7.9	0.0	25.86	7.82	7.8	0.0
26.13	7.72	7.6	0.1	26.13	7.95	7.9	0.0	26.13	7.85	7.9	0.0
26.39	7.69	7.7	0.0	26.39	7.97	7.9	0.0	26.39	7.96	7.9	0.1
26.66	7.67	7.7	0.0	26.66	7.99	8.0	0.0	26.66	7.97	7.9	0.0
26.93	7.80	7.7	0.1	26.93	8.05	8.0	0.0	26.93	7.99	8.0	0.0
27.19	7.80	7.8	0.0	27.19	8.05	8.1	0.0	27.19	7.99	8.0	0.0
27.46	7.75	7.8	-0.1	27.46	8.06	8.1	0.0	27.46	8.02	8.0	0.0
27.73	7.97	7.9	0.1	27.73	8.18	8.1	0.1	27.73	8.06	8.1	0.0
28.00	7.89	7.9	0.0	28.00	8.20	8.2	0.0	28.00	8.20	8.1	0.1
28.26	7.99	7.9	0.1	28.26	8.22	8.2	0.0	28.26	8.16	8.1	0.0
28.53	8.11	8.0	0.1	28.53	8.27	8.2	0.1	28.53	8.19	8.2	0.0
28.80	8.18	8.0	0.2	28.80	8.31	8.3	0.1	28.80	8.23	8.2	0.0
29.06	8.19	8.0	0.2	29.06	8.34	8.3	0.1	29.06	8.27	8.2	0.0
29.33	8.20	8.1	0.1	29.33	8.37	8.3	0.1	29.33	8.28	8.3	0.0
29.60	8.28	8.1	0.2	29.60	8.43	8.3	0.1	29.60	8.34	8.3	0.0
29.86	8.16	8.1	0.0	29.86	8.42	8.4	0.0	29.86	8.42	8.3	0.1
30.13	8.23	8.2	0.1	30.13	8.45	8.4	0.0	30.13	8.42	8.4	0.0
30.39	8.29	8.2	0.1	30.39	8.48	8.4	0.0	30.39	8.42	8.4	0.0
30.66	8.22	8.2	0.0	30.66	8.48	8.5	0.0	30.66	8.46	8.4	0.0
30.93	8.29	8.3	0.0	30.93	8.53	8.5	0.0	30.93	8.50	8.5	0.0
31.19	8.28	8.3	0.0	31.19	8.54	8.5	0.0	31.19	8.51	8.5	0.0
31.46	8.28	8.3	-0.1	31.46	8.55	8.6	0.0	31.46	8.54	8.5	0.0
31.73	8.29	8.4	-0.1	31.73	8.58	8.6	0.0	31.73	8.59	8.6	0.0
32.00	8.44	8.4	0.0	32.00	8.65	8.6	0.0	32.00	8.61	8.6	0.0
32.26	8.56	8.4	0.1	32.26	8.69	8.6	0.0	32.26	8.63	8.6	0.0
32.53	8.59	8.5	0.1	32.53	8.74	8.7	0.1	32.53	8.69	8.7	0.0
32.79	8.58	8.5	0.1	32.79	8.75	8.7	0.0	32.79	8.69	8.7	0.0
33.06	8.62	8.5	0.1	33.06	8.77	8.7	0.0	33.06	8.70	8.7	0.0
33.33	8.54	8.6	0.0	33.33	8.75	8.8	0.0	33.33	8.76	8.7	0.0
33.60	8.59	8.6	0.0	33.60	8.80	8.8	0.0	33.60	8.79	8.8	0.0
33.86	8.66	8.6	0.0	33.86	8.83	8.8	0.0	33.86	8.80	8.8	0.0
34.13	8.50	8.7	-0.2	34.13	8.81	8.8	0.0	34.13	8.82	8.8	0.0
34.39	8.68	8.7	0.0	34.39	8.88	8.9	0.0	34.39	8.85	8.9	0.0
34.66	8.68	8.7	0.0	34.66	8.90	8.9	0.0	34.66	8.88	8.9	0.0
34.93	8.78	8.7	0.0	34.93	8.95	8.9	0.0	34.93	8.92	8.9	0.0
35.20	8.75	8.8	0.0	35.20	8.96	8.9	0.0	35.20	8.95	8.9	0.0
35.46	8.80	8.8	0.0	35.46	8.99	9.0	0.0	35.46	8.94	9.0	0.0
35.73	8.87	8.8	0.0	35.73	9.02	9.0	0.0	35.73	8.96	9.0	0.0
36.00	8.82	8.9	0.0	36.00	8.99	9.0	0.0	36.00	8.99	9.0	0.0
36.26	8.83	8.9	-0.1	36.26	9.04	9.1	0.0	36.26	9.06	9.0	0.0
36.53	8.88	8.9	0.0	36.53	9.08	9.1	0.0	36.53	9.09	9.1	0.0
36.79	8.86	8.9	-0.1	36.79	9.09	9.1	0.0	36.79	9.10	9.1	0.0
37.06	8.96	9.0	0.0	37.06	9.12	9.1	0.0	37.06	9.14	9.1	0.0
37.33	8.93	9.0	-0.1	37.33	9.11	9.1	0.0	37.33	9.14	9.1	0.0
37.60	8.95	9.0	-0.1	37.60	9.14	9.2	0.0	37.60	9.17	9.2	0.0
37.86	8.95	9.0	-0.1	37.86	9.18	9.2	0.0	37.86	9.22	9.2	0.0
38.13	9.09	9.1	0.0	38.13	9.23	9.2	0.0	38.13	9.23	9.2	0.0
38.39	9.08	9.1	0.0	38.39	9.24	9.2	0.0	38.39	9.22	9.2	0.0
38.66	9.16	9.1	0.0	38.66	9.26	9.3	0.0	38.66	9.23	9.3	0.0
38.93	9.20	9.1	0.1	38.93	9.29	9.3	0.0	38.93	9.27	9.3	0.0
39.20	9.16	9.2	0.0	39.20	9.28	9.3	0.0	39.20	9.31	9.3	0.0
39.46	9.26	9.2	0.1	39.46	9.35	9.3	0.0	39.46	9.33	9.3	0.0
39.73	9.20	9.2	0.0	39.73	9.33	9.4	0.0	39.73	9.36	9.4	0.0
40.00	9.20	9.2	0.0	40.00	9.34	9.4	0.0	40.00	9.41	9.4	0.0
40.26	9.32	9.3	0.1	40.26	9.37	9.4	0.0	40.26	9.40	9.4	0.0
40.53	9.36	9.3	0.1	40.53	9.42	9.4	0.0	40.53	9.41	9.4	0.0
40.79	9.32	9.3	0.0	40.79	9.44	9.4	0.0	40.79	9.44	9.5	0.0
41.06	9.20	9.3	-0.1	41.06	9.41	9.5	0.0	41.06	9.48	9.5	0.0
41.33	9.38	9.4	0.0	41.33	9.49	9.5	0.0	41.33	9.51	9.5	0.0

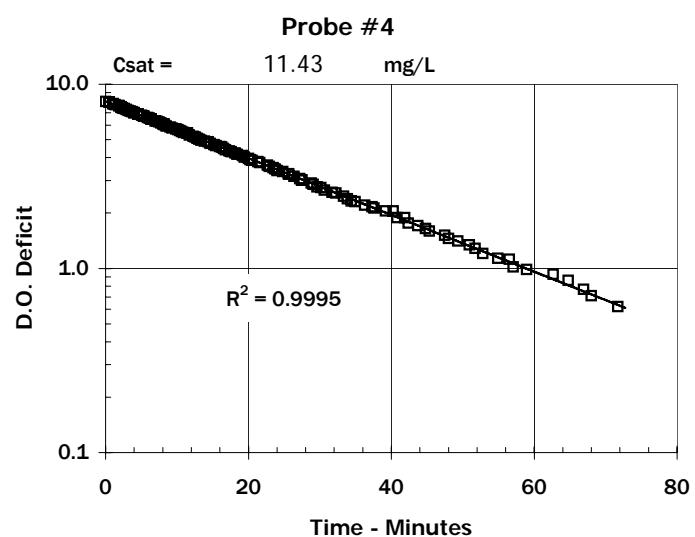
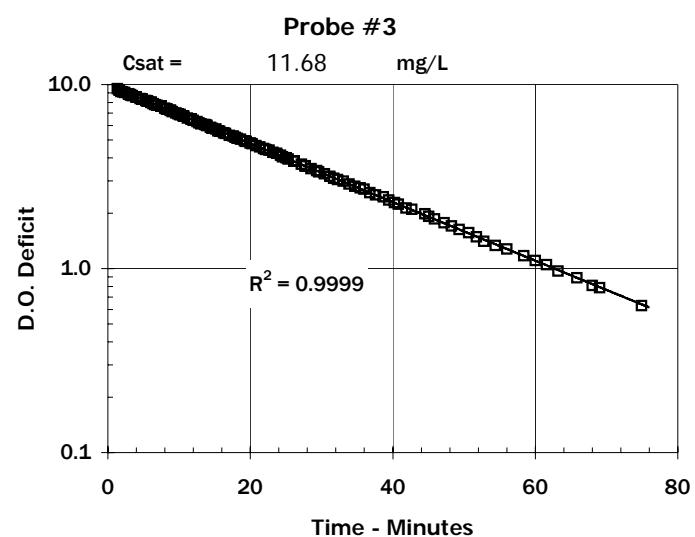
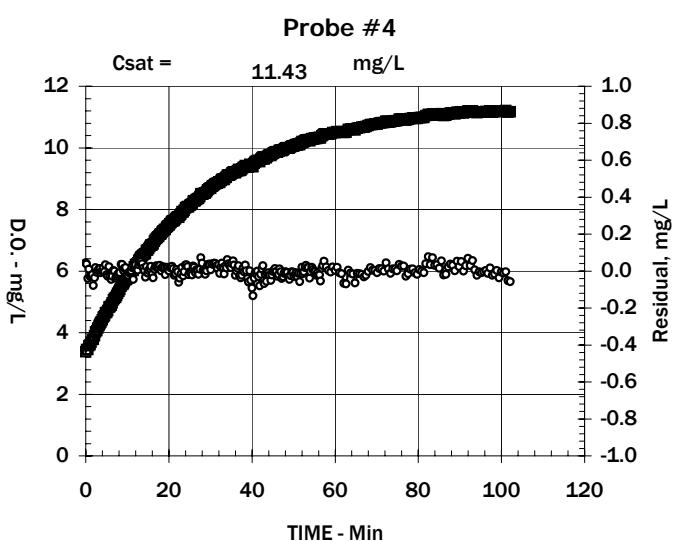
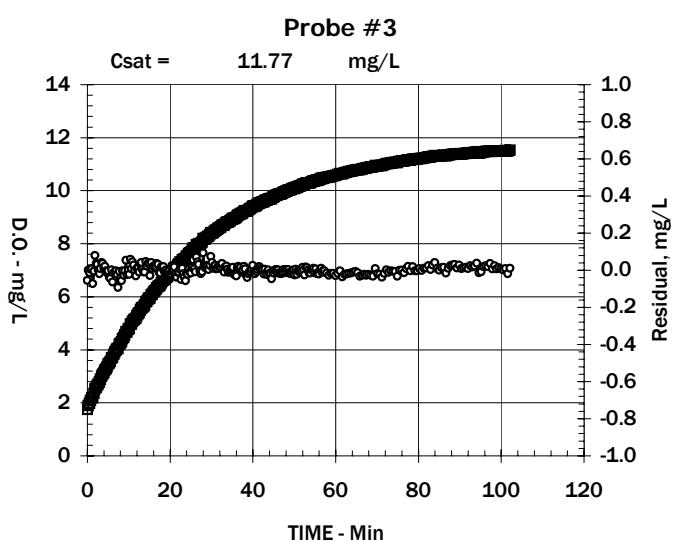
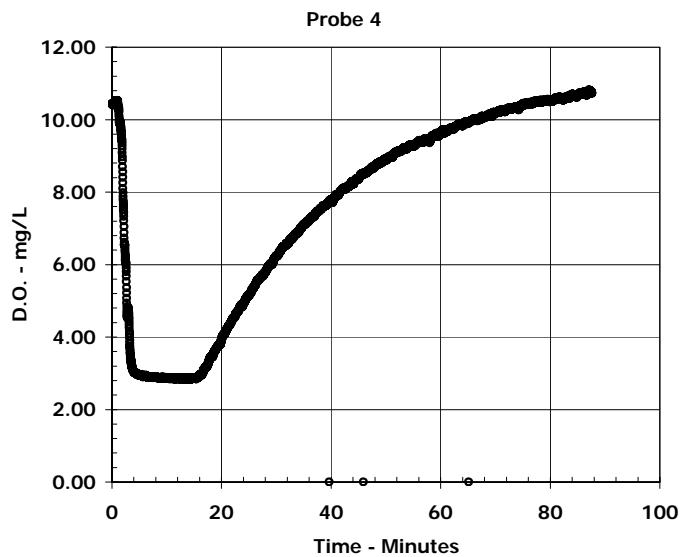
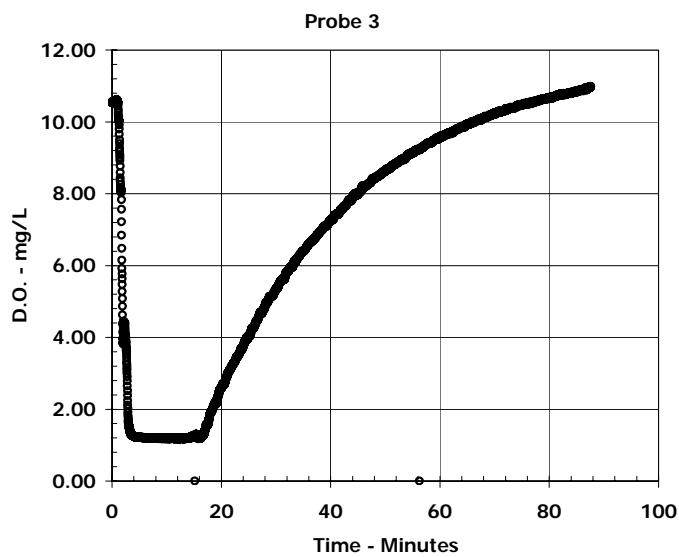
Pt. 1	est.	calc.	Pt. 2	est.	calc.	Pt. 3	est.	calc.	Pt. 4	est.	calc.
CO	1.27	1.27	CO	2.13	2.13	CO	1.80	1.80	CO	3.34	3.34
Kla-in	2.13	2.13	Kla-in	2.14	2.14	Kla-in	2.14	2.14	Kla-in	2.15	2.15
C*	11.79	11.79	C*	11.66	11.66	C*	11.77	11.77	C*	11.43	11.43
Sq.Dif.	2.1730	Sq.Dif.	0.3471	Sq.Dif.	0.1710 <th>Sq.Dif.</th> <td>0.2643</td> <th>Sq.Dif.</th> <td>0.2643</td> <th>Sq.Dif.</th> <td>0.2643</td>	Sq.Dif.	0.2643	Sq.Dif.	0.2643	Sq.Dif.	0.2643
Time	D.O.	D.O.calc	diff	Time	D.O.	D.O.calc	diff	Time	D.O.	D.O.calc	diff
41.60	9.38	9.4	0.0	41.60	9.50	9.5	0.0	41.60	9.54	9.5	0.0
41.86	9.39	9.4	0.0	41.86	9.49	9.5	0.0	41.86	9.55	9.5	0.0
42.13	9.39	9.4	0.0	42.13	9.52	9.5	0.0	42.13	9.56	9.6	0.0
42.39	9.35	9.5	-0.1	42.39	9.54	9.6	0.0	42.39	9.58	9.6	0.0
42.66	9.38	9.5	-0.1	42.66	9.55	9.6	0.0	42.66	9.58	9.6	0.0
42.93	9.51	9.5	0.0	42.93	9.59	9.6	0.0	42.93	9.63	9.6	0.0
43.20	9.36	9.5	-0.2	43.20	9.56	9.6	-0.1	43.20	9.63	9.6	0.0
43.46	9.57	9.5	0.0	43.46	9.63	9.6	0.0	43.46	9.64	9.7	0.0
43.73	9.62	9.6	0.1	43.73	9.68	9.7	0.0	43.73	9.68	9.7	0.0
44.00	9.49	9.6	-0.1	44.00	9.64	9.7	0.0	44.00	9.68	9.7	0.0
44.26	9.52	9.6	-0.1	44.26	9.66	9.7	0.0	44.26	9.71	9.7	0.0
44.53	9.59	9.6	0.0	44.53	9.68	9.7	0.0	44.53	9.70	9.7	0.0
44.79	9.62	9.6	0.0	44.79	9.72	9.7	0.0	44.79	9.75	9.8	0.0
45.06	9.65	9.7	0.0	45.06	9.74	9.8	0.0	45.06	9.76	9.8	0.0
45.33	9.62	9.7	-0.1	45.33	9.75	9.8	0.0	45.33	9.80	9.8	0.0
45.60	9.57	9.7	-0.1	45.60	9.75	9.8	0.0	45.60	9.82	9.8	0.0
45.86	9.46	9.7	-0.3	45.86	9.71	9.8	-0.1	45.86	9.82	9.8	0.0
46.13	9.73	9.7	0.0	46.13	9.81	9.8	0.0	46.13	9.85	9.9	0.0
46.39	9.63	9.8	-0.1	46.39	9.79	9.8	-0.1	46.39	9.85	9.9	0.0
46.66	9.82	9.8	0.0	46.66	9.87	9.9	0.0	46.66	9.88	9.9	0.0
46.93	9.80	9.8	0.0	46.93	9.87	9.9	0.0	46.93	9.89	9.9	0.0
47.20	9.71	9.8	-0.1	47.20	9.84	9.9	-0.1	47.20	9.91	9.9	0.0
47.46	9.81	9.8	0.0	47.46	9.89	9.9	0.0	47.46	9.95	9.9	0.0
47.73	9.88	9.9	0.0	47.73	9.93	9.9	0.0	47.73	9.95	10.0	0.0
48.00	9.89	9.9	0.0	48.00	9.95	9.9	0.0	48.00	9.98	10.0	0.0
48.26	9.96	9.9	0.1	48.26	9.98	10.0	0.0	48.26	9.98	10.0	0.0
48.53	9.92	9.9	0.0	48.53	9.98	10.0	0.0	48.53	10.01	10.0	0.0
48.79	9.97	9.9	0.0	48.79	9.99	10.0	0.0	48.79	10.01	10.0	0.0
49.06	10.05	9.9	0.1	49.06	10.02	10.0	0.0	49.06	10.03	10.0	0.0
49.33	10.08	10.0	0.1	49.33	10.05	10.0	0.0	49.33	10.05	10.1	0.0
49.60	10.05	10.0	0.1	49.60	10.06	10.0	0.0	49.60	10.07	10.1	0.0
49.86	10.00	10.0	0.0	49.86	10.06	10.1	0.0	49.86	10.09	10.1	0.0
50.13	10.03	10.0	0.0	50.13	10.06	10.1	0.0	50.13	10.08	10.1	0.0
50.39	9.93	10.0	-0.1	50.39	10.05	10.1	0.0	50.39	10.13	10.1	0.0
50.66	10.14	10.0	0.1	50.66	10.12	10.1	0.0	50.66	10.12	10.1	0.0
50.93	10.12	10.1	0.1	50.93	10.12	10.1	0.0	50.93	10.15	10.2	0.0
51.20	10.07	10.1	0.0	51.20	10.12	10.1	0.0	51.20	10.16	10.2	0.0
51.46	10.13	10.1	0.0	51.46	10.13	10.1	0.0	51.46	10.17	10.2	-0.1
51.73	10.06	10.1	-0.1	51.73	10.14	10.2	0.0	51.73	10.20	10.2	0.0
52.00	10.06	10.1	-0.1	52.00	10.16	10.2	0.0	52.00	10.23	10.2	0.0
52.26	10.03	10.1	-0.1	52.26	10.14	10.2	0.0	52.26	10.23	10.2	0.0
52.53	10.17	10.2	0.0	52.53	10.20	10.2	0.0	52.53	10.22	10.2	0.0
52.79	10.16	10.2	0.0	52.79	10.22	10.2	0.0	52.79	10.28	10.3	0.0
53.06	10.22	10.2	0.0	53.06	10.25	10.2	0.0	53.06	10.29	10.3	0.0
53.33	9.96	10.2	-0.2	53.33	10.17	10.2	-0.1	53.33	10.29	10.3	0.0
53.60	10.23	10.2	0.0	53.60	10.26	10.3	0.0	53.60	10.29	10.3	0.0
53.86	10.20	10.2	0.0	53.86	10.24	10.3	0.0	53.86	10.30	10.3	0.0
54.13	10.27	10.2	0.0	54.13	10.29	10.3	0.0	54.13	10.33	10.3	0.0
54.39	10.29	10.3	0.0	54.39	10.31	10.3	0.0	54.39	10.35	10.3	0.0
54.66	10.05	10.3	-0.2	54.66	10.24	10.3	-0.1	54.66	10.37	10.4	0.0
54.93	10.21	10.3	-0.1	54.93	10.29	10.3	0.0	54.93	10.36	10.4	0.0
55.20	10.16	10.3	-0.1	55.20	10.29	10.3	0.0	55.20	10.39	10.4	0.0
55.46	10.28	10.3	0.0	55.46	10.32	10.3	0.0	55.46	10.38	10.4	0.0
55.73	10.07	10.3	-0.3	55.73	10.26	10.4	-0.1	55.73	10.39	10.4	0.0
56.00	10.16	10.3	-0.2	56.00	10.30	10.4	-0.1	56.00	10.40	10.4	0.0
56.26	10.20	10.4	-0.2	56.26	10.32	10.4	-0.1	56.26	10.44	10.4	0.0
56.53	10.28	10.4	-0.1	56.53	10.35	10.4	0.0	56.53	10.46	10.4	-0.1
56.79	10.28	10.4	-0.1	56.79	10.37	10.4	0.0	56.79	10.45	10.5	0.0
57.06	10.36	10.4	0.0	57.06	10.41	10.4	0.0	57.06	10.47	10.5	0.0
57.33	10.31	10.4	-0.1	57.33	10.41	10.4	0.0	57.33	10.48	10.5	0.0
57.86	10.37	10.4	-0.1	57.86	10.43	10.5	0.0	57.86	10.49	10.5	0.0
58.39	10.46	10.5	0.0	58.39	10.47	10.5	0.0	58.39	10.51	10.5	0.0
58.93	10.44	10.5	-0.1	58.93	10.48	10.5	0.0	58.93	10.54	10.6	0.0
59.46	10.39	10.5	-0.1	59.46	10.48	10.5	0.0	59.46	10.56	10.6	0.0
60.00	10.45	10.5	-0.1	60.00	10.51	10.5	0.0	60.00	10.57	10.6	0.0
60.53	10.40	10.6	-0.2	60.53	10.51	10.6	-0.1	60.53	10.61	10.6	0.0
61.06	10.47	10.6	-0.1	61.06	10.54	10.6	0.0	61.06	10.64	10.6	0.0
61.60	10.46	10.6	-0.1	61.60	10.54	10.6	-0.1	61.60	10.63	10.7	0.0
62.13	10.54	10.6	-0.1	62.13	10.57	10.6	-0.1	62.13	10.67	10.7	0.0
62.66	10.54	10.7	-0.1	62.66	10.58	10.6	-0.1	62.66	10.69	10.7	0.0
63.20	10.71	10.7	0.0	63.20	10.67	10.7	0.0	63.20	10.71	10.7	0.0
63.73	10.67	10.7	0.0	63.73	10.67	10.7	0.0	63.73	10.73	10.7	0.0
64.26	10.67	10.7	0.0	64.26	10.68	10.7	0.0	64.26	10.76	10.8	0.0
64.79	10.70	10.7	0.0	64.79	10.68	10.7	0.0	64.79	10.78	10.8	0.0
65.33	10.67	10.8	-0.1	65.33	10.70	10.7	0.0	65.33	10.79	10.8	0.0
65.86	10.76	10.8	0.0	65.86	10.73	10.8	0.0	65.86	10.79	10.8	0.0
66.40	10.76	10.8	0.0	66.40	10.75	10.8	0.0	66.40	10.81	10.8	0.0
66.93	10.76	10.8	-0.1	66.93	10.75	10.8	0.0	66.93	10.84	10.9	0.0

Pt. 1	est.	calc.	Pt. 2	est.	calc.	Pt. 3	est.	calc.	Pt. 4	est.	calc.
CO	1.27	1.27	CO	2.13	2.13	CO	1.80	1.80	CO	3.34	3.34
Kla-in	2.13	2.13	Kla-in	2.14	2.14	Kla-in	2.14	2.14	Kla-in	2.15	2.15
C*	11.79	11.79	C*	11.66	11.66	C*	11.77	11.77	C*	11.43	11.43
Sq.Dif.	2.1730		Sq.Dif.	0.3471		Sq.Dif.	0.1710		Sq.Dif.	0.2643	
Time	D.O.	D.O.calc	diff	Time	D.O.	D.O.calc	diff	Time	D.O.	D.O.calc	diff
67.46	10.63	10.8	-0.2	67.46	10.72	10.8	-0.1	67.46	10.85	10.9	0.0
68.00	10.80	10.8	0.0	68.00	10.80	10.8	0.0	68.00	10.87	10.9	0.0
68.53	10.65	10.9	-0.2	68.53	10.76	10.8	-0.1	68.53	10.88	10.9	0.0
69.06	10.80	10.9	-0.1	69.06	10.82	10.9	0.0	69.06	10.89	10.9	0.0
69.59	10.84	10.9	-0.1	69.59	10.85	10.9	0.0	69.59	10.95	10.9	0.0
70.13	10.92	10.9	0.0	70.13	10.88	10.9	0.0	70.13	10.94	11.0	0.0
70.66	10.85	10.9	-0.1	70.66	10.87	10.9	0.0	70.66	10.95	11.0	0.0
71.20	11.08	10.9	0.1	71.20	10.95	10.9	0.0	71.20	10.95	11.0	0.0
71.73	11.00	11.0	0.0	71.73	10.93	10.9	0.0	71.73	10.99	11.0	0.0
72.26	11.07	11.0	0.1	72.26	10.99	10.9	0.0	72.26	11.02	11.0	0.0
72.79	11.17	11.0	0.2	72.79	11.01	11.0	0.1	72.79	11.02	11.0	0.0
73.33	11.18	11.0	0.2	73.33	11.02	11.0	0.1	73.33	11.04	11.0	0.0
73.86	10.96	11.0	-0.1	73.86	10.96	11.0	0.0	73.86	11.05	11.1	0.0
74.40	11.09	11.0	0.1	74.40	11.01	11.0	0.0	74.40	11.07	11.1	0.0
74.93	11.03	11.1	0.0	74.93	10.99	11.0	0.0	74.93	11.05	11.1	0.0
75.46	11.18	11.1	0.1	75.46	11.07	11.0	0.1	75.46	11.10	11.1	0.0
76.00	11.11	11.1	0.0	76.00	11.05	11.0	0.0	76.00	11.11	11.1	0.0
76.53	11.17	11.1	0.1	76.53	11.07	11.0	0.0	76.53	11.11	11.1	0.0
77.06	11.33	11.1	0.2	77.06	11.12	11.1	0.1	77.06	11.15	11.1	0.0
77.59	11.17	11.1	0.0	77.59	11.08	11.1	0.0	77.59	11.17	11.1	0.0
78.13	11.15	11.1	0.0	78.13	11.08	11.1	0.0	78.13	11.16	11.2	0.0
78.66	11.18	11.1	0.0	78.66	11.11	11.1	0.0	78.66	11.19	11.2	0.0
79.20	11.11	11.2	0.0	79.20	11.08	11.1	0.0	79.20	11.18	11.2	0.0
79.73	11.12	11.2	0.0	79.73	11.09	11.1	0.0	79.73	11.19	11.2	0.0
80.26	11.26	11.2	0.1	80.26	11.15	11.1	0.0	80.26	11.21	11.2	0.0
80.79	11.08	11.2	-0.1	80.79	11.09	11.1	0.0	80.79	11.21	11.2	0.0
81.33	11.25	11.2	0.0	81.33	11.16	11.1	0.0	81.33	11.24	11.2	0.0
81.86	11.28	11.2	0.1	81.86	11.19	11.2	0.0	81.86	11.25	11.2	0.0
82.40	11.20	11.2	0.0	82.40	11.19	11.2	0.0	82.40	11.27	11.2	0.0
82.93	11.05	11.2	-0.2	82.93	11.12	11.2	0.0	82.93	11.26	11.3	0.0
83.46	11.32	11.2	0.1	83.46	11.24	11.2	0.1	83.46	11.29	11.3	0.0
84.00	11.43	11.3	0.2	84.00	11.27	11.2	0.1	84.00	11.32	11.3	0.0
84.53	11.27	11.3	0.0	84.53	11.21	11.2	0.0	84.53	11.29	11.3	0.0
85.06	11.42	11.3	0.1	85.06	11.26	11.2	0.1	85.06	11.29	11.3	0.0
85.59	11.40	11.3	0.1	85.59	11.27	11.2	0.1	85.59	11.32	11.3	0.0
86.13	11.40	11.3	0.1	86.13	11.26	11.2	0.0	86.13	11.33	11.3	0.0
86.66	11.42	11.3	0.1	86.66	11.26	11.2	0.0	86.66	11.31	11.3	0.0
87.20	11.41	11.3	0.1	87.20	11.28	11.2	0.0	87.20	11.34	11.3	0.0
87.73	11.25	11.3	-0.1	87.73	11.24	11.2	0.0	87.73	11.36	11.3	0.0
88.26	11.48	11.3	0.1	88.26	11.32	11.3	0.1	88.26	11.37	11.3	0.0
88.79	11.36	11.3	0.0	88.79	11.28	11.3	0.0	88.79	11.39	11.4	0.0
89.33	11.42	11.3	0.1	89.33	11.32	11.3	0.0	89.33	11.37	11.4	0.0
89.86	11.42	11.4	0.1	89.86	11.32	11.3	0.0	89.86	11.40	11.4	0.0
90.40	11.50	11.4	0.1	90.40	11.35	11.3	0.1	90.40	11.39	11.4	0.0
90.93	11.49	11.4	0.1	90.93	11.34	11.3	0.0	90.93	11.40	11.4	0.0
91.46	11.53	11.4	0.2	91.46	11.37	11.3	0.1	91.46	11.41	11.4	0.0
92.00	11.55	11.4	0.2	92.00	11.39	11.3	0.1	92.00	11.41	11.4	0.0
92.53	11.59	11.4	0.2	92.53	11.40	11.3	0.1	92.53	11.43	11.4	0.0
93.06	11.59	11.4	0.2	93.06	11.41	11.3	0.1	93.06	11.43	11.4	0.0
93.59	11.52	11.4	0.1	93.59	11.37	11.3	0.0	93.59	11.44	11.4	0.0
94.13	11.61	11.4	0.2	94.13	11.40	11.3	0.1	94.13	11.47	11.4	0.0
94.66	11.50	11.4	0.1	94.66	11.36	11.3	0.0	94.66	11.42	11.4	0.0
95.20	11.49	11.4	0.1	95.20	11.36	11.3	0.0	95.20	11.43	11.4	0.0
95.73	11.35	11.4	-0.1	95.73	11.33	11.4	0.0	95.73	11.47	11.4	0.0
96.26	11.44	11.4	0.0	96.26	11.37	11.4	0.0	96.26	11.48	11.5	0.0
96.79	11.51	11.4	0.1	96.79	11.39	11.4	0.0	96.79	11.48	11.5	0.0
97.33	11.47	11.5	0.0	97.33	11.39	11.4	0.0	97.33	11.50	11.5	0.0
97.86	11.32	11.5	-0.1	97.86	11.32	11.4	-0.1	97.86	11.48	11.5	0.0
98.40	11.43	11.5	0.0	98.40	11.37	11.4	0.0	98.40	11.50	11.5	0.0
98.93	11.58	11.5	0.1	98.93	11.42	11.4	0.0	98.93	11.49	11.5	0.0
99.46	11.39	11.5	-0.1	99.46	11.35	11.4	0.0	99.46	11.50	11.5	0.0
100.00	11.47	11.5	0.0	100.00	11.39	11.4	0.0	100.00	11.50	11.5	0.0
100.53	11.41	11.5	-0.1	100.53	11.37	11.4	0.0	100.53	11.50	11.5	0.0
101.06	11.41	11.5	-0.1	101.06	11.38	11.4	0.0	101.06	11.51	11.5	0.0
101.59	11.48	11.5	0.0	101.59	11.38	11.4	0.0	101.59	11.49	11.5	0.0
102.13	11.41	11.5	-0.1	102.13	11.37	11.4	0.0	102.13	11.52	11.5	0.0

Probe 1			Probe 2			Probe 3			Probe 4		
Lower	9.69%	Upper	Lower	17.92%	Upper	Lower	14.84%	Upper	Lower	29.56%	Upper
Value	Abs.Un.	%LSE	Value	Abs.Un.	%LSE	Value	Abs.Un.	%LSE	Value	Abs.Un.	%LSE
C*	11.789	0.016	0.135	C*	11.665	0.006	0.054	C*	11.771	0.004	0.038
CO	1.266	0.019	1.487	CO	2.135	0.008	0.353	CO	1.803	0.005	0.293
KLaT	2.129	0.000	0.497	KLaT	2.140	0.000	0.219	KLaT	2.144	0.000	0.147
Error	0.086		Error	0.034		Error	0.024		Error	0.030	
PROJECT:	PHi - Membrane Tube Diffusers Only										
DATE:	11/8/2006										
RUN:	2.00										



Project: PHi - Membrane Tube Diffusers Only
 Date: Nov 08, 2006
 Run: 2



Project: PHi - Membrane Tube Diffusers Only
 Date: Nov 08, 2006
 Run: 2

**AIR FLOW RATE DETERMINATION
ANR 73 COMMERCIAL ANNULAR**

PROJECT : PHi - Membrane Tube Diffusers Only

$$\text{SCFM} = \frac{\text{C}''}{\frac{[\text{BP} + \text{LP}]}{[\text{LT} + 460]}}$$

$$\begin{aligned}\text{C}' &= \text{Fna} * \text{k} * \text{D}^2 * \text{Fra} * \text{Fpb} * \text{Ftb} * \text{Fg} * \text{Fpv} * \text{Faa} * \text{Fl} * \text{Fm} * \text{Ya} \\ \text{C}'' &= \text{C}' \text{ VALUE CORRECTED FOR HUMIDITY}\end{aligned}$$

RUN # **2**
DATE Nov-06

OPERATING CONDITIONS

ANNULAR TYPE		AWR-73	
BAROMETRIC PRESSURE	* BP	14.19	PSIA
LINE PRESSURE	* LP	8.87	PSIG
LINE TEMPERATURE	* LT	130	°F
DIFFERENTIAL PRESSURE	* ^H	0.02	In. H2O
RELATIVE HUMIDITY	* RH	68%	%
AMBIENT TEMPERATURE	*	15.5	62 °F
PIPE INSIDE DIAMETER	* D	4.026	In.
UNITS CONVERSION FACTOR	Fna	128.520	
ANNULAR FLOW COEFFICIENT	k	0.746	
SQUARE OF PIPE ID	D^2	16.209	
BASE PRESSURE		14.700	PSIA
BASE PRESSURE FACTOR	Fpb	1.002	
BASE TEMPERATURE		68.000	°F
BASE TEMPERATURE FACTOR	Ftb	1.015	
THERMAL EXPANSION FACTOR	Faa	1.002	
MANOMETER LOCATION FACTOR	Fl	1.000	
HG MANOMETER CORRECTION FACTOR	Fm	1.000	
REYNOLD NUMBER	Rd	15,211.9	
FLOWING VISCOSITY	vis	0.020	cP
REYNOLD NUMBER FACTOR	Fra	0.965	
SPECIFIC GRAVITY	g	1.000	
SPECIFIC GRAVITY FACTOR	Fg	1.000	
SUPERCOMPRESSIBILITY	Z	1.000	
SUPERCOMPRESSIBILITY FACTOR	Fpv	1.000	
GAS EXPANSION FACTOR	Ya	1.000	
SCFM UNCORRECTED FOR HUMIDITY	SCFM	41.6	
C'		1,527.58	
VAPOR PRESSURE OF WATER AMB. TEMP.	VP	0.275	
ACTUAL CUBIC FEET PER MINUTE	ACFM	29.6	335.4
HUMIDITY CORRECTED STANDARD AIR FLOW	SCFM	41.4	@68°F, 36% RH, 14.7 PSIA
INLET CUBIC FEET PER MINUTE	ICFM	48.1	
C"		1,519.15	

FORMULAS AND FACTORS DERIVED FROM: L.K.Spink; "Principles and Practice of FLOW METER ENGINEERING"; Ninth Ed., Nov 1975; The FOXBORO CO., Foxboro, Mass.

"ORIFICE FLOW METER"; THE BRISTOL COMPANY; Waterbury, Conn.

"ANNULAR FLOW HANDBOOK"; August 1978; DIETERICH STANDARD CORPORATION; Boulder, Co.

HUMIDITY CORRECTED AIR FLOW DETERMINED per: "ASCE STANDARD Measurement of Oxygen Transfer in Clean Water"; ANNEX A; July 1984; American Society of Civil Engineers

ASCE OXYGEN TRANSFER DETERMINATION

PROJECT: Phi - Membrane Tube Diffusers + Phi Pumping	599 Waldron Rd.			
DATE: 8-Nov-06	LaVergne, TN 37086			
RUN: 3	615/793-7547			
	FAX 615/793/5070			
Barometric Pres. (PSIA) (mm Hg)	14.182 733.40	14.180 733.30	14.176 733.10	C' Air Flow Device 1 (Annubar) 1,518.75 Air Flow Device 1 (SCFM) 40.08
Ambient Temperature (°F)	63.90	64.20	65.10	C' Air Flow Device 2 (Orifice) 133.88 Air Flow Device 2 (SCFM) 39.94
Relative Humidity (%)	65%	64%	63%	
Line Pressure (PSIG) (In. Hg)	8.866 18.05	8.866 18.05	8.866 18.05	
Line Temperature (°F)	135.00	136.00	136.00	
ΔH Air Flow Dev. 1 (Annubar)	0.019	0.018	0.017	Average Air Flow (SCFM) 40.01
ΔH Air Flow Dev. 2 (Orifice)	2.450	2.350	2.100	Effective Depth Correction (f) 0.32
ΔH Air Flow Dev. 3 (Annubar)	NA	NA	NA	Headloss (In. H ₂ O) 20.42
ΔH Air Flow Dev. 4 (Annubar)	NA	NA	NA	C* (mg/l) 11.60
Water Temp. (°C)	14.69	14.70	14.72	CsmT (Standard Methods, mg/l) 10.15
Orifice Diameter (in)		1.349		C* ₂₀ Standard Conditions 10.72
Number Of Aeration Devices		28		Tank Volume (Ft ³) 6,840.6
Side Water Depth (ft)		19.75	(6.00 m)	(Gallons) 51,171.4
Air Release Depth (ft)		18.75	(5.70 m)	(m ³) 193.7
Tank Length (ft)		0.00	(0.00 m)	(Million Pounds) 0.427
Tank Width (ft)		0.00	(0.00 m)	
Tank Diameter (ft)		21.00	(6.38 m)	#Na ₂ SO ₃ @ 160% Stoichiometric 63
Gear Reducer or Belt Efficiency		100.0%		Cobalt Concen. (mg/l) 0.100
Motor Efficiency		89.0%		Grams Cobalt Chloride 79.9
Total HP _{wire} av.		2.69	(2.01 kw)	Total HP _{motor} av. 2.39
				TDS (mg/L) 568.00

NON-LINEAR REGRESSION RESULTS

Probe	K _{LAT}	K _{La20}	SOTR	SOTR/Dev	SOTE	SAE _{wire}	C*	Std. Err.
1	2.58	2.93	13.58	0.48	32.75	5.05	11.70	0.0600
2	2.51	2.84	12.95	0.46	31.24	4.81	11.49	0.1001
3	2.58	2.92	13.51	0.48	32.59	5.02	11.66	0.0199
4	2.55	2.89	13.26	0.47	32.00	4.93	11.56	0.0316
avg.	2.55	2.90	13.32	0.48	32.14	4.95	11.60	0.0529
Avg	2.56	2.91	13.38	0.48	32.29	4.98	11.61	Exclude Max&Min
TDS	2.66	3.02	13.89	0.50	33.51	5.16	11.60	1.79%
<i>Corrected</i>	/hr	/hr	#O2/hr	0.444	%	#O2/hr-WHP		

OXYGEN TRANSFER

Total SCFM:	40.0	:Nm ³ /Hr	18.881	L/s	#O2/Hr:	13.89	6.300	:KgO2/Hr
SCFM/Diff.:	1.43	:Nm ³ /hr/Diff		#O2/Hr/Diff.:	0.50	0.225	:KgO2/Hr/Diff.	
SCFM/KCF:	5.8	:Nm ³ /hr/m ³		#O2/Day:	333.3	151.2	:KgO2/Day	
Total ICFM:	47.1	22.24 L/s		#O2/Day/1000 Ft ³ :	49	0.78	:KgO2/Day/m ³	

LINEAR REGRESSION RESULTS

Probe	K _{LAT}	K _{La20}	SOTR	SOTR/Dev	SOTE	SAE _{wire}	C*	Corr. Coeff.
1	2.65	3.00	13.79	0.49	33.27	5.13	11.59	0.9990
2	2.69	3.05	13.69	0.49	33.03	5.09	11.33	0.9992
3	2.68	3.04	13.93	0.50	33.61	5.18	11.55	0.9996
4	2.54	2.88	13.22	0.47	31.90	4.92	11.56	0.9996
avg.	2.64	2.99	13.66	0.49	32.95	5.08	11.51	0.9994
Avg	2.67	3.02	13.84	0.49	33.40	5.15	11.56	Exclude Max&Min
TDS	2.75	3.12	14.24	0.51	34.36	5.30	11.51	
<i>Corrected</i>	/hr	/hr	#O2/hr	0.444	%	#O2/hr-HPw		

EUROPEAN STANDARD

Probe	K _{LAT}	K _{La10}	SOTR	SOTR/Dev	SAE	C*
1	2.61	2.35	6.16	0.22	3.07	11.70
2	2.60	2.33	6.01	0.21	3.00	11.49
3	2.63	2.36	6.17	0.22	3.08	11.66
4	2.55	2.29	5.93	0.21	2.96	11.56
NA	NA	NA	NA	NA	NA	NA
NA	NA	NA	NA	NA	NA	NA
avg.	2.60	2.33	6.06	0.22	3.02	11.60
Avg	2.61	2.34	6.08	0.22	3.03	11.61
TDS	2.71	2.43	6.32	0.23	3.15	11.60
<i>Corrected</i>	/hr	/hr	kg O ₂ /hr		kg O ₂ /hr-kw	mg/L

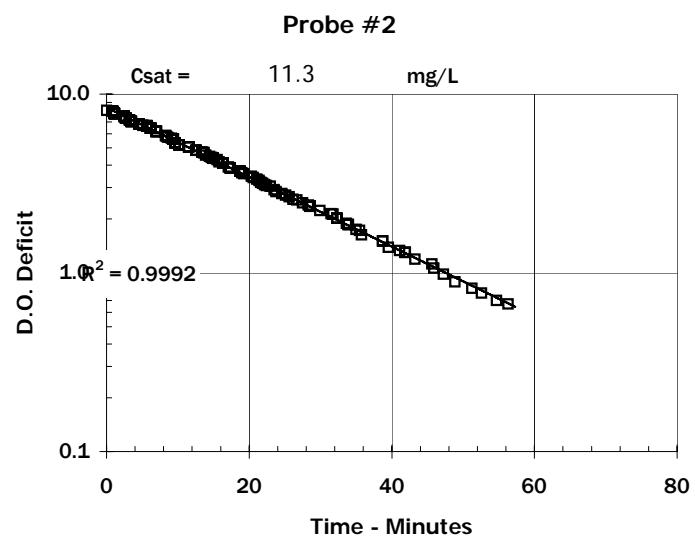
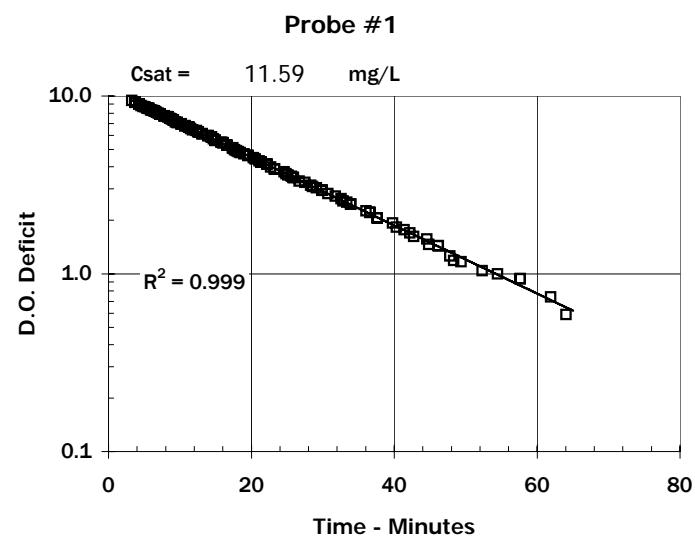
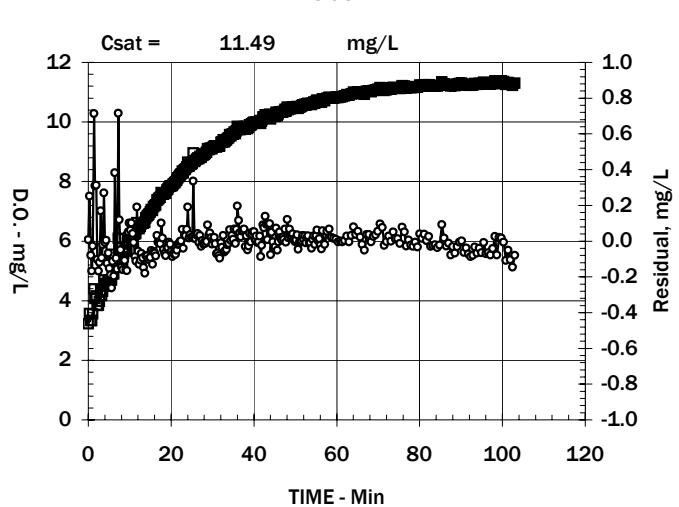
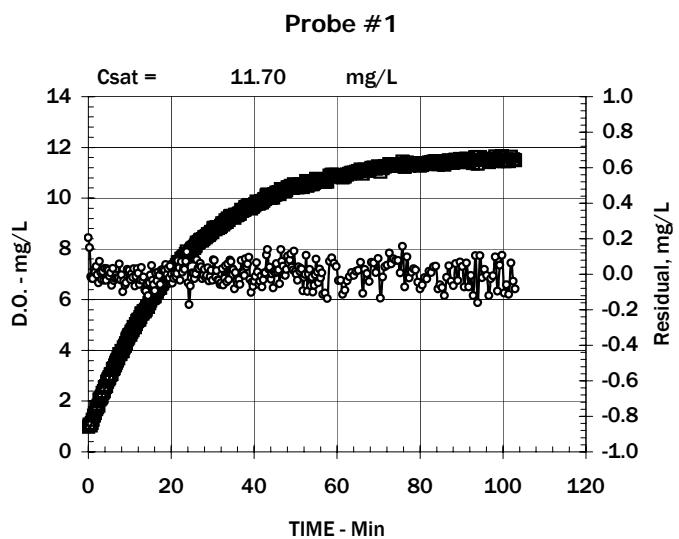
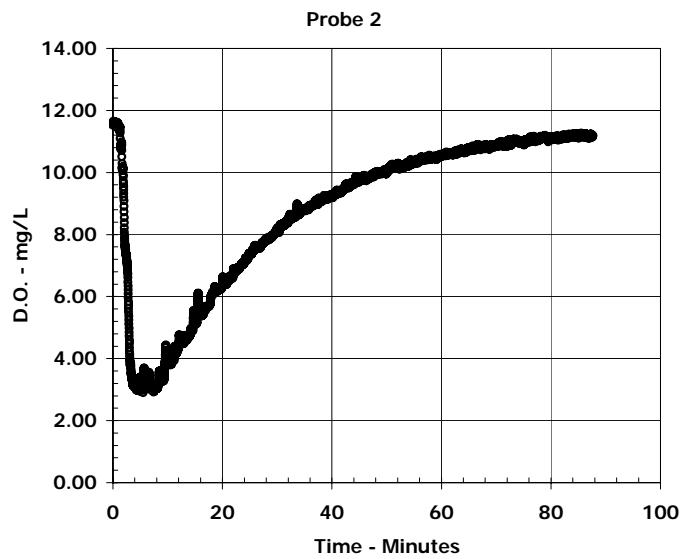
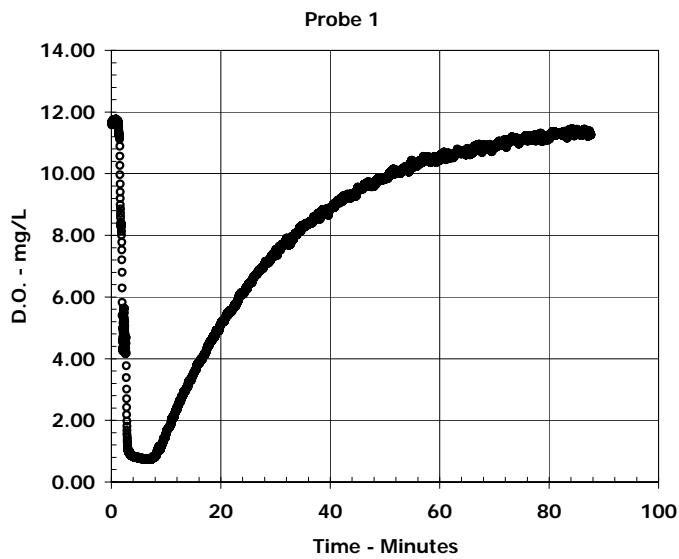
Pt. 1	est.	calc.	Pt. 2	est.	calc.	Pt. 3	est.	calc.	Pt. 4	est.	calc.
CO	0.78	0.78	CO	3.21	3.21	CO	0.99	0.99	CO	2.32	2.32
Kla-in	2.58	2.58	Kla-in	2.51	2.51	Kla-in	2.58	2.58	Kla-in	2.55	2.55
C*	11.70	11.70	C*	11.49	11.49	C*	11.66	11.66	C*	11.56	11.56
Sq.Dif.	1.0700		Sq.Dif.	2.9772		Sq.Dif.	0.1171		Sq.Dif.	0.2961	
Time	D.O.	D.O.calc	diff	Time	D.O.	D.O.calc	diff	Time	D.O.	D.O.calc	diff
0.00	0.98	0.8	0.2	0.00	3.22	3.2	0.0	0.00	1.00	1.0	0.0
0.31	1.07	0.9	0.2	0.31	3.57	3.3	0.3	0.31	1.13	1.1	0.0
0.58	1.03	1.0	0.0	0.58	3.33	3.4	-0.1	0.58	1.26	1.3	0.0
0.84	1.14	1.2	0.0	0.84	3.33	3.5	-0.2	0.84	1.35	1.4	0.0
1.11	1.26	1.3	0.0	1.11	3.56	3.6	0.0	1.11	1.47	1.5	0.0
1.38	1.43	1.4	0.0	1.38	4.39	3.7	0.7	1.38	1.58	1.6	0.0
1.64	1.53	1.5	0.0	1.64	4.07	3.8	0.3	1.64	1.73	1.7	0.0
1.91	1.68	1.6	0.0	1.91	4.16	3.8	0.3	1.91	1.88	1.8	0.0
2.18	1.75	1.8	0.0	2.18	3.83	3.9	-0.1	2.18	1.93	1.9	0.0
2.45	1.82	1.9	0.0	2.45	3.85	4.0	-0.2	2.45	2.07	2.1	0.0
2.71	2.05	2.0	0.1	2.71	3.98	4.1	-0.1	2.71	2.14	2.2	0.0
2.98	2.10	2.1	0.0	2.98	4.35	4.2	0.2	2.98	2.24	2.3	0.0
3.25	2.17	2.2	0.0	3.25	4.17	4.3	-0.1	3.25	2.36	2.4	0.0
3.51	2.32	2.3	0.0	3.51	4.32	4.3	0.0	3.51	2.48	2.5	0.0
3.78	2.38	2.4	0.0	3.78	4.69	4.4	0.3	3.78	2.60	2.6	0.0
4.04	2.55	2.5	0.0	4.04	4.49	4.5	0.0	4.04	2.72	2.7	0.0
4.31	2.59	2.6	0.0	4.31	4.58	4.6	0.0	4.31	2.82	2.8	0.0
4.58	2.76	2.7	0.0	4.58	4.53	4.7	-0.1	4.58	2.93	2.9	0.0
4.84	2.85	2.8	0.0	4.84	4.66	4.7	-0.1	4.84	3.00	3.0	0.0
5.11	2.92	2.9	0.0	5.11	4.65	4.8	-0.2	5.11	3.14	3.1	0.0
5.38	3.04	3.0	0.0	5.38	4.69	4.9	-0.2	5.38	3.24	3.2	0.0
5.65	3.07	3.1	-0.1	5.65	4.69	5.0	-0.3	5.65	3.33	3.3	0.0
5.91	3.26	3.2	0.0	5.91	4.91	5.0	-0.1	5.91	3.41	3.4	0.0
6.18	3.29	3.3	0.0	6.18	4.90	5.1	-0.2	6.18	3.50	3.5	0.0
6.45	3.40	3.4	0.0	6.45	5.55	5.2	0.4	6.45	3.55	3.6	0.0
6.71	3.51	3.5	0.0	6.71	5.14	5.2	-0.1	6.71	3.62	3.7	0.0
6.98	3.59	3.6	0.0	6.98	5.15	5.3	-0.2	6.98	3.76	3.8	0.0
7.25	3.68	3.7	0.0	7.25	6.09	5.4	0.7	7.25	3.83	3.8	0.0
7.51	3.85	3.8	0.1	7.51	5.56	5.4	0.1	7.51	3.88	3.9	-0.1
7.78	3.85	3.9	0.0	7.78	5.46	5.5	0.0	7.78	4.03	4.0	0.0
8.05	3.97	4.0	0.0	8.05	5.43	5.6	-0.1	8.05	4.14	4.1	0.0
8.31	3.96	4.1	-0.1	8.31	5.48	5.6	-0.2	8.31	4.19	4.2	0.0
8.58	4.11	4.1	0.0	8.58	5.59	5.7	-0.1	8.58	4.28	4.3	0.0
8.84	4.17	4.2	-0.1	8.84	5.66	5.8	-0.1	8.84	4.36	4.4	0.0
9.11	4.27	4.3	0.0	9.11	5.67	5.8	-0.2	9.11	4.47	4.4	0.0
9.38	4.43	4.4	0.0	9.38	5.73	5.9	-0.2	9.38	4.56	4.5	0.0
9.65	4.50	4.5	0.0	9.65	6.01	6.0	0.1	9.65	4.58	4.6	0.0
9.91	4.59	4.6	0.0	9.91	6.12	6.0	0.1	9.91	4.67	4.7	0.0
10.18	4.62	4.6	0.0	10.18	6.14	6.1	0.1	10.18	4.78	4.8	0.0
10.44	4.73	4.7	0.0	10.44	6.24	6.1	0.1	10.44	4.82	4.8	0.0
10.71	4.79	4.8	0.0	10.71	6.24	6.2	0.0	10.71	4.92	4.9	0.0
10.98	4.92	4.9	0.0	10.98	6.25	6.3	0.0	10.98	4.97	5.0	0.0
11.25	4.90	5.0	-0.1	11.25	6.23	6.3	-0.1	11.25	5.05	5.1	0.0
11.51	5.03	5.0	0.0	11.51	6.26	6.4	-0.1	11.51	5.15	5.2	0.0
11.78	5.15	5.1	0.0	11.78	6.62	6.4	0.2	11.78	5.22	5.2	0.0
12.05	5.20	5.2	0.0	12.05	6.43	6.5	-0.1	12.05	5.35	5.3	0.0
12.31	5.21	5.3	-0.1	12.31	6.41	6.5	-0.1	12.31	5.40	5.4	0.0
12.58	5.31	5.3	0.0	12.58	6.49	6.6	-0.1	12.58	5.47	5.4	0.0
12.84	5.45	5.4	0.0	12.84	6.58	6.6	-0.1	12.84	5.55	5.5	0.0
13.11	5.45	5.5	0.0	13.11	6.61	6.7	-0.1	13.11	5.59	5.6	0.0
13.38	5.54	5.6	0.0	13.38	6.61	6.8	-0.1	13.38	5.63	5.7	0.0
13.65	5.54	5.6	-0.1	13.65	6.63	6.8	-0.2	13.65	5.73	5.7	0.0
13.91	5.60	5.7	-0.1	13.91	6.78	6.9	-0.1	13.91	5.76	5.8	0.0
14.18	5.71	5.8	-0.1	14.18	6.83	6.9	-0.1	14.18	5.84	5.9	0.0
14.44	5.71	5.8	-0.1	14.44	6.86	7.0	-0.1	14.44	5.87	5.9	-0.1
14.71	5.85	5.9	0.0	14.71	6.91	7.0	-0.1	14.71	5.93	6.0	-0.1
14.98	5.96	6.0	0.0	14.98	6.97	7.1	-0.1	14.98	6.02	6.1	0.0
15.25	6.08	6.0	0.0	15.25	7.06	7.1	-0.1	15.25	6.12	6.1	0.0
15.51	6.06	6.1	0.0	15.51	7.03	7.2	-0.1	15.51	6.18	6.2	0.0
15.78	6.10	6.2	-0.1	15.78	7.15	7.2	-0.1	15.78	6.21	6.2	0.0
16.05	6.13	6.2	-0.1	16.05	7.19	7.3	-0.1	16.05	6.30	6.3	0.0
16.31	6.29	6.3	0.0	16.31	7.22	7.3	-0.1	16.31	6.39	6.4	0.0
16.58	6.31	6.3	0.0	16.58	7.38	7.3	0.0	16.58	6.41	6.4	0.0
16.85	6.42	6.4	0.0	16.85	7.39	7.4	0.0	16.85	6.46	6.5	0.0
17.11	6.46	6.5	0.0	17.11	7.43	7.4	0.0	17.11	6.52	6.5	0.0
17.38	6.47	6.5	-0.1	17.38	7.47	7.5	0.0	17.38	6.61	6.6	0.0
17.64	6.61	6.6	0.0	17.64	7.63	7.5	0.1	17.64	6.66	6.7	0.0
17.91	6.67	6.6	0.0	17.91	7.59	7.6	0.0	17.91	6.68	6.7	0.0
18.18	6.73	6.7	0.0	18.18	7.57	7.6	0.0	18.18	6.80	6.8	0.0
18.44	6.78	6.8	0.0	18.44	7.59	7.7	-0.1	18.44	6.84	6.8	0.0
18.71	6.87	6.8	0.1	18.71	7.62	7.7	-0.1	18.71	6.89	6.9	0.0
18.98	6.87	6.9	0.0	18.98	7.71	7.7	0.0	18.98	6.95	6.9	0.0
19.25	6.96	6.9	0.0	19.25	7.75	7.8	0.0	19.25	7.00	7.0	0.0
19.51	6.96	7.0	0.0	19.51	7.82	7.8	0.0	19.51	7.08	7.0	0.0
19.78	7.08	7.0	0.0	19.78	7.85	7.9	0.0	19.78	7.12	7.1	0.0
20.05	7.09	7.1	0.0	20.05	7.85	7.9	-0.1	20.05	7.15	7.1	0.0
20.31	7.09	7.1	-0.1	20.31	7.86	7.9	-0.1	20.31	7.20	7.2	0.0
20.58	7.17	7.2	0.0	20.58	7.92	8.0	-0.1	20.58	7.25	7.3	0.0

Pt. 1	est.	calc.	Pt. 2	est.	calc.	Pt. 3	est.	calc.	Pt. 4	est.	calc.
CO	0.78	0.78	CO	3.21	3.21	CO	0.99	0.99	CO	2.32	2.32
Kla-in	2.58	2.58	Kla-in	2.51	2.51	Kla-in	2.58	2.58	Kla-in	2.55	2.55
C*	11.70	11.70	C*	11.49	11.49	C*	11.66	11.66	C*	11.56	11.56
Sq.Dif.	1.0700	Sq.Dif.	2.9772	Sq.Dif.	0.1171 <th>Sq.Dif.</th> <td>0.2961<th></th><th></th><th></th><th></th></td>	Sq.Dif.	0.2961 <th></th> <th></th> <th></th> <th></th>				
Time	D.O.	D.O.calc	diff	Time	D.O.	D.O.calc	diff	Time	D.O.	D.O.calc	diff
20.85	7.25	7.2	0.0	20.85	7.95	8.0	-0.1	20.85	7.27	7.3	0.0
21.11	7.28	7.3	0.0	21.11	7.99	8.1	-0.1	21.11	7.35	7.4	0.0
21.38	7.35	7.3	0.0	21.38	8.05	8.1	-0.1	21.38	7.38	7.4	0.0
21.64	7.47	7.4	0.1	21.64	8.12	8.1	0.0	21.64	7.44	7.4	0.0
21.91	7.48	7.4	0.0	21.91	8.16	8.2	0.0	21.91	7.52	7.5	0.0
22.18	7.46	7.5	0.0	22.18	8.21	8.2	0.0	22.18	7.52	7.5	0.0
22.44	7.61	7.5	0.1	22.44	8.25	8.2	0.0	22.44	7.56	7.6	0.0
22.71	7.60	7.6	0.0	22.71	8.35	8.3	0.1	22.71	7.60	7.6	0.0
22.98	7.67	7.6	0.0	22.98	8.28	8.3	0.0	22.98	7.68	7.7	0.0
23.25	7.71	7.7	0.0	23.25	8.39	8.4	0.0	23.25	7.73	7.7	0.0
23.51	7.80	7.7	0.1	23.51	8.42	8.4	0.0	23.51	7.79	7.8	0.0
23.78	7.90	7.8	0.1	23.78	8.49	8.4	0.1	23.78	7.81	7.8	0.0
24.05	7.77	7.8	0.0	24.05	8.65	8.5	0.2	24.05	7.83	7.9	0.0
24.31	7.69	7.9	-0.2	24.31	8.51	8.5	0.0	24.31	7.90	7.9	0.0
24.58	7.84	7.9	-0.1	24.58	8.56	8.5	0.0	24.58	7.96	7.9	0.0
24.85	7.93	8.0	0.0	24.85	8.58	8.6	0.0	24.85	8.02	8.0	0.0
25.11	8.00	8.0	0.0	25.11	8.61	8.6	0.0	25.11	8.07	8.0	0.0
25.38	8.04	8.0	0.0	25.38	8.96	8.6	0.3	25.38	8.07	8.1	0.0
25.64	8.05	8.1	0.0	25.64	8.67	8.7	0.0	25.64	8.09	8.1	0.0
25.91	8.12	8.1	0.0	25.91	8.70	8.7	0.0	25.91	8.13	8.2	0.0
26.18	8.24	8.2	0.1	26.18	8.75	8.7	0.0	26.18	8.18	8.2	0.0
26.44	8.23	8.2	0.0	26.44	8.79	8.7	0.0	26.44	8.22	8.2	0.0
26.71	8.27	8.2	0.0	26.71	8.77	8.8	0.0	26.71	8.29	8.3	0.0
26.98	8.34	8.3	0.1	26.98	8.84	8.8	0.0	26.98	8.32	8.3	0.0
27.25	8.36	8.3	0.0	27.25	8.81	8.8	0.0	27.25	8.33	8.3	0.0
27.51	8.33	8.4	0.0	27.51	8.87	8.9	0.0	27.51	8.39	8.4	0.0
27.78	8.39	8.4	0.0	27.78	8.88	8.9	0.0	27.78	8.40	8.4	0.0
28.05	8.46	8.4	0.0	28.05	8.92	8.9	0.0	28.05	8.44	8.5	0.0
28.31	8.45	8.5	0.0	28.31	8.94	9.0	0.0	28.31	8.49	8.5	0.0
28.58	8.50	8.5	0.0	28.58	8.98	9.0	0.0	28.58	8.51	8.5	0.0
28.85	8.58	8.5	0.0	28.85	9.10	9.0	0.1	28.85	8.55	8.6	0.0
29.11	8.54	8.6	0.0	29.11	9.07	9.0	0.0	29.11	8.60	8.6	0.0
29.38	8.60	8.6	0.0	29.38	9.11	9.1	0.0	29.38	8.64	8.6	0.0
29.64	8.67	8.6	0.0	29.64	9.11	9.1	0.0	29.64	8.68	8.7	0.0
29.91	8.65	8.7	0.0	29.91	9.10	9.1	0.0	29.91	8.71	8.7	0.0
30.18	8.80	8.7	0.1	30.18	9.15	9.1	0.0	30.18	8.74	8.7	0.0
30.44	8.83	8.8	0.1	30.44	9.19	9.2	0.0	30.44	8.79	8.8	0.0
30.71	8.77	8.8	0.0	30.71	9.18	9.2	0.0	30.71	8.83	8.8	0.0
30.98	8.84	8.8	0.0	30.98	9.15	9.2	-0.1	30.98	8.85	8.8	0.0
31.25	8.82	8.9	0.0	31.25	9.18	9.2	-0.1	31.25	8.93	8.9	0.1
31.51	8.85	8.9	0.0	31.51	9.19	9.3	-0.1	31.51	8.94	8.9	0.0
31.78	8.86	8.9	-0.1	31.78	9.20	9.3	-0.1	31.78	8.92	8.9	0.0
32.04	8.90	8.9	0.0	32.04	9.31	9.3	0.0	32.04	8.96	9.0	0.0
32.31	9.01	9.0	0.0	32.31	9.31	9.3	0.0	32.31	8.98	9.0	0.0
32.58	8.95	9.0	-0.1	32.58	9.40	9.4	0.0	32.58	9.00	9.0	0.0
32.85	9.02	9.0	0.0	32.85	9.33	9.4	-0.1	32.85	9.05	9.1	0.0
33.11	9.12	9.1	0.0	33.11	9.36	9.4	-0.1	33.11	9.07	9.1	0.0
33.38	9.06	9.1	0.0	33.38	9.39	9.4	0.0	33.38	9.10	9.1	0.0
33.64	9.19	9.1	0.1	33.64	9.44	9.5	0.0	33.64	9.15	9.1	0.0
33.91	9.13	9.2	0.0	33.91	9.47	9.5	0.0	33.91	9.18	9.2	0.0
34.18	9.27	9.2	0.1	34.18	9.57	9.5	0.1	34.18	9.21	9.2	0.0
34.45	9.29	9.2	0.1	34.45	9.53	9.5	0.0	34.45	9.21	9.2	0.0
34.71	9.28	9.2	0.0	34.71	9.58	9.5	0.0	34.71	9.24	9.3	0.0
34.98	9.30	9.3	0.0	34.98	9.58	9.6	0.0	34.98	9.29	9.3	0.0
35.25	9.22	9.3	-0.1	35.25	9.66	9.6	0.1	35.25	9.30	9.3	0.0
35.51	9.34	9.3	0.0	35.51	9.60	9.6	0.0	35.51	9.34	9.3	0.0
35.78	9.32	9.4	0.0	35.78	9.70	9.6	0.1	35.78	9.36	9.4	0.0
36.04	9.33	9.4	-0.1	36.04	9.85	9.7	0.2	36.04	9.38	9.4	0.0
36.31	9.38	9.4	0.0	36.31	9.79	9.7	0.1	36.31	9.41	9.4	0.0
36.58	9.38	9.4	-0.1	36.58	9.74	9.7	0.0	36.58	9.46	9.4	0.0
36.85	9.54	9.5	0.1	36.85	9.74	9.7	0.0	36.85	9.45	9.5	0.0
37.11	9.50	9.5	0.0	37.11	9.79	9.7	0.1	37.11	9.48	9.5	0.0
37.38	9.52	9.5	0.0	37.38	9.81	9.8	0.1	37.38	9.50	9.5	0.0
37.64	9.53	9.5	0.0	37.64	9.84	9.8	0.1	37.64	9.54	9.5	0.0
37.91	9.65	9.6	0.1	37.91	9.76	9.8	0.0	37.91	9.57	9.6	0.0
38.18	9.63	9.6	0.0	38.18	9.84	9.8	0.0	38.18	9.58	9.6	0.0
38.45	9.67	9.6	0.1	38.45	9.78	9.8	0.0	38.45	9.61	9.6	0.0
38.71	9.73	9.6	0.1	38.71	9.82	9.8	0.0	38.71	9.62	9.6	0.0
38.98	9.63	9.7	0.0	38.98	9.91	9.9	0.0	38.98	9.64	9.7	0.0
39.25	9.58	9.7	-0.1	39.25	9.88	9.9	0.0	39.25	9.66	9.7	0.0
39.51	9.66	9.7	0.0	39.51	9.94	9.9	0.0	39.51	9.69	9.7	0.0
39.78	9.66	9.7	-0.1	39.78	9.97	9.9	0.1	39.78	9.71	9.7	0.0
40.04	9.71	9.8	0.0	40.04	9.99	9.9	0.1	40.04	9.73	9.7	0.0
40.31	9.76	9.8	0.0	40.31	9.96	10.0	0.0	40.31	9.78	9.8	0.0
40.58	9.86	9.8	0.1	40.58	10.00	10.0	0.0	40.58	9.79	9.8	0.0
40.85	9.83	9.8	0.0	40.85	9.98	10.0	0.0	40.85	9.79	9.9	0.0
41.11	9.78	9.8	-0.1	41.11	10.00	10.0	0.0	41.11	9.83	9.8	0.0
41.38	9.82	9.9	0.0	41.38	10.05	10.0	0.0	41.38	9.88	9.9	0.0

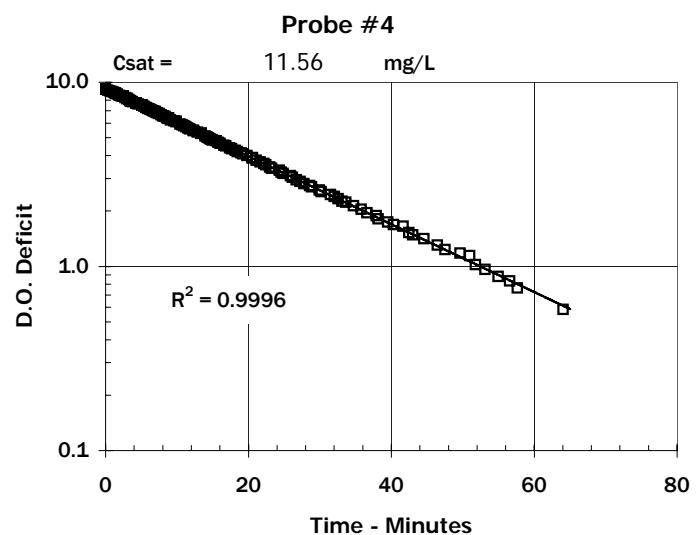
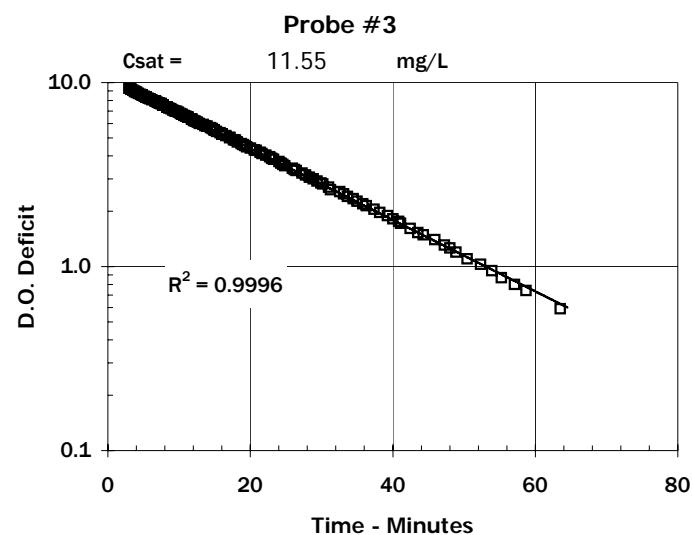
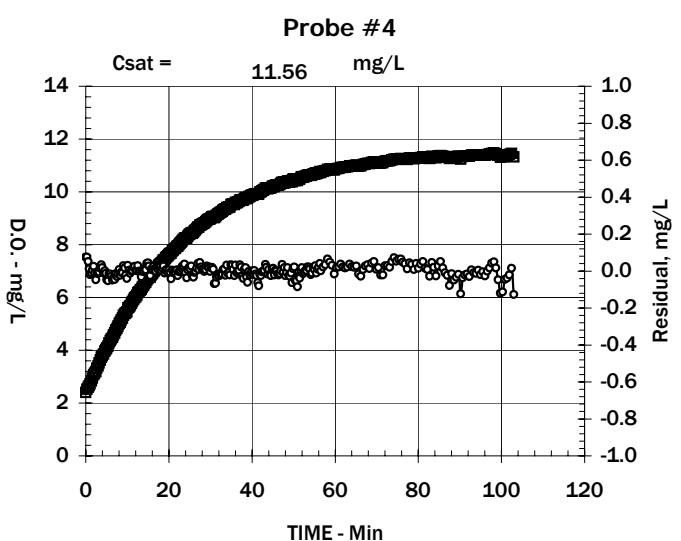
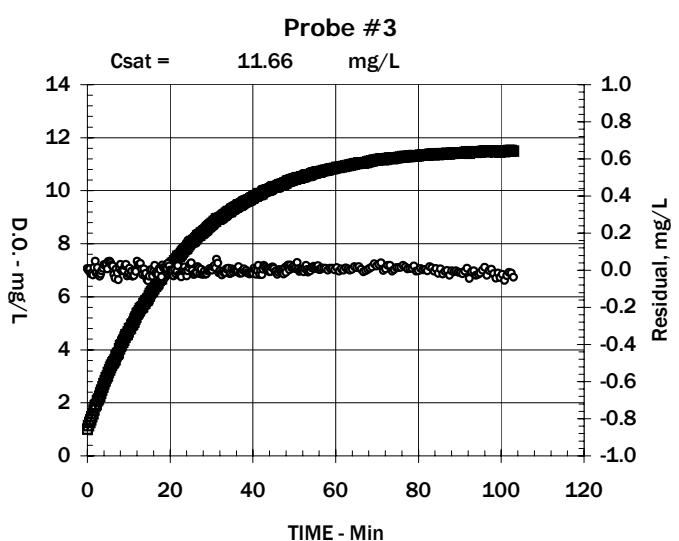
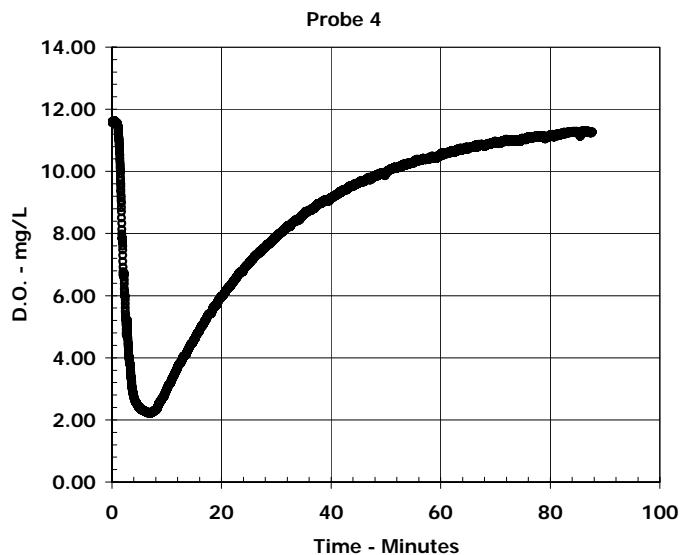
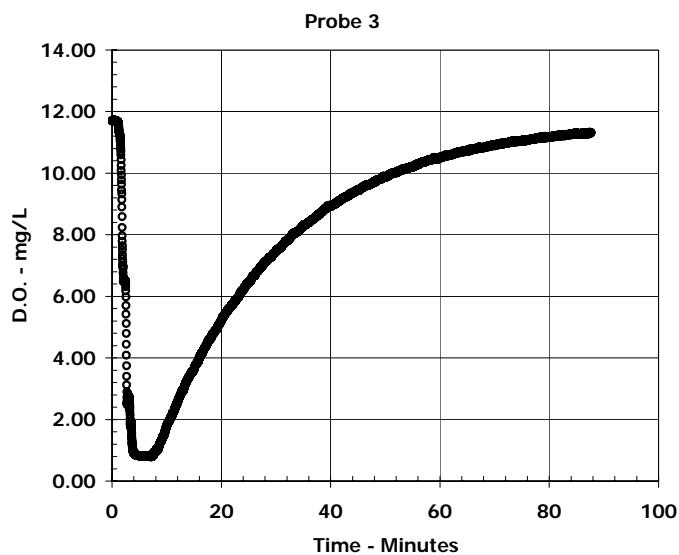
Pt. 1	est.	calc.	Pt. 2	est.	calc.	Pt. 3	est.	calc.	Pt. 4	est.	calc.				
CO	0.78	0.78	CO	3.21	3.21	CO	0.99	0.99	CO	2.32	2.32				
Kla-in	2.58	2.58	Kla-in	2.51	2.51	Kla-in	2.58	2.58	Kla-in	2.55	2.55				
C*	11.70	11.70	C*	11.49	11.49	C*	11.66	11.66	C*	11.56	11.56				
Sq.Dif.	0.0700		Sq.Dif.	2.9772		Sq.Dif.	0.1171		Sq.Dif.	0.2961					
Time	D.O.	D.O.calc	diff	Time	D.O.	D.O.calc	diff	Time	D.O.	D.O.calc	diff				
41.64	9.87	9.9	0.0	41.64	9.95	10.0	-0.1	41.64	9.85	9.9	0.0	41.64	9.91	10.0	-0.1
41.91	9.83	9.9	-0.1	41.91	10.03	10.1	0.0	41.91	9.89	9.9	0.0	41.91	9.99	10.0	0.0
42.18	9.89	9.9	0.0	42.18	10.16	10.1	0.1	42.18	9.89	9.9	0.0	42.18	10.00	10.0	0.0
42.45	9.95	9.9	0.0	42.45	10.16	10.1	0.1	42.45	9.94	9.9	0.0	42.45	10.04	10.0	0.0
42.71	9.97	10.0	0.0	42.71	10.24	10.1	0.1	42.71	9.98	10.0	0.0	42.71	10.06	10.1	0.0
42.98	10.09	10.0	0.1	42.98	10.21	10.1	0.1	42.98	9.99	10.0	0.0	42.98	10.08	10.1	0.0
43.25	10.14	10.0	0.1	43.25	10.14	10.1	0.0	43.25	10.00	10.0	0.0	43.25	10.13	10.1	0.0
43.51	10.05	10.0	0.0	43.51	10.24	10.1	0.1	43.51	10.02	10.0	0.0	43.51	10.13	10.1	0.0
43.78	10.08	10.0	0.0	43.78	10.26	10.2	0.1	43.78	10.03	10.0	0.0	43.78	10.11	10.1	0.0
44.04	10.03	10.1	0.0	44.04	10.10	10.2	-0.1	44.04	10.04	10.0	0.0	44.04	10.15	10.1	0.0
44.31	10.08	10.1	0.0	44.31	10.24	10.2	0.0	44.31	10.06	10.1	0.0	44.31	10.14	10.2	0.0
44.58	10.02	10.1	-0.1	44.58	10.20	10.2	0.0	44.58	10.10	10.1	0.0	44.58	10.15	10.2	0.0
44.85	10.13	10.1	0.0	44.85	10.18	10.2	0.0	44.85	10.12	10.1	0.0	44.85	10.20	10.2	0.0
45.11	10.14	10.1	0.0	45.11	10.20	10.2	0.0	45.11	10.13	10.1	0.0	45.11	10.22	10.2	0.0
45.38	10.21	10.2	0.1	45.38	10.32	10.2	0.1	45.38	10.13	10.1	0.0	45.38	10.20	10.2	0.0
45.64	10.18	10.2	0.0	45.64	10.21	10.3	-0.1	45.64	10.15	10.2	0.0	45.64	10.24	10.2	0.0
45.91	10.21	10.2	0.0	45.91	10.27	10.3	0.0	45.91	10.15	10.2	0.0	45.91	10.25	10.3	0.0
46.18	10.15	10.2	-0.1	46.18	10.34	10.3	0.1	46.18	10.18	10.2	0.0	46.18	10.25	10.3	0.0
46.45	10.36	10.2	0.1	46.45	10.32	10.3	0.0	46.45	10.21	10.2	0.0	46.45	10.26	10.3	0.0
46.71	10.31	10.2	0.1	46.71	10.32	10.3	0.0	46.71	10.22	10.2	0.0	46.71	10.28	10.3	0.0
46.98	10.30	10.3	0.0	46.98	10.35	10.3	0.0	46.98	10.23	10.2	0.0	46.98	10.31	10.3	0.0
47.25	10.27	10.3	0.0	47.25	10.35	10.3	0.0	47.25	10.24	10.3	0.0	47.25	10.36	10.3	0.0
47.51	10.28	10.3	0.0	47.51	10.42	10.4	0.1	47.51	10.25	10.3	0.0	47.51	10.33	10.3	0.0
47.78	10.33	10.3	0.0	47.78	10.36	10.4	0.0	47.78	10.30	10.3	0.0	47.78	10.37	10.4	0.0
48.04	10.42	10.3	0.1	48.04	10.50	10.4	0.1	48.04	10.29	10.3	0.0	48.04	10.34	10.4	0.0
48.31	10.40	10.3	0.1	48.31	10.41	10.4	0.0	48.31	10.34	10.3	0.0	48.31	10.37	10.4	0.0
48.58	10.43	10.4	0.1	48.58	10.47	10.4	0.1	48.58	10.36	10.3	0.0	48.58	10.41	10.4	0.0
48.85	10.48	10.4	0.1	48.85	10.44	10.4	0.0	48.85	10.35	10.3	0.0	48.85	10.38	10.4	0.0
49.11	10.42	10.4	0.0	49.11	10.45	10.4	0.0	49.11	10.39	10.4	0.0	49.11	10.39	10.4	0.0
49.38	10.42	10.4	0.0	49.38	10.48	10.4	0.0	49.38	10.39	10.4	0.0	49.38	10.42	10.4	0.0
49.64	10.54	10.4	0.1	49.64	10.46	10.5	0.0	49.64	10.41	10.4	0.0	49.64	10.38	10.4	-0.1
49.91	10.44	10.4	0.0	49.91	10.46	10.5	0.0	49.91	10.43	10.4	0.0	49.91	10.47	10.5	0.0
50.18	10.44	10.4	0.0	50.18	10.48	10.5	0.0	50.18	10.43	10.4	0.0	50.18	10.49	10.5	0.0
50.45	10.42	10.5	0.0	50.45	10.52	10.5	0.0	50.45	10.45	10.4	0.0	50.45	10.43	10.5	-0.1
50.71	10.51	10.5	0.0	50.71	10.45	10.5	0.0	50.71	10.49	10.4	0.0	50.71	10.44	10.5	-0.1
50.98	10.50	10.5	0.0	50.98	10.50	10.5	0.0	50.98	10.47	10.5	0.0	50.98	10.42	10.5	-0.1
51.25	10.53	10.5	0.0	51.25	10.51	10.5	0.0	51.25	10.47	10.5	0.0	51.25	10.49	10.5	0.0
51.51	10.54	10.5	0.0	51.51	10.53	10.5	0.0	51.51	10.49	10.5	0.0	51.51	10.49	10.5	0.0
51.78	10.43	10.5	-0.1	51.78	10.57	10.5	0.0	51.78	10.51	10.5	0.0	51.78	10.54	10.5	0.0
52.04	10.52	10.5	0.0	52.04	10.56	10.5	0.0	52.04	10.52	10.5	0.0	52.04	10.57	10.6	0.0
52.31	10.55	10.6	0.0	52.31	10.59	10.6	0.0	52.31	10.52	10.5	0.0	52.31	10.55	10.6	0.0
52.58	10.67	10.6	0.1	52.58	10.56	10.6	0.0	52.58	10.55	10.5	0.0	52.58	10.57	10.6	0.0
52.85	10.48	10.6	-0.1	52.85	10.60	10.6	0.0	52.85	10.58	10.6	0.0	52.85	10.59	10.6	0.0
53.11	10.59	10.6	0.0	53.11	10.62	10.6	0.0	53.11	10.57	10.6	0.0	53.11	10.60	10.6	0.0
53.38	10.63	10.6	0.0	53.38	10.59	10.6	0.0	53.38	10.57	10.6	0.0	53.38	10.63	10.6	0.0
53.64	10.55	10.6	-0.1	53.64	10.60	10.6	0.0	53.64	10.59	10.6	0.0	53.64	10.64	10.6	0.0
53.91	10.61	10.6	0.0	53.91	10.58	10.6	0.0	53.91	10.60	10.6	0.0	53.91	10.64	10.6	0.0
54.18	10.54	10.6	-0.1	54.18	10.64	10.6	0.0	54.18	10.63	10.6	0.0	54.18	10.62	10.6	0.0
54.45	10.59	10.7	-0.1	54.45	10.67	10.6	0.0	54.45	10.64	10.6	0.0	54.45	10.64	10.7	0.0
54.71	10.66	10.7	0.0	54.71	10.63	10.6	0.0	54.71	10.66	10.6	0.0	54.71	10.68	10.7	0.0
54.98	10.76	10.7	0.1	54.98	10.69	10.7	0.0	54.98	10.66	10.7	0.0	54.98	10.68	10.7	0.0
55.25	10.70	10.7	0.0	55.25	10.73	10.7	0.1	55.25	10.68	10.7	0.0	55.25	10.71	10.7	0.0
55.51	10.65	10.7	0.0	55.51	10.68	10.7	0.0	55.51	10.69	10.7	0.0	55.51	10.68	10.7	0.0
55.78	10.74	10.7	0.0	55.78	10.70	10.7	0.0	55.78	10.71	10.7	0.0	55.78	10.71	10.7	0.0
56.04	10.70	10.7	0.0	56.04	10.67	10.7	0.0	56.04	10.70	10.7	0.0	56.04	10.73	10.7	0.0
56.31	10.74	10.7	0.0	56.31	10.66	10.7	0.0	56.31	10.71	10.7	0.0	56.31	10.76	10.7	0.0
56.58	10.63	10.7	-0.1	56.58	10.77	10.7	0.1	56.58	10.73	10.7	0.0	56.58	10.73	10.7	0.0
57.11	10.66	10.8	-0.1	57.11	10.71	10.7	0.0	57.11	10.75	10.7	0.0	57.11	10.77	10.7	0.0
57.64	10.65	10.8	-0.1	57.64	10.80	10.7	0.1	57.64	10.77	10.8	0.0	57.64	10.80	10.8	0.0
58.18	10.88	10.8	0.1	58.18	10.83	10.8	0.1	58.18	10.78	10.8	0.0	58.18	10.85	10.8	0.1
58.71	10.92	10.8	0.1	58.71	10.80	10.8	0.0	58.71	10.81	10.8	0.0	58.71	10.85	10.8	0.0
59.25	10.91	10.8	0.1	59.25	10.81	10.8	0.0	59.25	10.83	10.8	0.0	59.25	10.85	10.8	0.0
59.78	10.91	10.9	0.0	59.78	10.82	10.8	0.0	59.78	10.84	10.8	0.0	59.78	10.82	10.8	0.0
60.31	10.85	10.9	0.0	60.31	10.82	10.8	0.0	60.31	10.87	10.9	0.0	60.31	10.87	10.9	0.0
60.85	10.87	10.9	0.0	60.85	10.84	10.8	0.0	60.85	10.87	10.9	0.0	60.85	10.89	10.9	0.0
61.38	10.81	10.9	-0.1	61.38	10.85	10.9	0.0	61.38	10.90	10.9	0.0	61.38	10.92	10.9	0.0
61.91	10.85	10.9	-0.1	61.91	10.87	10.9	0.0	61.91	10.91	10.9	0.0	61.91	10.92	10.9	0.0
62.45	10.92	11.0	0.0	62.45	10.91	10.9	0.0	62.45	10.94	10.9	0.0	62.45	10.93	10.9	

Pt. 1	est.	calc.	Pt. 2	est.	calc.	Pt. 3	est.	calc.	Pt. 4	est.	calc.
CO	0.78	0.78	CO	3.21	3.21 <th>CO</th> <td>0.99</td> <td>0.99</td> <th>CO</th> <td>2.32</td> <td>2.32</td>	CO	0.99	0.99	CO	2.32	2.32
Kla-in	2.58	2.58	Kla-in	2.51	2.51 <th>Kla-in</th> <td>2.58</td> <td>2.58</td> <th>Kla-in</th> <td>2.55</td> <td>2.55</td>	Kla-in	2.58	2.58	Kla-in	2.55	2.55
C*	11.70	11.70	C*	11.49	11.49 <th>C*</th> <td>11.66</td> <td>11.66</td> <th>C*</th> <td>11.56</td> <td>11.56</td>	C*	11.66	11.66	C*	11.56	11.56
Sq.Dif.	1.0700		Sq.Dif.	2.9772		Sq.Dif.	0.1171		Sq.Dif.	0.2961	
Time	D.O.	D.O.calc	diff	Time	D.O.	D.O.calc	diff	Time	D.O.	D.O.calc	diff
68.31	11.19	11.1	0.1	68.31	11.01	11.0	0.0	68.31	11.10	11.1	0.0
68.84	11.20	11.1	0.1	68.84	11.05	11.0	0.0	68.84	11.12	11.1	0.0
69.38	11.16	11.2	0.0	69.38	11.07	11.0	0.0	69.38	11.15	11.1	0.0
69.91	11.25	11.2	0.1	69.91	11.10	11.0	0.1	69.91	11.15	11.1	0.0
70.45	11.04	11.2	-0.1	70.45	11.15	11.1	0.1	70.45	11.17	11.1	0.0
70.98	11.17	11.2	0.0	70.98	11.14	11.1	0.1	70.98	11.19	11.2	0.0
71.51	11.24	11.2	0.0	71.51	11.05	11.1	0.0	71.51	11.16	11.2	0.0
72.04	11.26	11.2	0.1	72.04	11.08	11.1	0.0	72.04	11.18	11.2	0.0
72.58	11.34	11.2	0.1	72.58	11.12	11.1	0.0	72.58	11.21	11.2	0.0
73.11	11.29	11.2	0.1	73.11	11.10	11.1	0.0	73.11	11.22	11.2	0.0
73.65	11.33	11.2	0.1	73.65	11.16	11.1	0.1	73.65	11.20	11.2	0.0
74.18	11.33	11.3	0.1	74.18	11.13	11.1	0.0	74.18	11.22	11.2	0.1
74.71	11.34	11.3	0.1	74.71	11.14	11.1	0.0	74.71	11.24	11.2	0.1
75.25	11.28	11.3	0.0	75.25	11.12	11.1	0.0	75.25	11.25	11.2	0.1
75.78	11.44	11.3	0.2	75.78	11.22	11.1	0.1	75.78	11.26	11.2	0.0
76.31	11.22	11.3	-0.1	76.31	11.20	11.1	0.1	76.31	11.28	11.3	0.0
76.84	11.40	11.3	0.1	76.84	11.13	11.2	0.0	76.84	11.28	11.3	0.0
77.38	11.29	11.3	0.0	77.38	11.17	11.2	0.0	77.38	11.28	11.3	0.0
77.91	11.33	11.3	0.0	77.91	11.15	11.2	0.0	77.91	11.29	11.3	0.0
78.45	11.36	11.3	0.0	78.45	11.15	11.2	0.0	78.45	11.30	11.3	0.0
78.98	11.36	11.3	0.0	78.98	11.18	11.2	0.0	78.98	11.32	11.3	0.0
79.51	11.30	11.3	0.0	79.51	11.16	11.2	0.0	79.51	11.30	11.3	0.0
80.04	11.27	11.4	-0.1	80.04	11.24	11.2	0.0	80.04	11.31	11.3	0.0
80.58	11.30	11.4	-0.1	80.58	11.22	11.2	0.0	80.58	11.33	11.3	0.0
81.11	11.35	11.4	0.0	81.11	11.25	11.2	0.0	81.11	11.33	11.3	0.1
81.65	11.35	11.4	0.0	81.65	11.22	11.2	0.0	81.65	11.34	11.3	0.0
82.18	11.40	11.4	0.0	82.18	11.25	11.2	0.0	82.18	11.34	11.3	0.0
82.71	11.40	11.4	0.0	82.71	11.20	11.2	0.0	82.71	11.37	11.4	0.0
83.25	11.44	11.4	0.0	83.25	11.21	11.2	0.0	83.25	11.37	11.4	0.0
83.78	11.45	11.4	0.0	83.78	11.22	11.2	0.0	83.78	11.36	11.4	0.0
84.31	11.33	11.4	-0.1	84.31	11.21	11.2	0.0	84.31	11.38	11.4	0.0
84.84	11.36	11.4	-0.1	84.84	11.23	11.3	0.0	84.84	11.36	11.4	0.0
85.38	11.35	11.4	-0.1	85.38	11.35	11.3	0.1	85.38	11.39	11.4	0.0
85.91	11.31	11.4	-0.1	85.91	11.28	11.3	0.0	85.91	11.37	11.4	0.0
86.45	11.42	11.4	0.0	86.45	11.24	11.3	0.0	86.45	11.39	11.4	0.0
86.98	11.49	11.4	0.0	86.98	11.26	11.3	0.0	86.98	11.40	11.4	0.0
87.51	11.41	11.4	0.0	87.51	11.20	11.3	-0.1	87.51	11.38	11.4	0.0
88.04	11.39	11.5	-0.1	88.04	11.25	11.3	0.0	88.04	11.41	11.4	0.0
88.58	11.52	11.5	0.1	88.58	11.22	11.3	-0.1	88.58	11.41	11.4	0.0
89.11	11.43	11.5	0.0	89.11	11.26	11.3	0.0	89.11	11.42	11.4	0.0
89.65	11.54	11.5	0.1	89.65	11.29	11.3	0.0	89.65	11.42	11.4	0.0
90.18	11.52	11.5	0.0	90.18	11.30	11.3	0.0	90.18	11.42	11.4	-0.1
90.71	11.41	11.5	-0.1	90.71	11.24	11.3	-0.1	90.71	11.42	11.4	0.0
91.25	11.55	11.5	0.1	91.25	11.27	11.3	0.0	91.25	11.44	11.4	0.0
91.78	11.42	11.5	-0.1	91.78	11.24	11.3	-0.1	91.78	11.46	11.4	0.0
92.31	11.49	11.5	0.0	92.31	11.23	11.3	-0.1	92.31	11.41	11.5	0.0
92.84	11.38	11.5	-0.1	92.84	11.24	11.3	-0.1	92.84	11.45	11.5	0.0
93.38	11.61	11.5	0.1	93.38	11.29	11.3	0.0	93.38	11.46	11.5	0.0
93.91	11.35	11.5	-0.2	93.91	11.26	11.3	-0.1	93.91	11.44	11.5	0.0
94.45	11.62	11.5	0.1	94.45	11.29	11.3	0.0	94.45	11.45	11.5	0.0
94.98	11.50	11.5	0.0	94.98	11.27	11.3	-0.1	94.98	11.46	11.5	0.0
95.51	11.55	11.5	0.0	95.51	11.33	11.3	0.0	95.51	11.48	11.5	0.0
96.04	11.52	11.5	0.0	96.04	11.27	11.3	-0.1	96.04	11.50	11.5	0.0
96.58	11.41	11.5	-0.1	96.58	11.28	11.3	-0.1	96.58	11.46	11.5	0.0
97.11	11.51	11.5	0.0	97.11	11.27	11.3	-0.1	97.11	11.49	11.5	0.0
97.65	11.53	11.5	0.0	97.65	11.31	11.4	0.0	97.65	11.50	11.5	0.0
98.18	11.64	11.5	0.1	98.18	11.38	11.4	0.0	98.18	11.48	11.5	0.0
98.71	11.45	11.5	-0.1	98.71	11.28	11.4	-0.1	98.71	11.46	11.5	0.0
99.25	11.60	11.5	0.1	99.25	11.38	11.4	0.0	99.25	11.49	11.5	0.0
99.78	11.66	11.6	0.1	99.78	11.38	11.4	0.0	99.78	11.47	11.5	-0.1
100.31	11.45	11.6	-0.1	100.31	11.36	11.4	0.0	100.31	11.49	11.5	0.0
100.84	11.50	11.6	-0.1	100.84	11.26	11.4	-0.1	100.84	11.46	11.5	-0.1
101.38	11.45	11.6	-0.1	101.38	11.32	11.4	-0.1	101.38	11.49	11.5	0.0
101.91	11.63	11.6	0.1	101.91	11.27	11.4	-0.1	101.91	11.51	11.5	0.0
102.45	11.53	11.6	0.0	102.45	11.23	11.4	-0.1	102.45	11.51	11.5	0.0
102.98	11.49	11.6	-0.1	102.98	11.30	11.4	-0.1	102.98	11.49	11.5	0.0

Probe 1			Probe 2			Probe 3			Probe 4		
Lower	8.37%	Upper	Lower	28.02%	Upper	Lower	8.58%	Upper	Lower	20.76%	Upper
Value	Abs.Un.	%LSE	Value	Abs.Un.	%LSE	Value	Abs.Un.	%LSE	Value	Abs.Un.	%LSE
C*	11.703	0.009	0.076	C*	11.491	0.015	0.133	C*	11.656	0.003	0.025
CO	0.775	0.014	1.816	CO	3.212	0.023	0.724	CO	0.991	0.005	0.470
KLaT	2.581	0.000	0.307	KLaT	2.506	0.000	0.683	KLaT	2.578	0.000	0.104
Error	0.060		Error	0.100		Error	0.020		Error	0.032	
PROJECT:	PHi - Membrane Tube Diffusers + PHi Pumping										
DATE:	11/8/2006										
RUN:	3.00										



Project: PHi - Membrane Tube Diffusers + PHi Pumping
 Date: Nov 08, 2006
 Run: 3



Project: PHi - Membrane Tube Diffusers + PHi Pumping
 Date: Nov 08, 2006
 Run: 3

AIR FLOW RATE DETERMINATION

ANR 73 COMMERCIAL ANNubar - Diffused Air System

PROJECT : PHi - Membrane Tube Diffusers + PHi Pumping

$$\text{SCFM} = \frac{\text{C}''}{\frac{[\text{BP} + \text{LP}]}{[\text{LT} + 460]}}$$

$$\begin{aligned}\text{C}' &= \text{Fna} * \text{k} * \text{D}^2 * \text{Fra} * \text{Fpb} * \text{Ftb} * \text{Fg} * \text{Fpv} * \text{Faa} * \text{Fl} * \text{Fm} * \text{Ya} \\ \text{C}'' &= \text{C}' \text{ VALUE CORRECTED FOR HUMIDITY}\end{aligned}$$

RUN # 3
DATE Nov-06

OPERATING CONDITIONS

ANNUBAR TYPE		AWR-73		
BAROMETRIC PRESSURE	* BP	14.18 2 PSIA		
LINE PRESSURE	* LP	8.87 PSIG		
LINE TEMPERATURE	* LT	136 °F		
DIFFERENTIAL PRESSURE	* ^H	0.02 In. H2O		
RELATIVE HUMIDITY	* RH	64% %		
AMBIENT TEMPERATURE	*	15.5	64 °F	
PIPE INSIDE DIAMETER	* D	4.026 In.		

UNITS CONVERSION FACTOR	Fna	128.520
ANNUBAR FLOW COEFFICIENT	k	0.746
SQUARE OF PIPE ID	D^2	16.209
BASE PRESSURE		14.700 PSIA
BASE PRESSURE FACTOR	Fpb	1.002
BASE TEMPERATURE		68.000 °F
BASE TEMPERATURE FACTOR	Ftb	1.015
THERMAL EXPANSION FACTOR	Faa	1.002
MANOMETER LOCATION FACTOR	Fl	1.000
HG MANOMETER CORRECTION FACTOR	Fm	1.000
REYNOLD NUMBER	Rd	14,610.3
FLOWING VISCOSITY	vis	0.020 cP
REYNOLD NUMBER FACTOR	Fra	0.965
SPECIFIC GRAVITY	g	1.000
SPECIFIC GRAVITY FACTOR	Fg	1.000
SUPERCOMPRESSIBILTY	z	1.000
SUPERCOMPRESSIBILTY FACTOR	Fpv	1.000
GAS EXPANSION FACTOR	Ya	1.000
SCFM UNCORRECTED FOR HUMIDITY	SCFM	40.3
C'		1,527.70

VAPOR PRESSURE OF WATER AMB. TEMP.	VP	0.301
ACTUAL CUBIC FEET PER MINUTE	ACFM	29.0 328.2
HUMIDITY CORRECTED STANDARD AIR FLOW	SCFM	40.1 @68°F, 36% RH, 14.7 PSIA
INLET CUBIC FEET PER MINUTE	ICFM	47.1
C"		1,518.75

FORMULAS AND FACTORS DERIVED FROM: L.K.Spink: "Principles and Practice of FLOW METER ENGINEERING"; Ninth Ed., Nov 1975; The FOXBORO CO., Foxboro, Mass.
"ORIFICE FLOW METER"; THE BRISTOL COMPANY; Waterbury, Conn.

"ANNUBAR FLOW HANDBOOK"; August 1978; DIETERICH STANDARD CORPORATION; Boulder, Co.

HUMIDITY CORRECTED AIR FLOW DETERMINED per: "ASCE STANDARD Measurement of Oxygen Transfer in Clean Water"; ANNEX A; July 1984; American Society of Civil Engineers

AIR FLOW RATE DETERMINATION

ANR 73 COMMERCIAL ANNubar - Phi Mixing System

PROJECT : PHI

SCFM =

C"

$$\frac{[BP + LP]}{[LT + 460]}$$

C' = $F_{na} * k * D^2 * F_{ra} * F_{pb} * F_{tb} * F_g * F_{pv} * F_{aa} * F_l * F_m * Y_a$
 C" = C' VALUE CORRECTED FOR HUMIDITY

RUN #
DATE

3 (Est. PHI Additional O2 Provided)

Nov-06

OPERATING CONDITIONS		AWR-73		
ANNubar Type				2
Barometric Pressure	* BP	14.18	PSIA	
Line Pressure	* LP	65.00	PSIG	
Line Temperature	* LT	64	°F	
Differential Pressure	* ^H	0.01	In. H2O	
Relative Humidity	* RH	64%	%	
Ambient Temperature	*	15.5	64	°F
Pipe Inside Diameter	* D	4.026	In.	
Units Conversion Factor	F _{na}	128.520		
Annubar Flow Coefficient	k	0.746		
Square of Pipe ID	D ²	16.209		
Base Pressure		14.700	PSIA	
Base Pressure Factor	F _{pb}	1.002		
Base Temperature		68.000	°F	
Base Temperature Factor	F _{tb}	1.015		
Thermal Expansion Factor	F _{aa}	1.001		
Manometer Location Factor	F _l	1.000		
Hg Manometer Correction Factor	F _m	1.000		
Reynold Number	R _d	17,566.8		
Flowing Viscosity	vis	0.018	cP	
Reynold Number Factor	F _{ra}	0.965		
Specific Gravity	g	1.000		
Specific Gravity Factor	F _g	1.000		
Supercompressibility	Z	0.997		
Supercompressibility Factor	F _{pv}	1.001		
Gas Expansion Factor	Y _a	1.000		
SCFM Uncorrected for Humidity	SCFM	43.9		
C'		1,527.74		
Vapor Pressure of Water Amb. Temp.	VP	0.301		
Actual Cubic Feet per Minute	ACFM	8.1	91.5	
Humidity Corrected Standard Air Flow	SCFM	43.6	@68°F, 36% RH, 14.7 PSIA	
Inlet Cubic Feet per Minute	ICFM	45.2		
C"		1,518.79		

FORMULAS AND FACTORS DERIVED FROM:

L.K.Spink; "Principles and Practice of FLOW METER ENGINEERING"; Ninth Ed., Nov 1975; The FOXBORO CO., Foxboro, Mass.

"ORIFICE FLOW METER"; THE BRISTOL COMPANY; Waterbury, Conn.

"ANNUBAR FLOW HANDBOOK"; August 1978; DIETERICH STANDARD CORPORATION; Boulder, Co.

HUMIDITY CORRECTED AIR FLOW DETERMINED per: "ASCE STANDARD Measurement of Oxygen Transfer in Clean Water"; ANNEX A; July 1984; American Society of Civil Engineers

ASCE OXYGEN TRANSFER DETERMINATION

PROJECT: Phi (Faster Valve Test)			599 Waldron Rd.	
DATE: 9-Nov-06			LaVergne, TN 37086	
RUN: 4			615/793-7547	
			FAX 615/793/5070	
	Initial	Mid Point	Final	
Barometric Pres. (PSIA) (mm Hg)	14.199 734.30	14.232 736.00	14.263 737.60	C' Air Flow Device 1 (Annubar) 1,518.30 Air Flow Device 1 (SCFM) 38.07
Ambient Temperature (°F)	73.90	67.90	61.90	C' Air Flow Device 2 (Orifice) 249.20 Air Flow Device 2 (SCFM) 37.80
Relative Humidity (%)	49%	57%	65%	
Line Pressure (PSIG) (In. Hg)	44.943 91.50	45.188 92.00	44.943 91.50	
Line Temperature (°F)	73.90	67.90	61.90	
ΔH Air Flow Dev. 1 (Annubar)	0.006	0.006	0.006	Average Air Flow (SCFM) 37.93
ΔH Air Flow Dev. 2 (Orifice)	0.205	0.205	0.205	Effective Depth Correction (f) 0.01
ΔH Air Flow Dev. 3 (Annubar)	NA	NA	NA	Headloss (In. H ₂ O) 1,015.35
ΔH Air Flow Dev. 4 (Annubar)	NA	NA	NA	
Water Temp. (°C)	14.93	14.95	14.99	C* (mg/l) 9.85
Orifice Diameter (in)		1.840		CsmT (Standard Methods, mg/l) 10.09
Number Of Aeration Devices		1		C* ₂₀ Standard Conditions 9.16
Side Water Depth (ft)		19.25	(5.85 m)	Tank Volume (Ft ³) 6,667.4
Air Release Depth (ft)		19.25	(5.85 m)	(Gallons) 49,875.9
Tank Length (ft)		0.00	(0.00 m)	(m ³) 188.8
Tank Width (ft)		0.00	(0.00 m)	(Million Pounds) 0.416
Tank Diameter (ft)		21.00	(6.38 m)	#Na ₂ SO ₃ @ 160% Stoichiometric 52
Gear Reducer or Belt Efficiency		100.0%		Cobalt Concen. (mg/l) 0.100
Motor Efficiency		93.0%		Grams Cobalt Chloride 77.9
Total HP _{wire} av.		5.80	(4.33 kw)	Total HP _{motor} av. 5.40
				TDS (mg/L) 676.00

NON-LINEAR REGRESSION RESULTS

Probe	K _{LAT}	K _{La20}	SOTR	SOTR/Dev	SOTE	SAE _{wire}	C*	Std. Err.
1	0.11	0.12	0.47	0.47	1.20	0.08	9.76	0.0852
2	0.11	0.13	0.47	0.47	1.20	0.08	9.71	0.0165
3	0.11	0.12	0.49	0.49	1.24	0.08	10.07	0.0089
4	0.11	0.12	0.47	0.47	1.20	0.08	9.86	0.0153
avg.	0.11	0.12	0.47	0.47	1.21	0.08	9.85	0.0315
Avg	0.11	0.12	0.47	0.47	1.20	0.08	9.81	Exclude Max&Min
TDS	0.11	0.13	0.49	0.49	1.25	0.08	9.85	0.06%
<i>Corrected</i>	/hr	/hr	#O2/hr		%	#O2/hr-WHP		

OXYGEN TRANSFER

Total SCFM:	37.9	:Nm ³ /Hr	17.903	L/s	#O2/Hr:	0.49	0.222	:KgO2/Hr
SCFM/Diff.:	37.93	:Nm ³ /hr/Diff		#O2/Hr/Diff.:	0.49	0.222	:KgO2/Hr/Diff.	
SCFM/KCF:	5.7	:Nm ³ /hr/m ³		#O2/Day:	11.7	5.3	:KgO2/Day	
Total ICFM:	39.5	18.65 L/s		#O2/Day/1000 Ft ³ :	2	0.03	:KgO2/Day/m ³	

LINEAR REGRESSION RESULTS

Probe	K _{LAT}	K _{La20}	SOTR	SOTR/Dev	SOTE	SAE _{wire}	C*	Corr. Coeff.
1	0.11	0.12	0.46	0.46	1.18	0.08	9.85	0.9990
2	0.11	0.12	0.46	0.46	1.16	0.08	9.87	0.9999
3	0.11	0.12	0.48	0.48	1.23	0.08	10.10	1.0000
4	0.11	0.12	0.47	0.47	1.20	0.08	9.86	0.9999
avg.	0.11	0.12	0.47	0.47	1.19	0.08	9.92	0.9997
Avg	0.11	0.12	0.47	0.47	1.19	0.08	9.87	Exclude Max&Min
TDS	0.11	0.13	0.48	0.48	1.23	0.08	9.92	
<i>Corrected</i>	/hr	/hr	#O2/hr		%	#O2/hr-HPw		

EUROPEAN STANDARD

Probe	K _{LAT}	K _{La10}	SOTR	SOTR/Dev	SAE	C*
1	0.11	0.10	0.21	0.21	0.05	9.76
2	0.11	0.10	0.21	0.21	0.05	9.71
3	0.11	0.10	0.22	0.22	0.05	10.07
4	0.11	0.10	0.21	0.21	0.05	9.86
avg.	0.11	0.10	0.21	0.21	0.05	9.85
Avg	0.11	0.10	0.21	0.21	0.05	9.81
TDS	0.11	0.10	0.22	0.22	0.05	9.85
<i>Corrected</i>	/hr	/hr	kg O ₂ /hr		kg O ₂ /hr-kw	mg/L

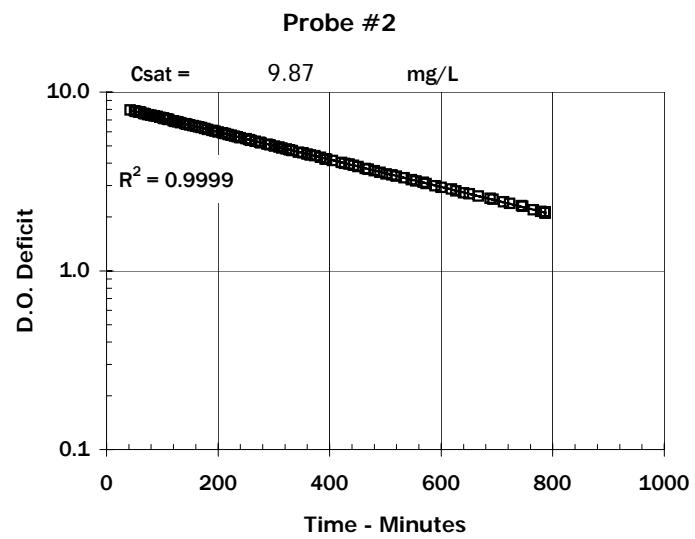
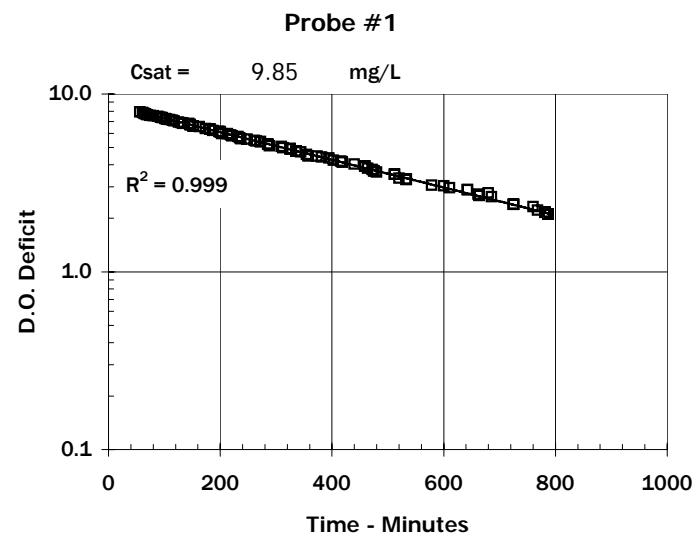
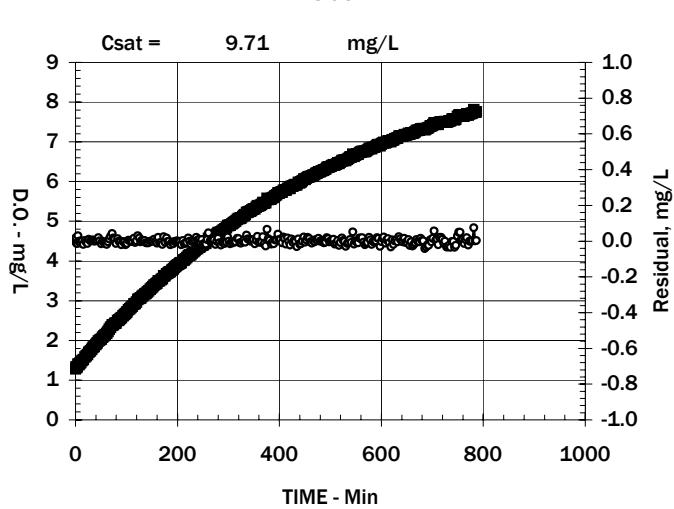
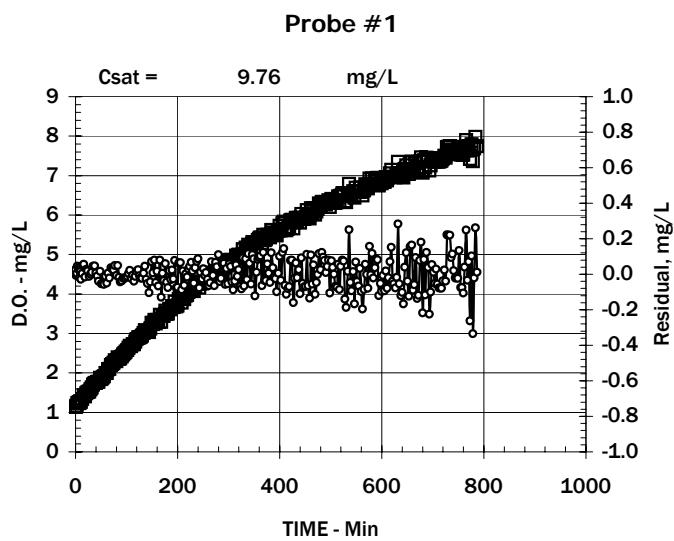
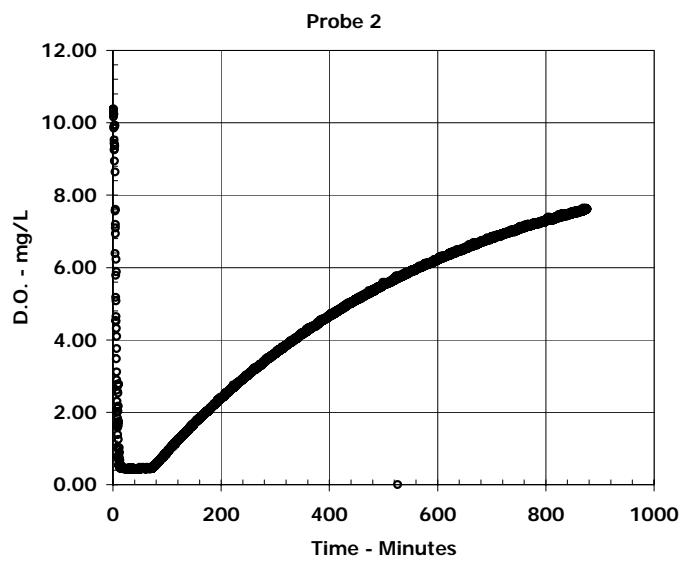
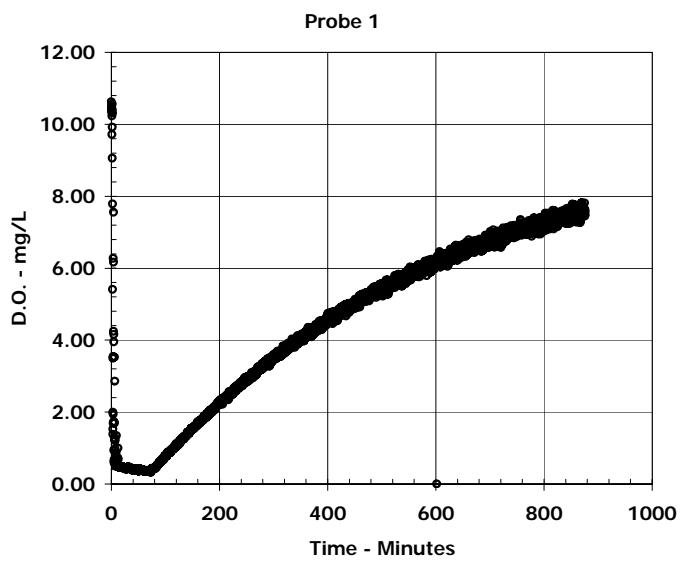
Pt. 1	est.	calc.	Pt. 2	est.	calc.	Pt. 3	est.	calc.	Pt. 4	est.	calc.
CO	1.12	1.12	CO	1.29	1.29	CO	0.96	0.96	CO	1.15	1.15
Kla-in	0.11	0.11	Kla-in	0.11	0.11	Kla-in	0.11	0.11	Kla-in	0.11	0.11
C*	9.76	9.76	C*	9.71	9.71	C*	10.07	10.07	C*	9.86	9.86
Sq.Dif.	2.1547		Sq.Dif.	0.0812		Sq.Dif.	0.0233		Sq.Dif.	0.0694	
Time	D.O.	D.O.calc	diff	Time	D.O.	D.O.calc	diff	Time	D.O.	D.O.calc	diff
0.00	1.15	1.1	0.0	0.00	1.28	1.3	0.0	0.00	0.96	1.0	0.0
1.33	1.14	1.1	0.0	1.33	1.33	1.3	0.0	1.33	0.98	1.0	0.0
2.67	1.17	1.2	0.0	2.67	1.32	1.3	0.0	2.67	0.99	1.0	0.0
4.00	1.23	1.2	0.0	4.00	1.34	1.4	0.0	4.00	1.04	1.0	0.0
5.33	1.24	1.2	0.0	5.33	1.40	1.4	0.0	5.33	1.06	1.0	0.0
6.67	1.25	1.2	0.0	6.67	1.39	1.4	0.0	6.67	1.06	1.1	0.0
8.00	1.23	1.3	0.0	8.00	1.41	1.4	0.0	8.00	1.08	1.1	0.0
9.33	1.28	1.3	0.0	9.33	1.43	1.4	0.0	9.33	1.11	1.1	0.0
10.67	1.26	1.3	0.0	10.67	1.44	1.5	0.0	10.67	1.12	1.1	0.0
13.33	1.34	1.3	0.0	13.33	1.49	1.5	0.0	13.33	1.18	1.2	0.0
16.00	1.43	1.4	0.1	16.00	1.51	1.5	0.0	16.00	1.22	1.2	0.0
18.67	1.40	1.4	0.0	18.67	1.58	1.6	0.0	18.67	1.25	1.3	0.0
21.33	1.48	1.5	0.0	21.33	1.609	1.6	0.0	21.33	1.31	1.3	0.0
24.00	1.51	1.5	0.0	24.00	1.64	1.7	0.0	24.00	1.37	1.4	0.0
26.67	1.53	1.5	0.0	26.67	1.703	1.7	0.0	26.67	1.41	1.4	0.0
29.33	1.58	1.6	0.0	29.33	1.734	1.7	0.0	29.33	1.42	1.4	0.0
32.00	1.63	1.6	0.0	32.00	1.776	1.8	0.0	32.00	1.46	1.5	0.0
34.67	1.70	1.7	0.0	34.67	1.818	1.8	0.0	34.67	1.51	1.5	0.0
37.33	1.74	1.7	0.0	37.33	1.85	1.9	0.0	37.33	1.55	1.6	0.0
40.00	1.74	1.7	0.0	40.00	1.89	1.9	0.0	40.00	1.62	1.6	0.0
42.67	1.77	1.8	0.0	42.67	1.93	1.9	0.0	42.67	1.66	1.6	0.0
45.33	1.78	1.8	0.0	45.33	1.98	2.0	0.0	45.33	1.69	1.7	0.0
48.00	1.87	1.9	0.0	48.00	2.01	2.0	0.0	48.00	1.74	1.7	0.0
50.67	1.84	1.9	-0.1	50.67	2.03	2.0	0.0	50.67	1.76	1.8	0.0
53.33	1.88	1.9	-0.1	53.33	2.08	2.1	0.0	53.33	1.81	1.8	0.0
56.00	1.91	2.0	-0.1	56.00	2.11	2.1	0.0	56.00	1.85	1.8	0.0
58.67	2.00	2.0	0.0	58.67	2.14	2.2	0.0	58.67	1.88	1.9	0.0
61.33	2.00	2.0	-0.1	61.33	2.17	2.2	0.0	61.33	1.92	1.9	0.0
64.00	2.09	2.1	0.0	64.00	2.23	2.2	0.0	64.00	1.96	2.0	0.0
66.67	2.10	2.1	0.0	66.67	2.28	2.3	0.0	66.67	2.01	2.0	0.0
69.33	2.19	2.2	0.0	69.33	2.33	2.3	0.0	69.33	2.05	2.0	0.0
72.00	2.23	2.2	0.0	72.00	2.38	2.3	0.0	72.00	2.09	2.1	0.0
74.67	2.26	2.2	0.0	74.67	2.39	2.4	0.0	74.67	2.13	2.1	0.0
77.33	2.32	2.3	0.0	77.33	2.42	2.4	0.0	77.33	2.17	2.2	0.0
80.00	2.30	2.3	0.0	80.00	2.43	2.4	0.0	80.00	2.21	2.2	0.0
82.67	2.39	2.3	0.0	82.67	2.50	2.5	0.0	82.67	2.25	2.2	0.0
85.33	2.36	2.4	0.0	85.33	2.52	2.5	0.0	85.33	2.28	2.3	0.0
88.00	2.37	2.4	0.0	88.00	2.55	2.6	0.0	88.00	2.32	2.3	0.0
90.67	2.41	2.5	0.0	90.67	2.57	2.6	0.0	90.67	2.36	2.4	0.0
93.33	2.47	2.5	0.0	93.33	2.62	2.6	0.0	93.33	2.39	2.4	0.0
96.00	2.50	2.5	0.0	96.00	2.65	2.7	0.0	96.00	2.44	2.4	0.0
98.67	2.54	2.6	0.0	98.67	2.67	2.7	0.0	98.67	2.48	2.5	0.0
101.33	2.58	2.6	0.0	101.33	2.72	2.7	0.0	101.33	2.52	2.5	0.0
104.00	2.63	2.6	0.0	104.00	2.77	2.8	0.0	104.00	2.55	2.5	0.0
106.67	2.68	2.7	0.0	106.67	2.80	2.8	0.0	106.67	2.58	2.6	0.0
109.33	2.67	2.7	0.0	109.33	2.83	2.8	0.0	109.33	2.63	2.6	0.0
112.00	2.73	2.7	0.0	112.00	2.86	2.9	0.0	112.00	2.64	2.7	0.0
114.67	2.73	2.8	0.0	114.67	2.91	2.9	0.0	114.67	2.70	2.7	0.0
117.33	2.79	2.8	0.0	117.33	2.93	2.9	0.0	117.33	2.73	2.7	0.0
120.00	2.85	2.8	0.0	120.00	2.97	3.0	0.0	120.00	2.75	2.8	0.0
122.67	2.89	2.9	0.0	122.67	3.03	3.0	0.0	122.67	2.79	2.8	0.0
125.33	2.89	2.9	0.0	125.33	3.05	3.0	0.0	125.33	2.83	2.8	0.0
128.00	2.91	2.9	0.0	128.00	3.06	3.1	0.0	128.00	2.86	2.9	0.0
130.67	2.95	3.0	0.0	130.67	3.10	3.1	0.0	130.67	2.88	2.9	0.0
133.33	3.01	3.0	0.0	133.33	3.13	3.1	0.0	133.33	2.95	2.9	0.0
136.00	3.08	3.0	0.0	136.00	3.17	3.2	0.0	136.00	2.99	3.0	0.0
138.67	3.04	3.1	0.0	138.67	3.19	3.2	0.0	138.67	3.01	3.0	0.0
141.33	3.05	3.1	-0.1	141.33	3.22	3.2	0.0	141.33	3.05	3.0	0.0
144.00	3.03	3.1	-0.1	144.00	3.25	3.3	0.0	144.00	3.08	3.1	0.0
146.67	3.12	3.2	0.0	146.67	3.29	3.3	0.0	146.67	3.11	3.1	0.0
149.33	3.27	3.2	0.1	149.33	3.32	3.3	0.0	149.33	3.15	3.1	0.0
152.00	3.24	3.2	0.0	152.00	3.35	3.4	0.0	152.00	3.18	3.2	0.0
154.67	3.34	3.3	0.1	154.67	3.40	3.4	0.0	154.67	3.22	3.2	0.0
157.33	3.25	3.3	0.0	157.33	3.42	3.4	0.0	157.33	3.27	3.2	0.0
160.00	3.34	3.3	0.0	160.00	3.44	3.4	0.0	160.00	3.28	3.3	0.0
162.67	3.29	3.4	-0.1	162.67	3.50	3.5	0.0	162.67	3.32	3.3	0.0
165.33	3.47	3.4	0.1	165.33	3.50	3.5	0.0	165.33	3.35	3.3	0.0
168.00	3.29	3.4	-0.1	168.00	3.53	3.5	0.0	168.00	3.40	3.4	0.0
170.67	3.46	3.5	0.0	170.67	3.55	3.6	0.0	170.67	3.41	3.4	0.0
173.33	3.45	3.5	0.0	173.33	3.63	3.6	0.0	173.33	3.44	3.4	0.0
176.00	3.57	3.5	0.1	176.00	3.63	3.6	0.0	176.00	3.48	3.5	0.0
178.67	3.50	3.5	0.0	178.67	3.68	3.7	0.0	178.67	3.50	3.5	0.0
181.33	3.50	3.6	-0.1	181.33	3.69	3.7	0.0	181.33	3.55	3.5	0.0
184.00	3.63	3.6	0.0	184.00	3.72	3.7	0.0	184.00	3.58	3.6	0.0
186.67	3.60	3.6	0.0	186.67	3.73	3.7	0.0	186.67	3.60	3.6	0.0
189.33	3.69	3.7	0.0	189.33	3.77	3.8	0.0	189.33	3.64	3.6	0.0
192.00	3.67	3.7	0.0	192.00	3.79	3.8	0.0	192.00	3.67	3.7	0.0
194.67	3.80	3.7	0.1	194.67	3.83	3.8	0.0	194.67	3.69	3.7	0.0

Pt. 1	est.	calc.	Pt. 2	est.	calc.	Pt. 3	est.	calc.	Pt. 4	est.	calc.
CO	1.12	1.12	CO	1.29	1.29	CO	0.96	0.96	CO	1.15	1.15
Kla-in	0.11	0.11	Kla-in	0.11	0.11	Kla-in	0.11	0.11	Kla-in	0.11	0.11
C*	9.76	9.76	C*	9.71	9.71 <th>C*</th> <td>10.07</td> <td>10.07</td> <th>C*</th> <td>9.86</td> <td>9.86</td>	C*	10.07	10.07	C*	9.86	9.86
Sq.Dif.	2.1547	Sq.Dif.	0.0812	Sq.Dif.	0.0233 <th>Sq.Dif.</th> <td>0.0694</td> <th>Sq.Dif.</th> <td>0.0694</td> <th>Sq.Dif.</th> <td>0.0694</td>	Sq.Dif.	0.0694	Sq.Dif.	0.0694	Sq.Dif.	0.0694
Time	D.O.	D.O.calc	diff	Time	D.O.	D.O.calc	diff	Time	D.O.	D.O.calc	diff
197.33	3.68	3.8	-0.1	197.33	3.87	3.9	0.0	197.33	3.72	3.7	0.0
200.00	3.71	3.8	-0.1	200.00	3.90	3.9	0.0	200.00	3.76	3.8	0.0
202.67	3.88	3.8	0.1	202.67	3.92	3.9	0.0	202.67	3.79	3.8	0.0
205.33	3.91	3.8	0.1	205.33	3.95	4.0	0.0	205.33	3.83	3.8	0.0
208.00	3.78	3.9	-0.1	208.00	3.96	4.0	0.0	208.00	3.85	3.9	0.0
210.67	3.92	3.9	0.0	210.67	4.01	4.0	0.0	210.67	3.88	3.9	0.0
213.33	3.87	3.9	-0.1	213.33	4.02	4.0	0.0	213.33	3.92	3.9	0.0
216.00	3.96	4.0	0.0	216.00	4.05	4.1	0.0	216.00	3.95	3.9	0.0
218.67	3.97	4.0	0.0	218.67	4.08	4.1	0.0	218.67	3.99	4.0	0.0
221.33	4.04	4.0	0.0	221.33	4.14	4.1	0.0	221.33	4.01	4.0	0.0
224.00	4.08	4.0	0.0	224.00	4.15	4.1	0.0	224.00	4.04	4.0	0.0
226.67	4.14	4.1	0.1	226.67	4.16	4.2	0.0	226.67	4.06	4.1	0.0
229.33	4.12	4.1	0.0	229.33	4.20	4.2	0.0	229.33	4.10	4.1	0.0
232.00	4.07	4.1	-0.1	232.00	4.23	4.2	0.0	232.00	4.13	4.1	0.0
234.67	4.19	4.2	0.0	234.67	4.26	4.3	0.0	234.67	4.16	4.2	0.0
237.33	4.25	4.2	0.1	237.33	4.30	4.3	0.0	237.33	4.19	4.2	0.0
240.00	4.29	4.2	0.1	240.00	4.31	4.3	0.0	240.00	4.21	4.2	0.0
242.67	4.16	4.2	-0.1	242.67	4.35	4.3	0.0	242.67	4.23	4.2	0.0
245.33	4.27	4.3	0.0	245.33	4.36	4.4	0.0	245.33	4.26	4.3	0.0
248.00	4.26	4.3	0.0	248.00	4.40	4.4	0.0	248.00	4.29	4.3	0.0
250.67	4.35	4.3	0.0	250.67	4.40	4.4	0.0	250.67	4.35	4.3	0.0
253.33	4.34	4.3	0.0	253.33	4.43	4.4	0.0	253.33	4.36	4.4	0.0
256.00	4.38	4.4	0.0	256.00	4.45	4.5	0.0	256.00	4.38	4.4	0.0
258.67	4.37	4.4	0.0	258.67	4.50	4.5	0.0	258.67	4.41	4.4	0.0
261.33	4.36	4.4	-0.1	261.33	4.57	4.5	0.0	261.33	4.45	4.4	0.0
264.00	4.40	4.4	0.0	264.00	4.54	4.5	0.0	264.00	4.47	4.5	0.0
266.67	4.54	4.5	0.1	266.67	4.58	4.6	0.0	266.67	4.49	4.5	0.0
269.33	4.49	4.5	0.0	269.33	4.60	4.6	0.0	269.33	4.50	4.5	0.0
272.00	4.46	4.5	-0.1	272.00	4.63	4.6	0.0	272.00	4.54	4.5	0.0
274.67	4.62	4.6	0.1	274.67	4.63	4.6	0.0	274.67	4.57	4.6	0.0
277.33	4.62	4.6	0.0	277.33	4.67	4.7	0.0	277.33	4.61	4.6	0.0
280.00	4.71	4.6	0.1	280.00	4.71	4.7	0.0	280.00	4.63	4.6	0.0
282.67	4.59	4.6	0.0	282.67	4.71	4.7	0.0	282.67	4.66	4.7	0.0
285.33	4.63	4.7	0.0	285.33	4.72	4.7	0.0	285.33	4.67	4.7	0.0
288.00	4.73	4.7	0.1	288.00	4.76	4.8	0.0	288.00	4.70	4.7	0.0
290.67	4.76	4.7	0.1	290.67	4.78	4.8	0.0	290.67	4.72	4.7	0.0
293.33	4.67	4.7	-0.1	293.33	4.81	4.8	0.0	293.33	4.75	4.8	0.0
296.00	4.78	4.8	0.0	296.00	4.84	4.8	0.0	296.00	4.78	4.8	0.0
298.67	4.72	4.8	-0.1	298.67	4.89	4.9	0.0	298.67	4.81	4.8	0.0
301.33	4.86	4.8	0.1	301.33	4.89	4.9	0.0	301.33	4.83	4.8	0.0
304.00	4.87	4.8	0.0	304.00	4.90	4.9	0.0	304.00	4.87	4.9	0.0
306.67	4.81	4.8	0.0	306.67	4.93	4.9	0.0	306.67	4.89	4.9	0.0
309.33	4.78	4.9	-0.1	309.33	4.95	5.0	0.0	309.33	4.92	4.9	0.0
312.00	4.86	4.9	0.0	312.00	4.98	5.0	0.0	312.00	4.93	4.9	0.0
314.67	4.97	4.9	0.1	314.67	5.00	5.0	0.0	314.67	4.97	5.0	0.0
317.33	4.93	4.9	0.0	317.33	5.05	5.0	0.0	317.33	4.99	5.0	0.0
320.00	4.99	5.0	0.0	320.00	5.07	5.1	0.0	320.00	5.01	5.0	0.0
322.67	4.92	5.0	-0.1	322.67	5.07	5.1	0.0	322.67	5.05	5.0	0.0
325.33	4.93	5.0	-0.1	325.33	5.09	5.1	0.0	325.33	5.08	5.1	0.0
328.00	5.13	5.0	0.1	328.00	5.12	5.1	0.0	328.00	5.08	5.1	0.0
330.67	4.99	5.1	-0.1	330.67	5.15	5.1	0.0	330.67	5.11	5.1	0.0
333.33	5.17	5.1	0.1	333.33	5.16	5.2	0.0	333.33	5.14	5.1	0.0
336.00	5.08	5.1	0.0	336.00	5.22	5.2	0.0	336.00	5.16	5.2	0.0
338.67	5.24	5.1	0.1	338.67	5.22	5.2	0.0	338.67	5.19	5.2	0.0
341.33	5.21	5.2	0.1	341.33	5.24	5.2	0.0	341.33	5.20	5.2	0.0
344.00	5.12	5.2	-0.1	344.00	5.25	5.3	0.0	344.00	5.23	5.2	0.0
346.67	5.31	5.2	0.1	346.67	5.29	5.3	0.0	346.67	5.25	5.3	0.0
349.33	5.31	5.2	0.1	349.33	5.31	5.3	0.0	349.33	5.29	5.3	0.0
352.00	5.12	5.2	-0.1	352.00	5.31	5.3	0.0	352.00	5.32	5.3	0.0
354.67	5.28	5.3	0.0	354.67	5.35	5.3	0.0	354.67	5.33	5.3	0.0
357.33	5.37	5.3	0.1	357.33	5.39	5.4	0.0	357.33	5.35	5.4	0.0
360.00	5.40	5.3	0.1	360.00	5.38	5.4	0.0	360.00	5.38	5.4	0.0
362.67	5.43	5.3	0.1	362.67	5.40	5.4	0.0	362.67	5.40	5.4	0.0
365.33	5.29	5.4	-0.1	365.33	5.42	5.4	0.0	365.33	5.42	5.4	0.0
368.00	5.50	5.4	0.1	368.00	5.47	5.5	0.0	368.00	5.44	5.4	0.0
370.67	5.36	5.4	0.0	370.67	5.45	5.5	0.0	370.67	5.45	5.5	0.0
373.33	5.38	5.4	0.0	373.33	5.46	5.5	0.0	373.33	5.51	5.5	0.0
376.00	5.50	5.4	0.1	376.00	5.58	5.5	0.1	376.00	5.51	5.5	0.0
378.67	5.46	5.5	0.0	378.67	5.55	5.5	0.0	378.67	5.53	5.5	0.0
381.33	5.43	5.5	0.0	381.33	5.56	5.6	0.0	381.33	5.56	5.5	0.0
384.00	5.62	5.5	0.1	384.00	5.56	5.6	0.0	384.00	5.58	5.6	0.0
386.67	5.56	5.5	0.0	386.67	5.59	5.6	0.0	386.67	5.59	5.6	0.0
389.33	5.53	5.5	0.0	389.33	5.60	5.6	0.0	389.33	5.61	5.6	0.0
392.00	5.54	5.6	0.0	392.00	5.64	5.6	0.0	392.00	5.64	5.6	0.0
394.67	5.48	5.6	-0.1	394.67	5.66	5.7	0.0	394.67	5.67	5.7	0.0
397.33	5.61	5.6	0.0	397.33	5.71	5.7	0.0	397.33	5.70	5.7	0.0
400.00	5.72	5.6	0.1	400.00	5.70	5.7	0.0	400.00	5.70	5.7	0.0
402.67	5.61	5.6	0.0	402.67	5.72	5.7	0.0	402.67	5.71	5.7	0.0

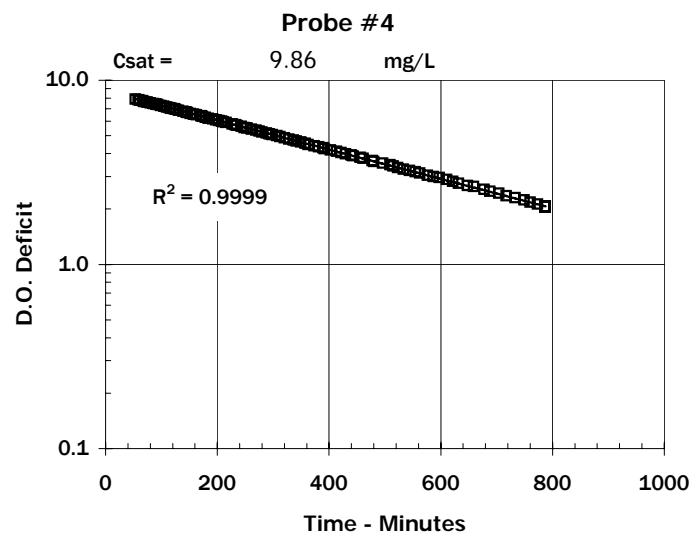
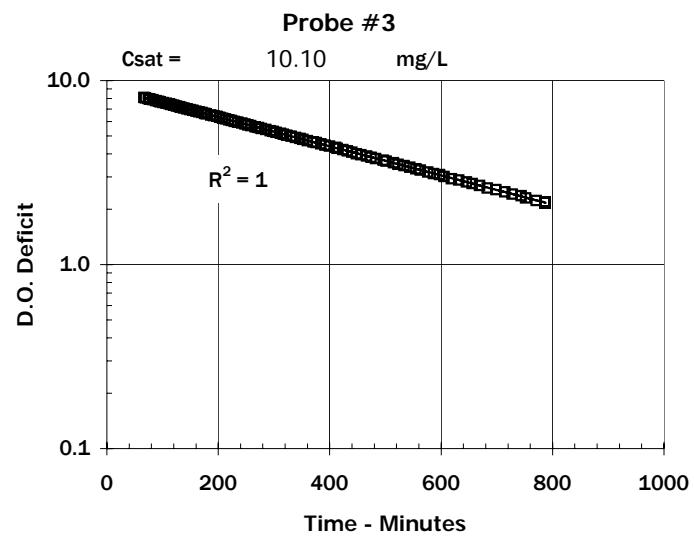
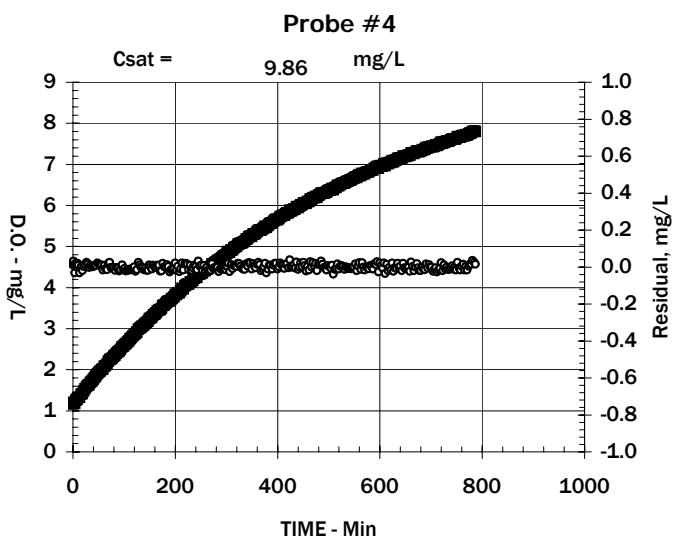
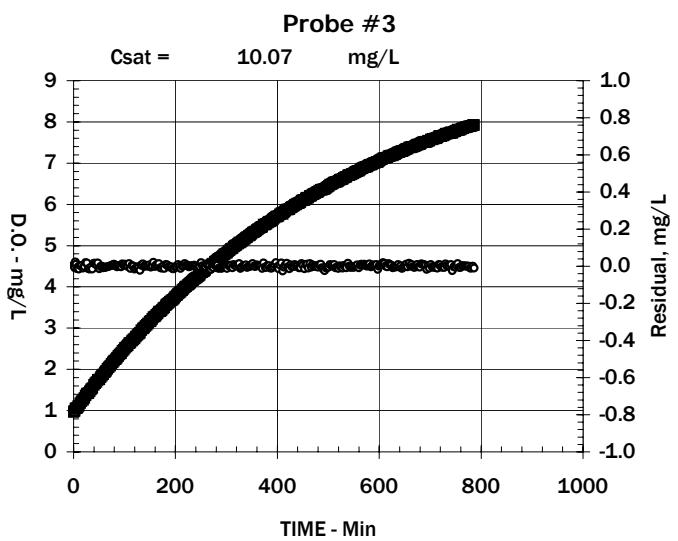
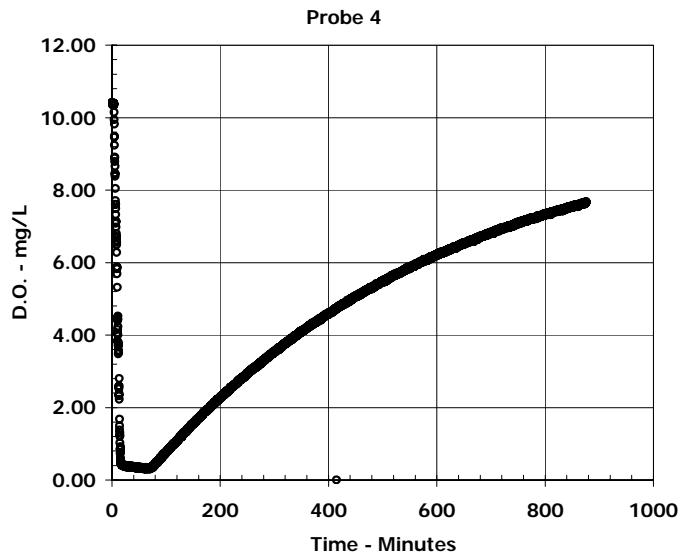
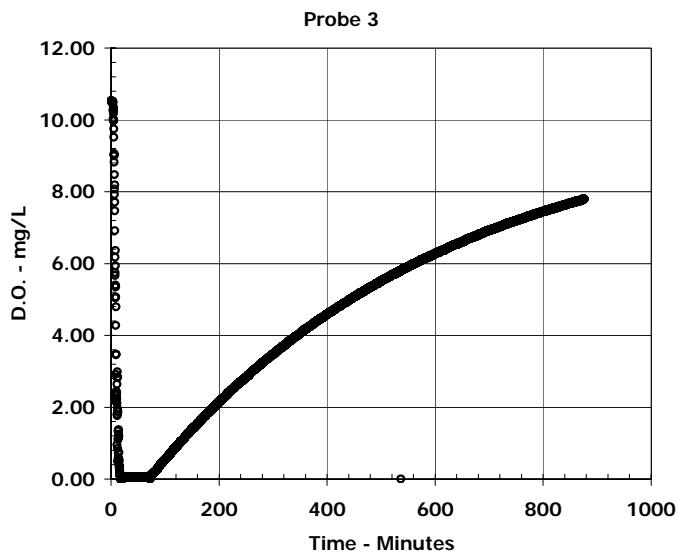
Pt. 1	est.	calc.	Pt. 2	est.	calc.	Pt. 3	est.	calc.	Pt. 4	est.	calc.				
CO	1.12	1.12	CO	1.29	1.29	CO	0.96	0.96	CO	1.15	1.15				
Kla-in	0.11	0.11	Kla-in	0.11	0.11	Kla-in	0.11	0.11	Kla-in	0.11	0.11				
C*	9.76	9.76	C*	9.71	9.71 <th>C*</th> <td>10.07</td> <td>10.07</td> <th>C*</th> <td>9.86</td> <td>9.86</td>	C*	10.07	10.07	C*	9.86	9.86				
Sq.Dif.	2.1547	Sq.Dif.	0.0812	Sq.Dif.	0.0233 <th>Sq.Dif.</th> <td>0.0694</td> <th>Sq.Dif.</th> <td>0.0694</td> <th>Sq.Dif.</th> <td>0.0694</td>	Sq.Dif.	0.0694	Sq.Dif.	0.0694	Sq.Dif.	0.0694				
Time	D.O.	D.O.calc	diff	Time	D.O.	D.O.calc	diff	Time	D.O.	D.O.calc	diff				
405.33	5.79	5.7	0.1	405.33	5.72	5.7	0.0	405.33	5.76	5.8	0.0	405.33	5.72	5.7	0.0
408.00	5.83	5.7	0.1	408.00	5.78	5.8	0.0	408.00	5.79	5.8	0.0	408.00	5.74	5.7	0.0
410.67	5.64	5.7	-0.1	410.67	5.79	5.8	0.0	410.67	5.77	5.8	0.0	410.67	5.76	5.7	0.0
413.33	5.61	5.7	-0.1	413.33	5.78	5.8	0.0	413.33	5.81	5.8	0.0	413.33	5.76	5.8	0.0
416.00	5.66	5.7	-0.1	416.00	5.83	5.8	0.0	416.00	5.84	5.8	0.0	416.00	5.80	5.8	0.0
418.67	5.69	5.8	-0.1	418.67	5.83	5.8	0.0	418.67	5.87	5.9	0.0	418.67	5.82	5.8	0.0
421.33	5.86	5.8	0.1	421.33	5.83	5.9	0.0	421.33	5.87	5.9	0.0	421.33	5.82	5.8	0.0
424.00	5.88	5.8	0.1	424.00	5.88	5.9	0.0	424.00	5.88	5.9	0.0	424.00	5.88	5.8	0.0
426.67	5.66	5.8	-0.2	426.67	5.88	5.9	0.0	426.67	5.92	5.9	0.0	426.67	5.86	5.9	0.0
429.33	5.82	5.8	0.0	429.33	5.91	5.9	0.0	429.33	5.93	5.9	0.0	429.33	5.88	5.9	0.0
432.00	5.92	5.9	0.1	432.00	5.92	5.9	0.0	432.00	5.95	6.0	0.0	432.00	5.91	5.9	0.0
434.67	5.86	5.9	0.0	434.67	5.91	5.9	0.0	434.67	5.99	6.0	0.0	434.67	5.91	5.9	0.0
437.33	5.92	5.9	0.0	437.33	5.98	6.0	0.0	437.33	6.00	6.0	0.0	437.33	5.97	5.9	0.0
440.00	5.81	5.9	-0.1	440.00	5.97	6.0	0.0	440.00	6.02	6.0	0.0	440.00	5.94	6.0	0.0
442.67	6.03	5.9	0.1	442.67	5.99	6.0	0.0	442.67	6.03	6.0	0.0	442.67	5.98	6.0	0.0
445.33	5.90	6.0	-0.1	445.33	6.02	6.0	0.0	445.33	6.05	6.1	0.0	445.33	6.02	6.0	0.0
448.00	5.90	6.0	-0.1	448.00	6.06	6.0	0.0	448.00	6.09	6.1	0.0	448.00	6.02	6.0	0.0
450.67	5.92	6.0	-0.1	450.67	6.05	6.1	0.0	450.67	6.10	6.1	0.0	450.67	6.06	6.0	0.0
453.33	6.12	6.0	0.1	453.33	6.08	6.1	0.0	453.33	6.10	6.1	0.0	453.33	6.06	6.1	0.0
456.00	5.97	6.0	-0.1	456.00	6.11	6.1	0.0	456.00	6.14	6.1	0.0	456.00	6.05	6.1	0.0
458.67	5.91	6.0	-0.1	458.67	6.12	6.1	0.0	458.67	6.16	6.2	0.0	458.67	6.09	6.1	0.0
461.33	6.17	6.1	0.1	461.33	6.12	6.1	0.0	461.33	6.16	6.2	0.0	461.33	6.09	6.1	0.0
464.00	6.03	6.1	-0.1	464.00	6.13	6.1	0.0	464.00	6.21	6.2	0.0	464.00	6.15	6.1	0.0
466.67	6.15	6.1	0.1	466.67	6.16	6.2	0.0	466.67	6.21	6.2	0.0	466.67	6.14	6.1	0.0
469.33	6.01	6.1	-0.1	469.33	6.17	6.2	0.0	469.33	6.24	6.2	0.0	469.33	6.18	6.2	0.0
472.00	6.09	6.1	0.0	472.00	6.21	6.2	0.0	472.00	6.25	6.2	0.0	472.00	6.18	6.2	0.0
474.67	6.15	6.2	0.0	474.67	6.22	6.2	0.0	474.67	6.27	6.3	0.0	474.67	6.22	6.2	0.0
477.33	6.29	6.2	0.1	477.33	6.25	6.2	0.0	477.33	6.29	6.3	0.0	477.33	6.20	6.2	0.0
480.00	6.22	6.2	0.0	480.00	6.25	6.2	0.0	480.00	6.30	6.3	0.0	480.00	6.25	6.2	0.0
482.67	6.33	6.2	0.1	482.67	6.27	6.3	0.0	482.67	6.33	6.3	0.0	482.67	6.27	6.3	0.0
485.33	6.32	6.2	0.1	485.33	6.28	6.3	0.0	485.33	6.35	6.3	0.0	485.33	6.30	6.3	0.0
488.00	6.32	6.2	0.1	488.00	6.29	6.3	0.0	488.00	6.35	6.4	0.0	488.00	6.30	6.3	0.0
490.67	6.27	6.3	0.0	490.67	6.31	6.3	0.0	490.67	6.36	6.4	0.0	490.67	6.30	6.3	0.0
493.33	6.32	6.3	0.0	493.33	6.35	6.3	0.0	493.33	6.37	6.4	0.0	493.33	6.31	6.3	0.0
496.00	6.37	6.3	0.1	496.00	6.36	6.3	0.0	496.00	6.40	6.4	0.0	496.00	6.32	6.3	0.0
498.67	6.21	6.3	-0.1	498.67	6.36	6.4	0.0	498.67	6.42	6.4	0.0	498.67	6.36	6.4	0.0
501.33	6.40	6.3	0.1	501.33	6.38	6.4	0.0	501.33	6.45	6.5	0.0	501.33	6.37	6.4	0.0
504.00	6.38	6.3	0.0	504.00	6.40	6.4	0.0	504.00	6.48	6.5	0.0	504.00	6.38	6.4	0.0
506.67	6.36	6.4	0.0	506.67	6.42	6.4	0.0	506.67	6.49	6.5	0.0	506.67	6.41	6.4	0.0
509.33	6.31	6.4	-0.1	509.33	6.41	6.4	0.0	509.33	6.51	6.5	0.0	509.33	6.38	6.4	0.0
512.00	6.32	6.4	-0.1	512.00	6.44	6.4	0.0	512.00	6.53	6.5	0.0	512.00	6.42	6.4	0.0
514.67	6.47	6.4	0.1	514.67	6.47	6.5	0.0	514.67	6.53	6.5	0.0	514.67	6.45	6.5	0.0
517.33	6.34	6.4	-0.1	517.33	6.46	6.5	0.0	517.33	6.55	6.6	0.0	517.33	6.49	6.5	0.0
520.00	6.49	6.4	0.0	520.00	6.49	6.5	0.0	520.00	6.56	6.6	0.0	520.00	6.48	6.5	0.0
522.67	6.54	6.5	0.1	522.67	6.53	6.5	0.0	522.67	6.59	6.6	0.0	522.67	6.51	6.5	0.0
525.33	6.55	6.5	0.1	525.33	6.53	6.5	0.0	525.33	6.60	6.6	0.0	525.33	6.53	6.5	0.0
528.00	6.35	6.5	-0.1	528.00	6.54	6.5	0.0	528.00	6.61	6.6	0.0	528.00	6.54	6.5	0.0
530.67	6.32	6.5	-0.2	530.67	6.53	6.6	0.0	530.67	6.64	6.6	0.0	530.67	6.54	6.6	0.0
533.33	6.54	6.5	0.0	533.33	6.56	6.6	0.0	533.33	6.65	6.7	0.0	533.33	6.57	6.6	0.0
536.00	6.79	6.5	0.3	536.00	6.58	6.6	0.0	536.00	6.67	6.7	0.0	536.00	6.58	6.6	0.0
538.67	6.51	6.6	0.0	538.67	6.61	6.6	0.0	538.67	6.71	6.7	0.0	538.67	6.59	6.6	0.0
541.33	6.48	6.6	-0.1	541.33	6.61	6.6	0.0	541.33	6.71	6.7	0.0	541.33	6.61	6.6	0.0
544.00	6.60	6.6	0.0	544.00	6.69	6.6	0.1	544.00	6.72	6.7	0.0	544.00	6.62	6.6	0.0
546.67	6.44	6.6	-0.2	546.67	6.63	6.7	0.0	546.67	6.74	6.7	0.0	546.67	6.64	6.6	0.0
549.33	6.69	6.6	0.1	549.33	6.67	6.7	0.0	549.33	6.75	6.8	0.0	549.33	6.67	6.7	0.0
552.00	6.59	6.6	0.0	552.00	6.68	6.7	0.0	552.00	6.77	6.8	0.0	552.00	6.70	6.7	0.0
554.67	6.58	6.6	-0.1	554.67	6.69	6.7	0.0	554.67	6.79	6.8	0.0	554.67	6.68	6.7	0.0
557.33	6.70	6.7	0.0	557.33	6.73	6.7	0.0	557.33	6.81	6.8	0.0	557.33	6.72	6.7	0.0
560.00	6.58	6.7	-0.1	560.00	6.74	6.7	0.0	560.00	6.81	6.8	0.0	560.00	6.75	6.7	0.0
562.67	6.50	6.7	-0.2	562.67	6.76	6.7	0.0	562.67	6.84	6.8	0.0	562.67	6.73	6.7	0.0
565.33	6.62	6.7	-0.1	565.33	6.75	6.8	0.0	565.33	6.86	6.9	0.0	565.33	6.78	6.8	0.0
568.00	6.78	6.7	0.1	568.00	6.75	6.8	0.0	568.00	6.87	6.9	0.0	568.00	6.77	6.8	0.0
570.67	6.74	6.7	0.0	570.67	6.77	6.8	0.0	570.67	6.89	6.9	0.0	570.67	6.77	6.8	0.0
573.33	6.68	6.8	-0.1	573.33	6.79	6.8	0.0	573.33	6.91	6.9	0.0	573.33	6.80	6.8	0.0
576.00	6.93	6.8	0.2	576.00	6.83	6.8	0.0	576.00	6.92	6.9	0.0	576.00	6.81	6.8	0.0
578.67	6.78	6.8	0.0	578.67	6.83	6.8	0.0	578.67	6.94	6.9	0.0	578.67	6.82	6.8	0.0
581.33	6.92	6.8	0.1	581.33	6.82	6.8	0.0	581.33	6.96	6.9	0.0	581.33	6.85	6.8	0.0
584.00	6.79	6.8	0.0	584.00	6.85	6.9	0.0	584.00	6.96	7.0	0.0	584.00	6.86	6.9	0.0
586.67	6.86	6.8	0.0	586.67	6.86	6.9	0.0	586.67	6.98	7.0	0.0	586.67	6.86	6.9	0.0
589.33	6.93	6.8	0.1	589.33	6.88	6.9	0.0</td								

Pt. 1	est.	calc.	Pt. 2	est.	calc.	Pt. 3	est.	calc.	Pt. 4	est.	calc.
CO	1.12	1.12	CO	1.29	1.29	CO	0.96	0.96	CO	1.15	1.15
Kla-in	0.11	0.11	Kla-in	0.11	0.11	Kla-in	0.11	0.11	Kla-in	0.11	0.11
C*	9.76	9.76	C*	9.71	9.71 <th>C*</th> <td>10.07</td> <td>10.07</td> <th>C*</th> <td>9.86</td> <td>9.86</td>	C*	10.07	10.07	C*	9.86	9.86
Sq.Dif.	2.1547	Sq.Dif.	0.0812	Sq.Dif.	0.0233 <th>Sq.Dif.</th> <td>0.0694</td> <th>Sq.Dif.</th> <td>0.0694</td> <th>Sq.Dif.</th> <td>0.0694</td>	Sq.Dif.	0.0694	Sq.Dif.	0.0694	Sq.Dif.	0.0694
Time	D.O.	D.O.calc	diff	Time	D.O.	D.O.calc	diff	Time	D.O.	D.O.calc	diff
613.33	6.95	7.0	0.0	613.33	7.02	7.0	0.0	613.33	7.12	7.1	0.0
616.00	7.05	7.0	0.1	616.00	7.01	7.0	0.0	616.00	7.14	7.1	0.0
618.67	7.15	7.0	0.2	618.67	7.00	7.0	0.0	618.67	7.17	7.2	0.0
621.33	6.97	7.0	-0.1	621.33	7.05	7.0	0.0	621.33	7.18	7.2	0.0
624.00	6.97	7.0	-0.1	624.00	7.04	7.1	0.0	624.00	7.19	7.2	0.0
626.67	6.96	7.0	-0.1	626.67	7.07	7.1	0.0	626.67	7.19	7.2	0.0
629.33	7.03	7.0	0.0	629.33	7.09	7.1	0.0	629.33	7.21	7.2	0.0
632.00	7.34	7.1	0.3	632.00	7.09	7.1	0.0	632.00	7.22	7.2	0.0
634.67	7.02	7.1	-0.1	634.67	7.14	7.1	0.0	634.67	7.24	7.2	0.0
637.33	6.97	7.1	-0.1	637.33	7.14	7.1	0.0	637.33	7.26	7.3	0.0
640.00	7.00	7.1	-0.1	640.00	7.14	7.1	0.0	640.00	7.26	7.3	0.0
642.67	6.95	7.1	-0.2	642.67	7.15	7.1	0.0	642.67	7.28	7.3	0.0
645.33	7.17	7.1	0.0	645.33	7.18	7.2	0.0	645.33	7.28	7.3	0.0
648.00	7.26	7.1	0.1	648.00	7.17	7.2	0.0	648.00	7.30	7.3	0.0
650.67	7.11	7.2	0.0	650.67	7.18	7.2	0.0	650.67	7.32	7.3	0.0
653.33	7.04	7.2	-0.1	653.33	7.21	7.2	0.0	653.33	7.34	7.3	0.0
656.00	7.33	7.2	0.2	656.00	7.19	7.2	0.0	656.00	7.34	7.3	0.0
658.67	7.35	7.2	0.2	658.67	7.22	7.2	0.0	658.67	7.38	7.4	0.0
661.33	7.11	7.2	-0.1	661.33	7.21	7.2	0.0	661.33	7.38	7.4	0.0
664.00	7.16	7.2	-0.1	664.00	7.23	7.2	0.0	664.00	7.40	7.4	0.0
666.67	7.32	7.2	0.1	666.67	7.25	7.3	0.0	666.67	7.40	7.4	0.0
669.33	7.10	7.2	-0.1	669.33	7.28	7.3	0.0	669.33	7.41	7.4	0.0
672.00	7.14	7.3	-0.1	672.00	7.28	7.3	0.0	672.00	7.43	7.4	0.0
674.67	7.34	7.3	0.1	674.67	7.29	7.3	0.0	674.67	7.45	7.4	0.0
677.33	7.46	7.3	0.2	677.33	7.32	7.3	0.0	677.33	7.45	7.5	0.0
680.00	7.07	7.3	-0.2	680.00	7.32	7.3	0.0	680.00	7.46	7.5	0.0
682.67	7.39	7.3	0.1	682.67	7.33	7.3	0.0	682.67	7.49	7.5	0.0
685.33	7.20	7.3	-0.1	685.33	7.30	7.3	0.0	685.33	7.50	7.5	0.0
688.00	7.45	7.3	0.1	688.00	7.32	7.4	0.0	688.00	7.51	7.5	0.0
690.67	7.38	7.3	0.0	690.67	7.34	7.4	0.0	690.67	7.52	7.5	0.0
693.33	7.12	7.4	-0.2	693.33	7.35	7.4	0.0	693.33	7.51	7.5	0.0
696.00	7.26	7.4	-0.1	696.00	7.40	7.4	0.0	696.00	7.54	7.5	0.0
698.67	7.43	7.4	0.1	698.67	7.40	7.4	0.0	698.67	7.54	7.6	0.0
701.33	7.40	7.4	0.0	701.33	7.43	7.4	0.0	701.33	7.57	7.6	0.0
704.00	7.34	7.4	-0.1	704.00	7.48	7.4	0.1	704.00	7.57	7.6	0.0
706.67	7.44	7.4	0.0	706.67	7.44	7.4	0.0	706.67	7.58	7.6	0.0
709.33	7.37	7.4	-0.1	709.33	7.46	7.4	0.0	709.33	7.59	7.6	0.0
712.00	7.35	7.4	-0.1	712.00	7.44	7.5	0.0	712.00	7.61	7.6	0.0
714.67	7.37	7.4	-0.1	714.67	7.49	7.5	0.0	714.67	7.62	7.6	0.0
717.33	7.38	7.5	-0.1	717.33	7.50	7.5	0.0	717.33	7.65	7.6	0.0
720.00	7.43	7.5	0.0	720.00	7.50	7.5	0.0	720.00	7.66	7.7	0.0
722.67	7.50	7.5	0.0	722.67	7.49	7.5	0.0	722.67	7.66	7.7	0.0
725.33	7.45	7.5	0.0	725.33	7.51	7.5	0.0	725.33	7.67	7.7	0.0
728.00	7.72	7.5	0.2	728.00	7.49	7.5	0.0	728.00	7.68	7.7	0.0
730.67	7.73	7.5	0.2	730.67	7.50	7.5	0.0	730.67	7.71	7.7	0.0
733.33	7.74	7.5	0.2	733.33	7.52	7.5	0.0	733.33	7.71	7.7	0.0
736.00	7.63	7.5	0.1	736.00	7.52	7.6	0.0	736.00	7.72	7.7	0.0
738.67	7.66	7.5	0.1	738.67	7.56	7.6	0.0	738.67	7.73	7.7	0.0
741.33	7.57	7.6	0.0	741.33	7.57	7.6	0.0	741.33	7.75	7.7	0.0
744.00	7.54	7.6	0.0	744.00	7.55	7.6	0.0	744.00	7.73	7.7	0.0
746.67	7.55	7.6	0.0	746.67	7.57	7.6	0.0	746.67	7.76	7.7	0.0
749.33	7.56	7.6	0.0	749.33	7.64	7.6	0.0	749.33	7.77	7.8	0.0
752.00	7.73	7.6	0.1	752.00	7.67	7.6	0.0	752.00	7.79	7.8	0.0
754.67	7.53	7.6	-0.1	754.67	7.68	7.6	0.0	754.67	7.81	7.8	0.0
757.33	7.54	7.6	-0.1	757.33	7.65	7.6	0.0	757.33	7.80	7.8	0.0
760.00	7.52	7.6	-0.1	760.00	7.66	7.6	0.0	760.00	7.81	7.8	0.0
762.67	7.68	7.6	0.0	762.67	7.65	7.7	0.0	762.67	7.84	7.8	0.0
765.33	7.90	7.6	0.2	765.33	7.68	7.7	0.0	765.33	7.85	7.8	0.0
768.00	7.63	7.7	0.0	768.00	7.70	7.7	0.0	768.00	7.86	7.9	0.0
770.67	7.74	7.7	0.1	770.67	7.67	7.7	0.0	770.67	7.87	7.9	0.0
773.33	7.42	7.7	-0.3	773.33	7.70	7.7	0.0	773.33	7.88	7.9	0.0
776.00	7.79	7.7	0.1	776.00	7.71	7.7	0.0	776.00	7.89	7.9	0.0
778.67	7.37	7.7	-0.3	778.67	7.72	7.7	0.0	778.67	7.89	7.9	0.0
781.33	7.69	7.7	0.0	781.33	7.80	7.7	0.1	781.33	7.90	7.9	0.0
784.00	7.98	7.7	0.3	784.00	7.74	7.7	0.0	784.00	7.92	7.9	0.0
786.67	7.74	7.7	0.0	786.67	7.75	7.7	0.0	786.67	7.92	7.9	0.0

Probe 1			Probe 2			Probe 3			Probe 4				
Lower	11.66%	Upper	Lower	13.23%	Upper	Lower	9.54%	Upper	Lower	11.76%	Upper		
Value	Abs.Un.	%LSE	Value	Abs.Un.	%LSE	Value	Abs.Un.	%LSE	Value	Abs.Un.	%LSE		
C*	9.763	0.065	9.713	0.012	0.128	C*	10.070	0.007	0.067	C*	9.863	0.012	0.120
CO	1.124	0.016	1.288	0.003	0.241	CO	0.956	0.002	0.174	CO	1.149	0.003	0.250
KLaT	0.110	0.000	0.111	0.000	0.281	KLaT	0.111	0.000	0.140	KLaT	0.109	0.000	0.256
Error	0.085		Error	0.017		Error	0.009			Error	0.015		
PROJECT:	PHI (Faster Valve Test)												
DATE:	11/9/2006												
RUN:	4.00												



Project: PHi (Faster Valve Test)
 Date: Nov 09, 2006
 Run: 4



Project: PHi (Faster Valve Test)
 Date: Nov 09, 2006
 Run: 4

AIR FLOW RATE DETERMINATION
ANR 73 COMMERCIAL ANNULAR

PROJECT : PHi (Faster Valve Test)

$$\text{SCFM} = \frac{\text{C}''}{\frac{[\text{BP} + \text{LP}]}{[\text{LT} + 460]}}$$

$$\begin{aligned}\text{C}' &= \text{Fna} * \text{k} * \text{D}^2 * \text{Fra} * \text{Fpb} * \text{Ftb} * \text{Fg} * \text{Fpv} * \text{Faa} * \text{Fl} * \text{Fm} * \text{Ya} \\ \text{C}'' &= \text{C}' \text{ VALUE CORRECTED FOR HUMIDITY}\end{aligned}$$

RUN # 4
DATE Nov-06

OPERATING CONDITIONS

ANNULAR TYPE		AWR-73	
BAROMETRIC PRESSURE	* BP	14.23 PSIA	
LINE PRESSURE	* LP	45.02 PSIG	
LINE TEMPERATURE	* LT	68 °F	
DIFFERENTIAL PRESSURE	* ^H	0.01 In. H2O	
RELATIVE HUMIDITY	* RH	57% %	
AMBIENT TEMPERATURE	*	15.5	68 °F
PIPE INSIDE DIAMETER	* D	4.026	In.
UNITS CONVERSION FACTOR	Fna	128.520	
ANNULAR FLOW COEFFICIENT	k	0.746	
SQUARE OF PIPE ID	D^2	16.209	
BASE PRESSURE		14.700	PSIA
BASE PRESSURE FACTOR	Fpb	1.002	
BASE TEMPERATURE		68.000	°F
BASE TEMPERATURE FACTOR	Ftb	1.015	
THERMAL EXPANSION FACTOR	Faa	1.001	
MANOMETER LOCATION FACTOR	Fl	1.000	
HG MANOMETER CORRECTION FACTOR	Fm	1.000	
REYNOLD NUMBER	Rd	15,244.7	
FLOWING VISCOSITY	vis	0.018 cP	
REYNOLD NUMBER FACTOR	Fra	0.965	
SPECIFIC GRAVITY	g	1.000	
SPECIFIC GRAVITY FACTOR	Fg	1.000	
SUPERCOMPRESSIBILTY	Z	0.998	
SUPERCOMPRESSIBILITY FACTOR	Fpv	1.001	
GAS EXPANSION FACTOR	Ya	1.000	
SCFM UNCORRECTED FOR HUMIDITY	SCFM	38.3	
C'		1,527.28	
VAPOR PRESSURE OF WATER AMB. TEMP.	VP	0.340	
ACTUAL CUBIC FEET PER MINUTE	ACFM	9.5	107.4
HUMIDITY CORRECTED STANDARD AIR FLOW	SCFM	38.1	@68°F, 36% RH, 14.7 PSIA
INLET CUBIC FEET PER MINUTE	ICFM	39.5	
C"		1,518.30	

FORMULAS AND FACTORS DERIVED FROM:

L.K.Spink: "Principles and Practice of FLOW METER ENGINEERING"; Ninth Ed., Nov 1975; The FOXBORO CO., Foxboro, Mass.
"ORIFICE FLOW METER"; THE BRISTOL COMPANY; Waterbury, Conn.
"ANNULAR FLOW HANDBOOK"; August 1978; DIETERICH STANDARD CORPORATION; Boulder, Co.

HUMIDITY CORRECTED AIR FLOW DETERMINED per: "ASCE STANDARD Measurement of Oxygen Transfer in Clean Water"; ANNEX A; July 1984; American Society of Civil Engineers